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ELECTRICAL RESISTIVITY OF CHROMIUM, COBALT, IRON, AND NICKEL

> By T. K. Chu and C. Y. Ho

> > CINDAS Report 60

June 1982

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PREFACE

This technical report was prepared by the Center for Information and Numerical Data Analysis and Synthesis (CINDAS), Purdue University, West Lafayette, Indiana, under the auspices of the Office of Standard Reference Data of the National Bureau of Standards (NBS), Department of Commerce, Washington, D.C.

This report represents the most exhaustive compilation and critical evaluation of the recorded world knowledge on the electrical resistivity of chromium, cobalt, iron, and nickel, and is one of a series of technical reports on the electrical resistivity of selected elements. The literature search and data compilation have been done in a most extensive and detailed manner, making it possible for all users of the subject to have access to the original data without having to duplicate the laborious and costly process of literature search and data extraction. Also, for the active researchers in the field, a detailed discussion is presented for each material, reviewing the available data and information, giving details of data analysis and synthesis, and discussing the considerations involved in arriving at the final recommended values.

It is hoped that this work will prove useful not only to the engineers and scientists in the field but also to other engineering research and development programs and for industrial applications, as it provides a wealth of knowledge heretofore unknown or inaccessible to many. In particular, it is thought that the critical evaluation, analysis and synthesis, and reference data generation constitute a unique aspect of this work.

Although this report is primarily the result of financial support and interest of the NBS Office of Standard Reference Data, the extensive documentary activity essential to this work was supported by the Defense Logistics Agency of the Department of Defense. Thanks are due Dr. H. J. White, Jr., of the NBS Office of Standard Reference Data for his guidance, cooperation, and sympathetic understanding during the course of this work.

ABSTRACT

This work compiles, reviews, and discusses the available data and information on the electrical resistivity of chromium, cobalt, iron, and nickel and presents the recommended values resulting from critical evaluation, correlation, analysis, and synthesis of the available data and information. The recommended values presented are uncorrected and also corrected for the thermal expansion of the material and cover the temperature range from 1 K to above the melting point into the molten state. The estimated uncertainties in most of the recommended values are about $\pm 5\%$.

Key words: Chromium; cobalt; conductivity; critical evaluation; data analysis; data compilation; data synthesis; electrical conductivity; electrical resistivity; elements; iron; metals; nickel; recommended values; resistivity.

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NOMLACLATURE

- A Constant in eqs (3b) and (8)
- c Impurity concentration
- C Constant in eq (3a)
- e Base of natural logarithm
- \hbar Planck constant divided by 2π
- k Boltzmann constant
- L Length of specimen at T
- L₀ Length of specimen at T₀
- $\Delta L = L L_0$
- M Atomic weight
- T Temperature
- T₀ Reference temperature
- $x = \hbar \omega / kT$
- α Constant in eqs (7) and (8)
- Δ Deviation from the Matthiessen's rule
- θ_{D} Debye temperature
- $\boldsymbol{\theta}_R$ Characteristic temperature for intrinsic electrical resistivity
- ρ Electrical resistivity
- ρ₀ Residual electrical resistivity
- ρ_e Electrical resistivity due to electron-electron scattering
- ρ_i Intrinsic electrical resistivity
- ω Phonon angular frequency

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1. INTRODUCTION

1

The principal objective of this project was to exhaustively compile, critically evaluate, analyze, and synthesize all the available data and information on the electrical resistivity of a large number of selected elements and to generate recommended values over a full range of temperature from 1 K to the melting point and beyond. The results on the electrical resistivity of chromium, cobalt, iron, and nickel are presented in this work, which is one in a series of similar works on the electrical resistivity of selected elements, some published $[1-3]^1$. The comprehensive study of the electrical resistivity of the elements at the Center for Information and Numerical Data Analysis and Synthesis (CINDAS) has been a continuation of a similar extensive work on the thermal conductivity of the elements [4].

The general background information on this work is given in Section 2, which includes a brief introduction to the theory of the electrical resistivity of metals and a detailed explanation of the specifics and conventions used in the presentation of the data and information.

The experimental data and information and the recommended values for the electrical resistivity of the four elements are presented in Section 3. In the discussion of the electrical resistivity of each element, individual pieces of available data and information are reviewed, details of data analysis and synthesis are given, the considerations involved in arriving at the final assessment and recommendation are discussed, the recommended values and the experimental data are compared, and the uncertainties in the recommended values are stated. Recommended values uncorrected and corrected for the thermal expansion of the material are both presented in this section. The values cover the temperature range from 1 K to above the melting point.

The last three sections are for acknowledgments, appendices, and references. There are two appendices given. The first appendix presents a logical organization of the methods for the measurement of electrical resistivity. The methods are are designated with respective code letters and the same code letters are used in the "Method Used" column of the Table of Measurement Information for indicating

¹Numbers in brackets indicate literature references listed in Section 6.

the experimental methods used by the various authors. The second appendix presents conversion factors for the units of electrical resistivity, which may be used to convert easily the electrical resistivity values in the SI units given in this work to values in any of the several other units listed.

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2. GENERAL BACKGROUND

2.1. Theoretical Background

It was found experimentally by Matthiessen [5,6] that the increase in the electrical resistivity of a metal due to the presence of a small amount of another metal in solid solution is independent of the temperature. According to this Matthiessen's rule, the total electrical resitivity of an impure metal may therefore be separated into two additive contributions and written in the form

$$\rho(c,T) = \rho_0(c) + \rho_1(T),$$
 (1)

where ρ_0 is the residual resistivity caused by the scattering of electrons by impurity atoms and lattice defects and is temperature-independent but dependent on the impurity concentration, c, and ρ_i is the temperature-dependent intrinsic resistivity arising from the scattering of electrons by lattice waves, or phonons.

In reality, however, deviations from Matthiessen's rule do occur. Thus, in general the electrical resistivity of an impure metal is given by

$$\rho(c,T) = \rho_0(c) + \rho_1(T) + \Delta(c,T),$$
 (2)

where Δ is the deviation from the Matthiessen's rule.

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The intrinsic electrical resistivity which is due to scattering of electrons by phonons may be approximated by the Bloch-Grüneisen formula [7,8]:

$$\rho_{i} = \frac{C}{M\theta_{R}} \left(\frac{T}{\theta_{R}} \right)^{5} \int_{0}^{\theta_{R}/T} \frac{x^{5}e^{x} dx}{(e^{x} - 1)^{2}}$$
(3a)

$$= A \left[\frac{T}{\theta_R}\right]^5 \int_{0}^{\theta_R/T} \frac{x^5 e^x dx}{(e^x - 1)^2},$$
 (3b)

where C is a constant characteristic of the metal and proportional to the square of the electron-phonon interaction constant, M is the atomic weight, θ_{R} is a characteristic temperature of the metal which characterizes its intrinsic electrical resistivity in the same way as the Debye temperature,

 $\theta_{\rm D}$, characterizes its lattice specific heat, and A \equiv C/M $\theta_{\rm R}$. The dimensionless variable of integration x = $\hbar\omega/kT$, where \hbar is the Planck constant divided by 2π , ω is the phonon angular frequency, and k is the Boltzmann constant. The derivation of eq (3) is based on the simplifying assumptions that the Fermi surface is spherical, that the conduction electrons can be treated as free in the first approximation, that the spectrum of lattice vibrations is that of the Debye model, that the phonon distribution is essentially undisturbed by the scattering processes, and that electron-phonon Umklapp processes can be ignored. Consequently, it is perhaps most reasonable to expect the Bloch-Grüneisen formula to agree with experiment in the case of monovalent metals. Nevertheless, the intrinsic resistivity of many metals can be well represented by eq (3) over a wide temperature range by a suitable choice of $\theta_{\rm R}$ and C, though no single values of $\theta_{\rm p}$ can fits the data at all temperatures.

At low temperatures (T $\leq \theta_R/20$), eq (3a) reduced to

$$\rho_{i} = \frac{124.4C}{M\theta_{R}} \left(\frac{T}{\theta_{R}}\right)^{5}, \qquad (4)$$

while at high temperatures (T > θ_p), to a good approximation, it reduces to

$$\rho_{1} \approx \frac{C}{4M\theta_{R}} \left(\frac{T}{\theta_{R}} \right).$$
 (5)

Thus it agrees with the experimental facts that at very low temperatures the intrinsic electrical resistivity (after subtracting ρ_0 from ρ) of most metallic elements is proportional to T⁵, and at high temperatures the resist_vity of most metals increases approximately linearly with temperature.

In separating the electrical resistivity into its components, the temperature dependent part sometimes includes the electrical resistivity due to electron-electron scattering, ρ_e ; indeed, this is thought to be the dominant temperature-dependent term in transition metals at low temperatures. That is,

$$\rho = \rho_0 + \rho_a + \rho_i(\mathbf{T}) \tag{6}$$

As in the case of the scattering of electrons by phonons, electron-electron collisions are of two types: normal processes in which the total wave vector is conserved, and Umklapp processes in which the total wave vectors before and after the collision differ by a reciprocal lattice vector. On the other hand, unlike electron-phonon Umklapp processes which are frozen out at low temperatures

if the Fermi surface is everywhere clear of the zone boundary, electron-electron Umklapp processes are not frozen out at low temperatures. Normal processes, involving the collision between two s-band conduction electrons, do not contribute directly to the electrical resistivity because they do not change the total momentum and thus have no effect on the current. Normal processes involving the scattering of an s-band conduction electron by a non-conducting d-band electron do contribute to the electrical resistivity, and are thought to be the dominant temperature-dependent resistive processes in transition elements and their alloys at very low temperatures, since their resistivities show the T^2 temperature dependence expected for electron-electron scattering rather than the T^5 temperature dependence expected for the intrinsic resistivity. This temperature dependence of the electrical resistivity due to electronelectron scattering:

$$\rho_{\rm g} = \alpha T^2 \tag{7}$$

comes about through the double application of the exclusion principle in the scattering processes; it applies to both the initial states and final states. In eq (7), α is a constant.

Umklapp processes between two conduction electrons do contribute to the electrical resistivity. Because these processes involve a reciprocal lattice vector, the wave functions of the electrons involved cannot be regarded as simple plane waves, but must be treated as true Bloch functions having the periodicity of the lattice. The results of this are to introduce into the expression for the resistivity the square of an interference factor. Apparently this factor is quite small, as the low temperature electrical resistivity of most ordinary metals does not show the T^2 temperature dependence expected for such a resistive mechanism.

Substituting eqs (7) and (3b) into eq (6) yields

$$\rho = \rho_0 + \alpha T^2 + A \left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x^5 e^x dx}{(e^x - 1)^2} .$$
 (8)

Equation (8) has been used frequently in analyzing the experimental data and in generating the recommended values for the electrical resistivity of cobalt, iron, and nickel at low temperatures.

2.2. Presentation of Data and Information

In each of the subsections in Section 3, electrical resistivity data and information for each element are presented in the following order:

- (1) A discussion text,
- (2) A table of recommended values,
- (3) A figure presenting recommended values and experimental data as a function of temperature in log-log scale,
- (4) A figure presenting recommended values and experimental data as a function of temperature in linear scale,
- (5) A table giving measurement information on the experimental data presented in the figures, and
- (6) A comparable table tabulating experimental data of all the data sets presented in the figures and/or listed in the tables.

In the discussion text on the electrical resistivity of each alloy system, individual pieces of available data and information are reviewed, details of data analysis and synthesis are given, the considerations involved in arriving at the final assessment and recommendation are discussed, the recommended values and the experimental data are compared, and the uncertainties of the recommended values are stated.

The recommended values are for well-annealed high-purity specimens of the respective elements; however, those values for low temperatures are applicable only to the particular specimens having residual electrical resistivities as given at 1 K in the tables.

Recommended values uncorrected and corrected for the thermal expansion of the element are both given in the table. The uncorrected and corrected values are related by the following equation:

$$\rho_{\text{corrected}}(T) = \left(1 + \frac{\Delta L(T)}{L_0}\right) \rho_{\text{uncorrected}}(T), \qquad (9)$$

where $\Delta L = L - L_0$, and L and L_0 are the lengths of the specimen at any temperature T and at a reference temperature T_0 , respectively. The thermal expansion correction amounts roughly to about -0.2% to -0.7% at very low temperatures, zero at room temperature, about 0.3% to 0.7% at 500 K, and about 2% near the melting point of the element. The recommended values in some cases are given with more significant figures than warranted, which is merely for tabular smoothness or for the convenience of internal comparison. Hence, the number of significant figures given in the table has no bearing on the degree of accuracy or uncertainty in the values; the uncertainty in the values is always explicitly stated.

In the figures, a data set consisting of a single data point is denoted by a number enclosed by a square, and a curve that connects a set of two or more data points is denoted by a ringed number. These data set numbers correspond to those listed in the accompanying tables providing measurement information and tabulating numerical data for each of the data sets. When several sets of data are too close together to be distinguishable, some of the data sets, though listed and tabulated in the tables, are omitted from the figure for the sake of clarity. The data set numbers of those data sets omitted from the figure are asterisked in both tables providing the measurement information and tabulating the experimental data. If only part of the data points of a data set are omitted from the figure, only those data points omitted are asterisked in the table tabulating the experimental data.

The tables providing the measurement information contain for each set of experimental data the following information: data set number, reference number, author(s), year of publication, experimental method used for the measurement, temperature range covered by the data, name and specimen designation, specimen composition, specification and characterization, and information on measurement conditions, which are contained in the original paper. The experimental methods used for the measurement of the electrical resistivity are indicated in the column heated "Method Used" in the table by the following code letters:

- A Direct-current potentiometer method
- B Direct-current bridge method
- C Alternating-current potentiometer method
- D Alternating-current brige method
- G Galvanometer amplifier method
- R Rotating magnetic field method
- V Voltmeter and ammeter direct reading method

This symbol means either that the method described by the author is not sufficient for assigning a specific code letter or that the use of a code letter would not convey enough of the information reported in the research document, and therefore the method used is described briefly in the last column of the table.

Details of these and other methods for the measurement of electrical resistivity may be found in the literature references given in Appendix 5.1, which presents a complete scheme for the classification and organization of the methods.

In the tables tabulating the experimental data, all the original data reported in different units have been converted to have the same units: the SI units $10^{-8} \Omega$ m. The recommended values generated are also given in the same units. Conversion factors for the units of electrical resistivity, which may be used to convert the electrical resistivity values in the SI units given in this work to values in other units, are given in Appendix 5.2.

3. ELECTRICAL RESISTIVITY DATA AND INFORMATION

3.1. Chromium

There are 163 sets of experimental data available for the electrical resistivity of chromium. The information on specimen characterization and measurement condition for each of the data sets is given in table 2. The data are tabulated in table 3 and shown partially in figures 1 and 2.

Chromium undergoes an antiferromagnetic-paramagnetic transition at about 312 K; it is not surprising that more than one third of the data sets deal with the behavior of the electrical resistivity at temperatures in the vicinity of the transition. In general, the purities of the chromium specimens studied are not as high as those of other more common elements, such as iron and nickel. Judging from the impurity analyses reported, a purity of 99.99% appears to be the highest available at the present time. It is therefore not unexpected that the reported residual resistivity ratios are not very high. Indeed, the highest for a polycrystalline specimen is 380 given by Laubitz and Matsumura [9] (data sets 53-61). Their specimen was the same as that of Moore et al. [10] (data sets 50-52), who reported a residual resistance ratio of 280. This specimen was prepared by compacting (apparently small) crystals, and by hot extending. The former authors, in addition, carried out extended annealing periods: four days at 1100 K and one day at 1200 K. The reported purity of this specimen was not particularly high; 99.98⁺% with major impurities of 0.0070% C and 0.0030% Fe. For comparison, the cast specimen of Meaden et al. [11-13] (data sets 69-75), had a reported purity of 99.999% with major impurities of 0.0010% C and 0.0080% 0. However, the residual resistance ratio of this specimen is only 178. After annealing at >1273 K for 75 hours (of which 50 hours is at 1473 K), the residual resistance ratio increases to 295 (data sets 76, 77). It is apparent that, in order to obtain a true indication of the residual resistivity of a chromium specimen, prolonged annealing at temperatures in excess of 1000 K is quite essential. The present recommendation for the electrical resistivity of chromium at low temperatures is only for chromium having a particular residual resistivity, which is based on the residual resistance ratio reported by Laubitz and Matsumura [9] for data set 53.

There are only a few data sets which give the electrical resistivity of chromium from liquid-helium temperature to room temperature in reasonably small temperature intervals: Harper et al. [14] (data set 17), Goff [15,16] (data sets 79,80), and Arajs et al. [17-20] (data sets 94-102). The data of Harper

et al. had been analyzed by White and Woods [21] who found the temperature dependent part of the resistivity proportional to $T^{3,2}$ for temperatures below 100 K. A similar analysis on the data sets 7, 79-80, and 99-100 substantiated the finding of White and Woods; the exponent was found to be 3.23, with an uncertainty of ±0.20. In addition, selected data points from those reported by Chiu et al. [22] (data set 46), and by Moore et al. [10] (data sets 47-50) in the temperature range 80-100 K are also in agreement with this finding. With a coefficient of 5.756 x $10^{-15} \Omega m K^{-3.23}$, the experimental data of ρ - ρ_0 predominantly stay within 0.1 x $10^{-8} \Omega m$ of the calculated values at the higher end of this temperature range, and within 0.002 x $10^{-8} \Omega m$ at lower temperatures (<20 K). (It is interesting to note that the specimen of Arajs et al. [17,18] (data sets 94-99) is for a single crystal specimen with residual resistivity of 1.06 x $10^{-8} \Omega m$.) The electrical resistivity values below 100 K were therefore obtained by the relation

 $\rho(10^{-8} \Omega m) = \rho_0 + 5.756 \times 10^{-7} T^{3.23}$ (10)

At temperatures above 100 K, the rate of increase of the temperature dependent part of the resistivity becomes slower with increasing temperature. The discrepancies between the data sets also become larger with increasing temperature, indicating that the deviation from Mattheissen's Rule becomes important. From studies of the electrical resistivities of chromium alloys (see, e.g., Arajs et al. [20], deVries [23], Cox and Lucke [24], Taylor [25], and Muheim and Müller [26]), it was found that impurities not only affect the values of the resistivity, but also the Néel temperature. Since the electrical resistivities of chromium and dilute chromium alloys generally show a local maximum at temperatures slightly below the Néel temperature, it is not unexpected that the data sets show greater discrepancies as the Néel temperature is approached. Furthermore, depending on the type of impurity, the electrical resistivity of a chromium alloy can be lower than that of the pure chromium at temperatures immediately below the Néel temperature of pure chromium (see, e.g., Taylor [25], Susuki [27] and deVries [23]). The recommended values in the temperature range from 100 K to the Néel temperature are based on the data of Moore et al. [10] (data set 50), and in the vicinity of the Néel temperature they are based on the above data and that of Laubitz and Matsumura [9] (data set 53). As it is mentioned previously, the same specimen was used in both of these two measurements: the latter authors annealed the specimen at a higher temperature for

long periods of time. The difference between the resistivity values of these data sets at ~ 300 K is $\sim 0.4\%$ or $\sim 0.05 \times 10^{-8} \Omega m$. This difference is higher than the difference of $\sim 0.01 \times 10^{-8} \Omega m$ in their residual resistivities (calculated from the reported residual resistance ratios); but is still within the limits given by the reported measurement inaccuracies. The data of Meaden et al. [13, 28] (data sets 76-78) for a specimen with a residual resistance ratio of 295 show slightly weaker temperature dependence: the values being $\sim 10\%$ above and $\sim 2\%$ below those of data set 50 at ~ 100 K and ~ 300 K, respectively.

The behavior of the electrical resistivity of chromium in the vicinity of the Néel temperature has been studied quite extensively: it goes through a broad maximum at approximately 4 K below the Néel temperature and decreases rapidly as the Néel temperature is approached. The temperature derivative of the electrical resistivity then goes through a spike-like minimum. The ensuing minimum in electrical resistivity value occurs at a few tenth of a degree above the Néel temperature. The position of the minimum in the temperature derivative has been associated with the Néel temperature. However it has been proposed recently, from theoretical calculations, that the temperature derivative of the electrical resistivity should follow a power law relation: $(T_N-T)T_N^{-1}$ (see, e.g., Suezaki and Mori [29], Alexander et al. [30]). The recent publication by Rapp et al. [31] showed that the power law was only applicable in the temperature range from $T_{\rm N}$ - 8.5 K to $T_{\rm N}$ - 0.5 K, and the temperature derivative of the measured resistance was at a minimum at about 0.18 degree below T_N determined by a fit to the power law relation. The simulataneous measurements of electrical resistivity and sublattice magnetization by neutron diffraction method on a single crystalline iodide chromium specimen by Ishikawa et al. [32] (data set 158), showed that the minimum in the electrical resistivity occurred at about 0.5 degree above the Néel temperature. They also found that there was some residual ordering above the transition. This residual ordering persisted till \sim 315 K, and was attributed by the authors to the strain introduced in spot welding the specimen. However, this interpretation appears to be in conflict with the observation of Stebler [33] (data sets 112-115), who reported considerable hysteresis across the Néel transition. Stebler attributed the hysteresis to (thermal) strain, but failed to observe appreciable residual ordering (again with neutron diffraction method) in his specimen. It is apparent that the critical phenomenon of antiferromagnetic-paramagnetic transition in chromium is

a complex one and is still subject to further investigations. Experimentally, the accurate determination of the electrical resistivity in the close vicinity of the Néel temperature poses considerable difficulties. This is due to the rapid change in the temperature derivative of the electrical resistivity over a narrow temperature range, while the value of the electrical resistivity itself changes only slightly. Thus, even for the same specimen, Laubitz and Matsumura [9] (data set 53) found that the position of the resistivity minimum was at 311.7 K, but from the data of Moore et al. [34] (data set 63), it appeared that the minimum occurred at around 312.3 K. For comparison, Matsumoto and Mitsui [35] stated that the minimum was at 312.0 K for a specimen with residual resistivity ratio comparable to that of the above (350 instead of 380). For these reasons, it is concluded that a recommendation for the detailed variation of the electrical resistivity of chromium at the close vicinity ($v\pm 0.5$ degree K) is beyond the scope of the present study. The position of the resistivity minimum is tentative taken at 311.7 K following Laubitz and Matsumura [9], as these authors apparently made their measurements at very small temperature intervals. This temperature is within ± 0.2 degree of those determined from the data of Anderson et al. [36] (data set 87), Stebler [33] (data sets 114, 115) and Trego and Mackintosh [37] (data set 116). The Néel temperature of chromium is tentatively taken as 311.5 K, as determined by specific heat measurements.

Even though hysteresis across the Néel transition is not generally mentioned by most authors, it has been reported by some: Mitsui and Tomizuka [38] (data sets 33, 34), and Stebler [33] (data sets 112, 113). If the hysteresis is caused by strain, as suggested by Stebler [33], it should disappear in specimens that have been annealed for a sufficiently long period of time at high temperatures and are heated up and/or cooled down through the transition at a sufficiently slow rate during the measurements.

For chromium, there is another transition occurring at about 120 K: the spin-flip transition. At this temperature, the polarizations of the spin-density waves, which give rise to the antiferromagnetism in chromium, changes from longitudinal (at lower temperatures) to transverse (at higher temperatures). Arajs [39], upon reanalyzing the earlier data of Arajs and Dunmyre [19] (data set 100), concluded that there is a change in the temperature coefficient of the resistivity, which was first reported by Matsumoto et al. [35]. Meaden et al. [12,13] (data sets [1-77] reported a step-type anomaly, in addition to a change of slope.

However, the slope changes reported are quite different: from $T^{2\cdot8}$ to $T^{2\cdot0}$ according to Arajs [39] and from $T^{2\cdot45}$ to $T^{2\cdot25}$ according to Meaden et al. [12,13]. In addition, the step-type anomaly, also reported by Kostina et al. [40] (data sets 134, 138) for single crystalline specimen, is in the opposite direction (a decrease instead of an increase in value) to that reported by Meaden et al. [12,13]. Most other authors did not report any unusual behavior of the electrical resistivity at this temperature, and Moore et al. [10] stated that the spin-flip transition did not have a noticeable effect on the electrical resistivity. Muir and Ström-Olsen [41] also did not detect any change of the temperature coefficient of the measured resistance of their single domain specimen at the spin-flip temperature. In generating the present recommended values, it is assumed that the electrical resistivity is not affected by this transition, and the values and their temperature derivative are continuous through the transition.

At temperatures above the Néel transition, the electrical resistivity of chromium varies smoothly with temperature. Among the available data sets, there are three from independent sources that agree well with one another: Moore et al. [34] (data set 64), Arajs et al. [20] (data set 102), and Cox and Lucke [24] (data set 103). The agreement between data sets 64 and 102 is within 1% from 400 to 1000 K, and between data sets 64 and 103 is within 2.5% from 400 to 1300 K. The recommended values from the Néel temperature to 1300 K are based on these three data sets, with more weight given to that of Moore et al. [34] (data set 64) since the specimen of this data set is the same as that of data sets 50 and 53 upon which the recommended values at lower temperatures are based. It should be noted here that the resistivity values reported by Moore et al. [34] had been corrected for thermal expansion. However, these authors did not report the method by which the correction was applied. Therefore, the comparison mentioned above was carried out after account had been taken of the effect of thermal expansion, using the recommended thermal expansion values of Touloukian et al. [42, p. 61].

There are a number of data sets for temperatures above 1300 K. The agreement between them is not good: the spread among them is about 20 x $10^{-8} \Omega m$ at 1500 K and 30 x $10^{-8} \Omega m$ at 1900 K. Even though there are five data sets (26, 27, 29, 82, 83) from essentially two groups of workers that show agreement within $\pm 4 \times 10^{-8} \Omega m$ at 1700 K, these data are considered not reliable. Those by Anderson et al. [43] (data sets 82, 83) give values that are much too low at lower temperatures, and

those by Baum et al. [44,45] (data sets 26, 27), and by Levin et al. [46] (data set 29) show slopes that are considered too low. In addition, the room temperature value given by data set 26 is much too high (by $\sim 4.5 \times 10^{-8} \Omega$ m than the recommended value). The recommended values from 1300 to 1700 K were derived by extrapolation of the recommended values for lower temperatures with a temperature dependence that was based roughly on the data by Powell and Tye [47] (data set 106) and by Anderson et al. [43] (data set 84). In this temperature range, both of these data sets show a slight curvature toward the temperature axis, and are more or less parallel to each other, even though data set 106 is for a 99.985% pure electrodeposited specimen and data set 84 is apparently for a single crystalline specimen. The slight curvature also appears to be evident in data sets 26, 27, and 29. The recommended values for temperatures from 1700 K to the melting point are based on numerical extrapolation of the values for 1300 to 1700 K. At 1700 K the recommended value is higher by $\sim 11\%$ (or $\sim 9 \times 10^{-8} \Omega$ m) than the data of Baum et al. [44,45] (data set 26, 27), and at 2100 K it is higher by 12% (or $12 \times 10^{-8} \Omega$ m). Anderson et al. [43] (data sets 82, 83) reported sudden increase in electrical resistivity values at \sim 1900 K, which they attributed to the evaporation of sample material. There was no evidence of such behavior from the data of Baum et al. [44,45] (data sets 26, 27) and those of Levin et al. [46] (data set 29). Neither was evident from the data of Grube and Knabe [48] (data sets 6-8) which were apparently for specimens that were either porous and/or less pure.

There are only three data sets on the electrical resistivity of chromium in the molten state: by Baum et al. [44,45] (data sets 26, 27) and by Levin et al. [46] (data set 29). As it is mentioned in the last paragraph, the electrical resistivity values of these data for lower temperatures appeared to be questionable. The recommended value for the electrical resistivity of molten chromium at the melting point was obtained by multiplying the recommended value for solid chromium at the melting point by the ratio of the electrical resistivity values (101.5 and 108.1 x $10^{-8} \Omega$ m, respectively, for the solid and the molten states) reported explicitly in the text by Baum et al. [45] (data set 27). For temperatures above the melting point, the recommended values were calculated according to a linear dependence based on data sets 26 and 29.

The recommended values both uncorrected and corrected for thermal expansion of the material are presented in table 1, while only the uncorrected values are

shown in figures 1 and 2 along with the experimental data. The values are applicable to chromium of purity 99.98% or higher; however, those values for temperatures below 100 K are applicable only to chromium having a residual resistivity of 0.0306 x 10^{-8} Ω m. The estimated uncertainty in the recommended values is about $\pm 5\%$ up to 1300 K. The uncertainty increases with temperature at higher temperatures and is estimated to be $\pm 10\%$ immediately below the melting point, and $\pm 15\%$ for the molten state.

From the available data, it appears that the low-temperature resistivity of chromium of lower purity can be obtained by the use of the Mattheissen's rule if the residual resistivity of a specimen does not exceed $\sim 0.2 \times 10^{-8} \Omega m$. Thus, using the recommended values and the Mattheissen's rule, the data for the specimen CrB of Moore et al. [10] (data set 47) would be reproduced to within $\sim \pm 5\%$. For the data of Chiu et al. [22] (data set 46), it was $\sim \pm 10\%$. Generally, this method underestimates the resistivity values. And even though the derivation from Mattheissen's rule can be negative for some dilute chromium alloys, it is not likely to occur for chromium of reasonable purity.

The recommended values uncorrected for thermal expansion given in table 1 can be represented approximately by the following expressions to within $\pm 0.5\%$. 1-90 K:

$$\rho = 0.0306 + 5.756 \times 10^{-7} T^{3 \cdot 23}$$
(11)

90-293 K:

$$\rho = 0.398 - 2.950 \times 10^{-2} T + 5.112 \times 10^{-4} T^2 - 9.218 \times 10^{-7} T^3$$
(12)

293-305 K:

$$\rho = 250.125 - 2.65115 T + 9.68307 \times 10^{-3} T^2 - 1.16108 \times 10^{-5} T^3$$
(13)

305-311 K:

$$\rho = 1.4614467 \times 10^4 - 1.4360559 \times 10^2 T + 4.7073008 \times 10^{-1} T^2 - 5.142874 \times 10^{-4} T^3$$
(14)

312-400 K:

$$\rho = 27.036 - 1.5301 \times 10^{-1}T + 4.5057 \times 10^{-4}T^2 - 3.4505 \times 10^{-7}T^3$$
 (15)
400-1300 K:

 $\rho = 4.457 + 1.3084 \times 10^{-2}T + 4.9046 \times 10^{-5}T^{2} - 3.0031 \times 10^{-8}T^{3} + 8.653 \times 10^{-12}T^{4}$ (16)

1300-2133 K:

$$\rho = -49.515 + 1.11856 \times 10^{-1} T - 2.3954 \times 10^{-5} T^2 + 3.4937 \times 10^{-9} T^3$$
(17)

(18)

2133-2300 K:

 $\rho = 14.54 + 0.050 \text{ T}$

It should be emphasized that these expressions do not necessarily suggest any theoretical justification, and should be treated, most appropriately, as numerical aids only. It should also be understood that giving these expressions does not imply a recommendation for the temperature derivative of the electrical resistivity.

S. (16)

| T | ρ |) | T | | ρ |
|-------|-------------|-----------|------|-------------------------|------------------------------------|
| | uncorrected | corrected | _ | uncorrected | corrected |
| 1 | 0.0306 | 0.0306 | 316 | 12.785 | 12.786 |
| 4 | 0.0307 | 0.0307 | 320 | 12.905 | 12.907 |
| 7 | 0.0309 | 0.0309 | 350 | 13.888 | 13.891 |
| 10 | 0.0316 | 0.0316 | 400 | 15.84 | 15.86 |
| 15 | 0.0342 | 0.0342 | 500 | 20.05 | 20.08 |
| 20 | 0.0398 | 0.0398 | 600 | 24.60 | 24.66 |
| 25 | 0.0495 | 0.0495 | 700 | 29.43 | 29.53 |
| 30 | 0.0646 | 0.0645 | 800 | 34.48 | 34.64 |
| 35 | 0.0865 | 0.0864 | 900 | 39.75 | 39.98 |
| 40 | 0.117 | 0.117 | 1000 | 45.21 | 45.52 |
| 50 | 0.207 | 0.207 | 1100 | 50.89 | 51.30 |
| 60 | 0.349 | 0.349 | 1200 | 56.84 | 57.37 |
| 70 | 0.555 | 0.554 | 1300 | 63.09 _b | 63.78 _b |
| 80 | 0.838 | 0.837 | 1400 | 69.72 ^b | 70.56 b |
| 90 | 1.212 | 1.21 | 1500 | 76.16 | 77.18 |
| 100 | 1.64 | 1.64 | 1600 | 82.44 ^b | 83.68 ^h |
| 150 | 4.36 | 4.36 | 1700 | 88.58 | 90.05 |
| 200 | 7.57 | 7.57 | 1800 | 94.59 | 96. 3 3 ⁵ |
| 250 | 10.57 | 10.57 | 1900 | 100.5 ^D | 102.5 ^D |
| 273 | 11.69 | 11.69 | 2000 | 106.3 | 108.7 |
| 293 | 12.45 | 12.45 | 2100 | $112.1_{\rm b}^{\rm b}$ | 114.8 ^b |
| 300 | 12.650 | 12.650 | 2133 | <u>114.0'(s)</u> | <u>116.8 (s)</u> |
| 306 | 12.760 | 12.761 | 2133 | 121.4 ^b (l) | 124.4 ^b (l) |
| 308 | 12.779 | 12.780 | 2200 | 124.8 ^D | 127.8 ^b |
| 309 | 12.779 | 12.780 | 2300 | 129.8 | 132.8 |
| 310 | 12.769 | 12.770 | | | |
| 311 | 12.739 | 12.740 | | | |
| 311.7 | 12.670 | 12.671 | | | |
| 312 | 12.673 | 12.674 | | | |
| 314 | 12.728 | 12.729 | | | |

TABLE 1. RECOMMENDED VALUES FOR THE ELECTRICAL RESISTIVITY OF CHROMIUM^a

[Temperature, T, K; Electrical Resistivity, ρ , $10^{-8} \Omega$ m]

^a The values are for chromium of purity 99.98% or higher, but those below 100 K are applicable only to chromium having a residual resistivity of 0.0306 x $10^{-8} \Omega$ m. The columns headed uncorrected and corrected refer to values uncorrected and corrected for thermal expansion, respectively. Solid line separating tabular values indicates solid to liquid state transformation.

A7.44

^D Provisional value.







| | | | TABLE | 2. MEA | SUREMENT INFO | RMATION ON THE E | LECTRICAL RESISTIVITY OF CHROMIUM Cr |
|--------------------|------------|--|-------|-----------------|-------------------|-------------------------------------|--|
| Deta Set No. | Ref. | Author (s) | Year | Me thod Used | Temp. Range, K | Name and Spectmen Designation | Composition (weight percent), Specifications and Remarks |
| * | 49 | McLennan, J.C. and Niven, C.D. | 1927 | œ | 2.4-290 | Unaged-I | Trace of Cu; strip sample obtained from General Electric Co. of England; electrolytically deposited sheet ground down to 3.81 cm (1.5 in.) long and 0.475 cm (0.187 in.) thick; unannealed; data un- corrected for thermal expansion. |
| 5* | 49 | McLennan, J.C. and Niven, C.D. | 1927 | £ | 2.2-290 | Unaged-11 | Trace of Cu; strip sample; material obtained from General Electric Co. of England; electrolytically deposited sheet dissolved in acid with aid of electrical potential; unannealed; data uncorrected for thermal expansion. |
| ŧ. | 49 | McLennan, J.C. and Niven, C.D. | 1927 | £ | 20.6-292 | Aged-1 | Similar to the above specimen; annealed for 1 h at comparatively low temperature, cooled to room temperature, annealed for 2 h at much higher temperature; data uncorrected for thermal expansion. |
| 4 | 50 | McLennan, J.C., Niven, C.D., and Wilheim, J.O. | 1928 | 8 | 2.3-293 | | The above specimen with measurements extended to lower temperatures (there is an apparent discrepancy between values at 80 K between data set and the above). |
| * 5 | 48 | Grube, G. and Knabe, R. | 1936 | ¥ | 373-1673 | | "Pure Cr." |
| ę | 87 | Grube, G. and Knabe, R. | 1936 | ¥ | 293-2073 | | Electrolytic Cr, sintered in H ₂ atmosphere at 16/3 K; density 6.95 x 10 ³ kg cm ⁻³ . |
| * | 48 | Grube, G. and Knabe, R. | 1936 | × | 1643-1973 | £ | Electrolytic Cr, remeited and measured in an Ar atmosphere. |
| * | 48 | Grube, G. and Knabe, R. | 1936 | × | 1643-1933 | £ | The above specimen measured with decreasing temperature. |
| * | 48 | Grube, G. and Knabe, R. | 1936 | ~ | 1553-1973 | υ | Electrolytical Cr, remelted and measured in an Ar atmosphere. |
| 10* | 6 4 | Grube, G. and Knabe, R. | 1936 | ¥ | 1563-1953 | υ | The above specimen measured with decreasing temperature. |
| 11* | 15 | Potter, H.H. | 1941 | ^ | 87-1064 | | "99.99" pure; 1 cm long; annealed at 873 K. |
| 12 | 21 | Potter, H.H. | 1941 | > | 87-941 | | Similar to the above; outgassed just below the melting point by electron bombardment. |
| 13* | 14 | Harper, A.F.A., Kemp, W.R.G., Klemens, P.G., Tainsh, R.J., and Mhite, G.K. | 1957 | U | 4.2 | Sample I | 99.998 pure; supplied by Dr. H.L. Wain of the Aeronautical Res. Lab., Commonwealth Dept. of Supply; 3 mm in diam and 8 cm long; cold worked; temperature 4.2 K assumed. |
| 14* | 1 | Harper, A.F.A., et al. | 1957 | U | 4.2 | Sample 2 | The above specimen annealed in vacuum at 1323 K for 4 h. |
| * Not | shown | in figure. | | | | | |

| Ret a | Ref. | Author (s) | Year | Me thod Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------|------|--|------|-----------------|------------------|-------------------------------------|--|
| 15* | 14 | Harper, A.F.A., Kemp, W.R.G., Klemens, P.G., Tainsh, R.J., and White, G.K. | 1957 | U | 4.2 | Sample 3 | Similar to the above; partially recrystallized after cold worked. |
| 16* | 14 | Harper, A.F.A., et al. | 1957 | U | 4.2 | Sample 4 | The above specimen; annealed. |
| 17 | 14 | Harper, A.F.A., et al. | 1957 | ც | 4.2-320 | Sample 5 | Similar to the above; cold worked and fully recrystallized. |
| 18* | 52 | De Morton, M.E. | 1958 | | 200-344 | | 0.013 0 ₂ , 0.0015 C, 0.0005 Al, Fe, N ₂ and Si each, 0.00027 H ₂ (3N1/ 100 gm), 0.0002 Cu, Mg, and Pb each, and 0.00001 Ag; metallic impuri- ties spectrographically determined; 0.073 cm diam and 20.7 rm long; arc-melted electrolytic CT ingot 1.5 in. diam; extruded to 0.5 in. diam; swaged to 0.2 in. diam; drawn at 573 K to 0.027 in. diam; given a 3X reduction at 423 K; total reduction 98X. |
| 19* | 52 | De Morton, M.E. | 1958 | | 200-346 | | The above specimen annealed at 973 K for 15 min. under a vacuum of 2×10^{-4} wmHg; "completely recrystallized". |
| 20* | 23 | Nevmann, M.M. and Stevens, K.W.H. | 1959 | ۲ | 94-390 | | Spectrographically standardized chromium supplied by Johnson and Matthey Co.; contains dissolved oxygen; 2 cm long; machined; sealed in evacuated quartz tube and annealed at 1200 K for 1 month. |
| 21* | 54 | Sabine, T.M. and Svenson, A.C. | 1968 | Ð | 301-328 | | 0.024 0 ₂ and 0.015 N ₂ ; supplied by Aeronautic Res. Lab., Meltourne; hot extruded (1373 K); 0.5 in. in diam and 3 in. long; measured with an AC bridge at 50 Hz; error of measurement 13. |
| 22* | 54 | Sabine, T.M. and Svenson, A.C. | 1968 | ٩ | 291-328 | | Similar to the above, annealed at 1373 K. |
| 23# | 54 | Sabine, T.M. and Svenson, A.C. | 1968 | Q | 289-328 | | Similar to the above, annealed at 1673 K; fine grained. |
| 24* | 54 | Sabine, T.M. and Svenson, A.C. | 1968 | Q | 289-328 | | Similar to the above, annealed at 1673 K; course grained; grain diam 0.25 in. approximately. |
| 25* | 55 | Hamaguchi, Y. and Kunitomi, N. | 1964 | | 295-810 | | 99.9 pure; cut by diamond saw; measured in vacuum. |
| 26 | 44 | Baum, B.A., Cel'd, P.V., and Sachil'nikov, S.I. | 1964 | × | 300-2194 | | 99.98 pure. |
| 27 | 45 | Baum, B.A., Gel'd, P.V., and Sachil'nikov, S.I. | 1963 | æ | 1673-2113 | | >99.98 pure (specimen appears to be the same as the above);resistivity values at melting point (reported at 2113 K approximately) from text. |
| * Not | hown | in figure. | | | | | |

| Pata Set a | Ref. No. | Author (s) | Year | Me thod Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---------------------|-------------|--|------|-----------------|-------------------|-------------------------------------|--|
| 28# | 56 | Pavars, I.A., Baum, B.A., and Gel'd, P.V. | 1969 | æ | 2013 | | 99.98 pure, doubly refined electrolytic chromium; melted in a fusion induction furnace in an argon atmosphere of 500 mmMg. |
| 29 | 46 | Levin, E.S., Gel'd, P.V., and Ayushina, G.D. | 1973 | æ | 1084-2261 | | 99.98 pure, doubly refined electrolytic. |
| 30# | 57 | Levin, E.S. | 1971 | ĸ | £791 | | 99.98 pure, doubly refined. |
| 31* | 58 | Fine, M.E., Greiner, E.S., and Ellis, W.C. | 1951 | × | 78-401 | | 99.8 pure; prepared by cold pressing sintered electrolytic powder compact; annealed at 1673 K in purified helium. |
| 32* | 85 | Fine, M.E., et al. | 1951 | < | 275-377 | | 99.998 pure, from electrochemical analysis by E.K. Jaycox, no Fe or Ni detected; electroformed from an aqueous solution by R.A. Ehrhardt and G. Brittrich, using the method of Brennar, Burhead and Jennings, NBS J. of Res., <u>40</u> , 31, (1948); vacuum annealed at 1273 K with speci- men packed in chromium powder. |
| 33 | 38 | Mitsui, T. and Tomizuka, C.T. | 1965 | K | 243-331 | | 0.08 N and 0.03 O, others not detectable spectrographically; supplied by Prof. R. Street of Monash Univ., Melbourne; 0.5 mm vide, 0.5 mm thick and 58 mm long approximately; manufactured from ARL chromium ingot; ground and formed; annealed and recrystallized at 1523 K for 2 h; resistivity values calculated from reported $\rho(T)/\rho(273 \text{ K})$ and reported $\rho(273 \text{ K}) = 12.7 \times 10^{-6} \Omega m$. |
| 34* | 38 | Mitsui, T. and Tomízuka, C.T. | 1965 | V | 243-322 | | The above measured with decreasing temperature. |
| 35* | 38 | Mitsui, T. and Tomizuka, C.T. | c961 | ~ | 243-330 | | The above measured under a pressure of 0.98 kbar. |
| 36# | 99 | Mitsui, T. and Tomizuka, C.T. | 1965 | × | 243-326 | | The above with decreasing temperature. |
| 37* | 38 | Mitsui, T. and Tomizuka, C.T. | 1965 | × | 243-331 | | The above measured under a pressure of 1.96 kbar. |
| 38* | 38 | Mitsui, T. and Tomizuka, C.T. | 1965 | 4 | 243-329 | | The above with decreasing temperature. |
| 39# | 38 | Mitsui, T. and Tomizuka, C.T. | 1965 | × | 243-331 | | The above measured under a pressure of 2.94 kbar. |
| * 0 * | 38 | Mitsui, T. and Tomizuka, C.T. | 1965 | × | 243-326 | | The above measured under a pressure of 5.30 kbar. |
| * Not | shown | in figure. | | 1 | | | |

| Bata Set a | Ref. | Author (s) | Year | Method Úseď | Temp . Range , K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---------------|-----------|--|------|----------------|---------------------|-------------------------------------|---|
| 41* | 8 | Mitsui, T. and Tomizuka, C.T. | 1965 | v | 243-326 | | The above with decreasing temperature. |
| 424 | 8 | Mitsui, T. and Tomizuka, C.T. | 1965 | < | 243-325 | | The above measured under a pressure of 7.16 kbar. |
| 434 | 8 | Mitsui, T. and Tomizuka, C.T. | 1965 | ۲ | 243-326 | | The above measured under a pressure of 7.85 kbar. |
| 4 | 29 | Barykin, B.M., Gordon, V.G., Levinov, B.M. Rekov, A.I., and Spiridonov, E.G. | 1974 | > | 1124-1938 | | 99.9 ⁺ pure chromium powder; average particle size 5-10 μ m; pressed and sintered at 1973 K; density 7.0 g cm ⁻³ ; porosity 1.5%. |
| 45# | 59 | Barykin, B.M., et al. | | ^ | 1120-1976 | | Similar to the above. |
| 46 | 22 | Chiu, C.H., Jericho, N.M., and March, R.H. | 1971 | > | 5.1-313 | | 0.0012 02 and Fe each, 0.0010 S1, 0.00009 N2, 0.00003 A1, Ca and N1 each, 0.00002 H2 and 0.00001 Cu, Mg, and Mn each $(at.\chi)$; " 10^{-2} cm^2 dlameter," and 5 cm long; spark machined; measurement error 2 χ . |
| 47* | 10 | Moore, J.P., William, R.K., and McElroy, D.L. | 1968 | ~ | 80-400 | CrB | 99.98 ⁺ pure; 0.0060 C, 0.0028 N, <0.0020 Ga, 0.0009 H, 0.0008 Mo, 0.0006 0, 0.0005 x, s, and Si each, 0.0004 K, 0.0003 Co, Fe, and U each, <0.0003 Pt, <0.0002 Sr and Zn each, 0.0001 B, <0.0001 Hg, Pd, Rn, Ru, Sb, Te, T1, U, W, and Zr each, <0.00008 Cu and Pb each, 0.00006 Ca, <0.00005 Ag and Ba each, <0.00004 Bi, 0.00001 Mg, Li, and P each (at.1); content of C by combustion analysis, H, N, and 0 by vacuum fusion analysis, and drop-cast into a rod of 1.6 cm diam and into a disc-shaped inget and drop-cast into a rod of 1.6 cm diam and 15 cm long; machined to 0.96 cm in diam and 7.7 cm in length; density 7.15 g cm ³ ; grain diam 440 to 840 µm; $p(273 K)/p(4.2 K) = 58; mea-surement error ±0.38%; smoothed values from table.$ |
| *8* | 10 | Moore, J.P., et al. | 1968 | ۲ | 310-315 | CrB | The above in the vicinity of the Néel temperature. |
| *65 | 10 | Moore, J.P., et al. | 1968 | • | 307-320 | CrB | The above measured with a temperature gradient of 0.014 k m $^{-1}$. |
| | | | | | | | |
| k Kot | shown | in figure. | | ļ | | | |
1100 K for 4 days and 1200 K for 1 day; p(273 K)/p(4.2 K) = 380; specimen immersed in oil bath maintained to with 1 x 10²³ K of desired temperature; measured with an ac (7 Hz) bridge with an absolute accuracy of 0.2%, and a precision of 0.03%; smoothed values from curve, which is reported to be based on 68 data points and to deviate 0.00004 K and Nb each, <0.00004 B1, <0.00003 Co, <0.00002 Ge, In, and Na each, and <0.00001 Li and Rn each (at.%); same methods of analysis diam and 60 cm long (by BMI); machined to a rod of 0.96 cm diam and 7.7 cm long; density 7.19 g cm⁻³; average grain diam 63 µm; p(273 K)/p(4.2 K) = 280; measurement error ± 0.38 %; smoothed values from table. The above measured in a thermal conductivity apparatus, with tempera-The above specimen on loan from Oak Ridge National Lab.; annealed at The above specimen measured during a thermal conductivity experiment with temperature difference along specimen less than 0.25 K. The above specimen measured during a thermal conductivity experiment above specimen measured during a thermal conductivity experiment 99.98⁺ pure; 0.0070 C, 0.0030 Fe, <0.0020 Au and Mg each, 0.0015 S, 0.0014 0, 0.0010 Mn, <0.0010 Pt, 0.0006 Ca, 0.0005 H and Si each, 0.0003 B, N and U each, 0.0002 Ba, Cu, and Pb each, <0.0002 Ta, 0.0001 Ag and As each, <0.0001 Hg, P, Pd, Ru, Sb, Sn, Te, Tl, U, W, and Zr each, <0.0008 Cd, 0.00005 Ti, <0.00005 Mo, Ni, and Sr each, acket after cleaned and compacted; hot extruded to a rod of 1.6 cm from the measured values by amounts less than the precision of the as above; crystals supplied by Chromalloy Corp.; sealed in vacuum Composition (weight percent), Specifications and Remarks The above measured with a temperature gradient of 0.014 K m^{-1} . with temperature difference along specimen less than 0.5 K. with temperature difference along specimen less than 1.0 K. The above in the vicinity of the Néel temperature. ture difference along specimen less than 0.01 K. ¥. The above after being cooled from 320 K. х. The above after being cooled from 320 K. The above after being cooled from 320 The above after being cooled from 320 neasurements. The Designation Specimen Name and CrA CrA CrA Range, K 308-320 301-318 80-400 307-320 300-319 301-318 301-315 302-319 Temp. 318 301 301 302 Method Used × Δ < ~ Δ Δ ۵ ρ ۵ ρ Þ Year 1968 1970 1970 1970 1970 1970 1968 1968 1970 1970 1970 1970 TABLE 2. Moore, J.P., et al. Moore, J.P. William, R.K., and McElroy, D.L. Moore, J.P., et al. and and and Laubitz, M.J. and Laubitz, M.J. and Laubitz, M.J. and Laubitz, M.J. and and Laubitz, M.J. and Author(s) Laubitz, M.J. Laubitz, M.J. Matsumura, T. Matsumura, T. Matsumura, T. Laubitz, M.J. Laubitz, M.J. Matsumura, T. Matsumura, T. Matsumura, T. Matsumura, T. Matsumura, T. Matsumura, T. Raf. ŝ 2 2 2 • ~ Data ž ş, 51* 52* 53# \$ Ż 55# 56# 57* \$ **2**6 3 **#**19

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* Not shown in figure.

(continued) 5 MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF CHROMIUM

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| s it a | 19 19 | Author (s) | Year | Me thod Vsed | Temp. Rărge, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|------------|----------|---|------|-----------------|-------------------|-------------------------------------|---|
| 5 | 34 | Moore, J.P., Williame, R.K., and Graves, R.S. | 1977 | < | 293 - 1008 | CrA' | Same sample material as the above; average grain diam 50 µm; P(273 K) P(4.2 K) = 280 - 380, depending on thermal cycling; measurement error ±0.38%; corrected for thermal expansion. |
| *. *. | ž | Moore, J.P., et al. | 1977 | ¥ | 300-320 | CrA' | The above in the vicinity of the Néel temperature; corrected for thermal expansion. |
| 4 | ₹. | Moore, J.P., et al. | 1977 | • | 371-1172 | CrA | From the same stock as the above; thermally cycled during brazing of specimen to heater and nickel heat sink; $p(273 \text{ K})/p(4.2 \text{ K}) = 380$; corrected for thermal expansion. |
| ν | 34 | Moore, J.P., et al. | 1977 | ~ | 518-1319 | Cr B | Same specimen material as for Data Set 47; density 7.19 g cm ⁻¹ ; grain size 400 to 800 µm; arc-cast, $\rho(273 \text{ K})/\rho(4.2 \text{ K}) = 58;$ specimen found to have a hairline casting void along its axis, causing approximately 1% change in the measured values; corrected for thermal expansion. |
| * • | 9 | Söchtig, H. | 1940 | | 79-319 | Cr.I | From Dr. Kroll of Luxenburg; cut from a rolled plate; approximate dimensions: 0.12 cm thick, 0.21 cm wide and 1.37 cm long; resistivit values calculated from reported resistances and reported p(273 K) = $19.7 \times 10^{-6} \Omega \text{ m}$. |
| * | 3 | Söchtig, H. | 1940 | | 20.8-373 | Cr I I | Electrolytic chromium; approximate dimensions: 0.21 cm wide, 0.23 cn thick, and 0.58 cm long; resistivity values calculated from reported resistances and reported $p(273 \text{ K}) = 21.1 \times 10^{-8} \text{ Am}$. |
| * | 61 | Meaden, G.T., Rao, K.V., and Loo, H.Y. | 1969 | | 278-323 | | 99.999 pure; 0.0010 C, 0.0009 O ₁ , 0.0003 Ca, 0.0002 Fe, 0.0001 Al, Cu and Mg each, and 0.0008 Hz; residual resistance ratio 178. |
| * 6 | 11 | Meaden, G.T. and Sze, N.H. | 1969 | | 301-317 | | 99.999 pure; 0.0010 C, 0.0008 0, 0.0003 Ca and N ₂ each, 0.0002 Fe, 0.0001 AI, Cu, and Ng each, and 0.00008 Hz; cast fodde chromium machined to 3.8 mm in diam and 65 mm in length; unannealed; $\rho(295 \text{ K})/\rho(4.2 \text{ K}) = 178$; measured with increasing temperature (specimen is apparently the same as the above). |
| * | 11 | Meaden, G.T. and Sze, N.H. | 6961 | | 300-318 | | The above specimen measured with decreasing temperature. |
| * | 12 | Meaden, G.T., Rao, K.V., and Loo, H.Y. | 1969 | | 100-145 | | 99.999 pure; 0.0010 C, 0.0008 0_2 , 0.0003 Cs, 0.0002 Fe, 0.0001 Al, C and Mg each; residual resistivity ratio 178 (specimen is apparently the same as the above). |
| 5 * | ព | Meaden, C.T. and Sze, N.H. | 1969 | | 101-140 | Cr-0 | 99.999 pure; unannealed; grain diam 0.25 mm; residual resistivity ratio 178 (specimen is apparently the same as the above). |
| | 13 | Meaden, G.T. and Sze, N.H. | 1969 | | 116-124 | Cr-0 | The above in the vicinity of the spin-filp transition. |

| | | TAB | LE 2. | MEASUREMEN | IT INFORMATIO | N ON THE ELECTRI | CAL RESISTIVITY OF CHROMIUM Cr (continued) |
|----------|-------|--|--------------|----------------|------------------|-------------------------------------|---|
| Ret Bata | Ref. | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
| 74.* | 13 | Meaden, G.T. and Sze, N.H. | 1969 | | 101-140 | Cr-1 | Similar to the above except annealed at 1473 K for 1 h. |
| 15* | 13 | Meaden, G.T. and Sze, N.H. | 1969 | | 116-125 | Cr-1 | The above in the vicinity of the spin-flip transition. |
| 76* | 13 | Meaden, G.T. and Sze, N.H. | 1969 | | 101-140 | Cr-50 | Similar to the above except annealed for 75 h at temperatures above 1273 K, 50 h of which is at 1473 K; grain diam 2 to 4 mm; grain orien- tation is random as determined by x-ray Laue photography; residual resistivity ratio 295. |
| *11 | 13 | Meaden, G.T. and Sze, N.H. | 1969 | | 117-125 | Cr-50 | The above in the vicinity of the spin-flip transition (discrepancies between these two data sets are due to graph-reading errors). |
| 78* | 28 | Meaden, G.T., Rao, K.V., and Tee, K.T. | 1970 | | 202-329 | | Pure chromium sample; annealed in vacuum $(10^{-6}$ Torr) for 75 h above 1273 K of which 50 h is at 1473 K; grain diam 2 to 4 mm; residual resistivity ratio 295 (specimen is apparently the same as the above). |
| 61 | 51 | Goff, J.F. | 1970 | × | 2.4-343 | Cr I I | 99.92 pure; 0.005 Fe, 0.004 Mn, 0.003 Cu, 0.002 Mg, and balance mostly S, P, N1 and Mn; electrolytic; meited with argon arc, cast in oxygen-free copper boat; annealed twice at 1173 K for 24 h; ground to approx-fmate dimensions of 4 mm wide, 4 mm thick and 50 mm long; polycrystalline; $p(297 \text{ K})/p(4 \text{ K}) = 88$; average residual resistivity 0.145 x $10^{-6} \Omega m$; measurement error 13. |
| 80* | 15, | Goff, J.F. Goff, J.F. | 1970 1968 | ۲ | 1.2-286 | CrI | Similar to the above except $p(297 \text{ K})/p(4 \text{ K}) = 72$ and average residual resistivity (1.2 K to 12.9 K) = 0.1834 x 10^{-8} Rm . |
| 81* | 62 | Moore, J.P., Williams, R.K., and McElroy, D.L. | 1969 | V | 90-360 | | The above specimen; p(296 K)/p(4.2 K) = 70.5; smoothed values from table. |
| 83 | 64 | Anderson, J.M., Stewart, A.D., and Ramsay, I. | 1970 | ۲ | 330-1973 | | Single crystal produced by the iodide process; supplied by Material Research Corp.; 0.0025 interstitial impurities and 0.0015 substitutional impurities, quoted by manufacturers; 1 mm thick, 1 mm wide and 5 mm long; cut by a combination of diamond sav, rpark planning and electropolishing techniques; measurement done in a high purity hydrogen atmosphere; reported errors in resistivity value 0.002%, and in temperature 0.2%; values corrected for thermal expansion using expansion data of B.N. Vasyutinskii, G.N. Katurazov and G.N. Finkel, Soviet PhysPhys. Met. Metallog., <u>12</u> , 141 (1961); rapid increase of resistivity above 1730 K was reported to be due to evaporation of material. |
| 83 | 64 | Anderson, J.M., et al. | 1970 | ۲ | 391-1905 | | Similar to the above, except supplied by Koch-Light Lab. and containing 0.0021 interstitial and 0.0005 substitutional impurities. |
| 94 | 64 | Anderson, J.M., et al. | 1970 | × | 1272-1724 | | "Crystal 3"; no specimen detail reported; measured with decreasing temperature. |
| Not | shown | in figure. | | l | | | |

| Data Set | Ref. | Author (s) | Year | Method Nised | Temp. Rance K | Name and Specimen | Composition (weight percent), Specifications and Remarks |
|-------------|-------------------|---|--------------|-----------------|------------------|----------------------|--|
| 85# | 3 | Anderson, J.M., Stewart, A.D., and Ramsay, I. | 1970 | V | 1482-1740 | Designation | The above specimen; measured with increasing temperature. |
| 86* | 64 | Anderson, J.M., et al. | 1970 | ¥ | 1469-1693 | | The above specimen; measured with decreasing temperature again. |
| 87 | 36 | Anderson, J.M., Stewart, A.D., and Ramsay, I. | 1972 | ۲ | 285-324 | | 0.0012 02 and Fe each, 0.0010 Si, 0.00009 N ₂ , 0.00002 H ₂ , <0.000001 C and 0.0002 others (at. χ); single crystal prepared from Koch-Light crystalline, cut with diamond saw, spark planned and electropolished; 1 mm thick, 1 mm wide and 7 mm long; specimen axis parallel to the [100] direction; annealed at 1970 K for 3 h in hydrogen; T _N 311.5 K. |
| 88* | 36 | Anderson, J.M., et al. | 1972 | ¥ | 282-324 | | The above specimen deformed at a strain rate of 5 x 10^{-5} s^{-1} ; T_N 309 K. |
| #68 | 36 | Anderson, J.M., et al, | 1972 | ¥ | 11 | | 0.03 02, 0.02 Hz, 0.0030 C and 0.0010 Nz (at.X); polycrystal from vacuum melted ingot; average grain size 1 mm. |
| *06 | 63 | Marcinkowski, M.J. and Lipsitt, H.A. | 1961 | | 199-414 | | Pure; plastically deformed: 96% reduction in area at 623 K. |
| \$16 | 63 | Marcinkowski, M.J. and Lipsitt, H.A. | 1961 | | 283-323 | | The above specimen in the vicinity of the Néel temperature. |
| 92 | 63 | Marcinkowski, M.J. and Lipsitt, H.A. | 1961 | | 196-425 | | The above specimen recrystallized by annealing at 1323 K for 1/2 h. |
| 93* | 63 | Marcinkowski, M.J. and Lipsitt, H.A. | 1961 | | 284-323 | | The above specimen in the vicinity of the Néel temperature. |
| 446 | 17 18 | Arajs, 'and Colvin, R.V., and Marcinkowski, M.J. Calvin, R.V. and Arajs, S. | 1962 1962 | × | 298-315 | | 0.055 02 and <0.001 N2; single crystal; 0.235 cm thick, 0.254 cm wide and 0.900 cm long; long axis of specimen aligned to within 1 degree of the [100] direction; measured at temperatures in the order: 297.4, 305.3, 306.1, 307.2, 313.5, 314.5, 312.4, 311.4, 310.3, 308.8, 309.5, and 309.6 K. |
| 95* | 17 . 18 | Arajs, S., et al. | 1962 | × | 310-328 | | The above specimen measured after being left overnight at 309.6 K; measurements between 309.6 K and 312.7 K were done over a period of 8 h, changing temperature slowly; the rest of the data points were obtained the following day. |
| 96 * | 17, 18 | Arajs, S., et al. | 1962 | × | 312 | | The above specimen, cooled; "leaving the crystal at this temperature overnight did not change the value of the resistivity". |
| *16 | 17, 18 | Arajs, S., et al. | 1962 | ¥ | 78 | | The above specimen; heated to 373 K and cooled rapidly to 78 K, and kept at 78 K for two days. |
| 98 # | 17. | Arajs, S., et al. | 1962 | ۷ | 78-140 | | The above specimen. |
| *66 | 17, | Arajs, S., et al. | 1962 | × | 4.2.330 | | The above specimen, cooled to 78 K, left overnight and cooled to 4.2 K; measurements in the temperature ranges, 4 to 115 K, 130 to 155 K, |
| * Not | ahown | in figura. | | Ī | | | 155 to 215 K, and 215 to 295 K were done in successive days. |

| ket a | т. жо. | Auchor (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent). Specifications and Remarks |
|-------|-----------|--|------|----------------|-------------------|-------------------------------------|---|
| 8 | 19 | Arajs, S. and Dunayre, G.R. | 1965 | ~ | 4-297 | | 0.0013 0, 0.0010 C and Si each, 0.0001 Ca, Mg, N, and Ni each, and 0.00005 H, others not detected; contents of 0, H, and N determined by vacuum fusion, of C by combustion, and the rest by spectroscopic methods; arc-melted polycrystalline ingest $0.7 \times 1.6 \times 8.0 \mathrm{cm}$ supplied by Chromailoy Corp.; cut by surface grinding machine to $0.478 \pm 0.001 \mathrm{cm}$ thick, $0.476 \pm 0.001 \mathrm{cm}$ viacums $10, 0.053 \mathrm{K}/10.13 \pm 0.001 \mathrm{cm}$ this ingest $0.7 \times 1.6 \times 8.0 \mathrm{cm}$ supplied by Chromailoy Corp.; cut by surface grinding machine to $0.478 \pm 0.001 \mathrm{cm}$ thick. $7_{\rm N}$ 313.0 $4.0.7 \mathrm{K}/2 \mathrm{K}/10.4.2 \mathrm{K}/10.1 \mathrm{cm}$ this curve does not repeated to rest the measurement B h; specimen was left at 290.5 K for 15 h without detectable change in resistivity (due to small size of graph, data points below 80 K are selected values; hence this curve does not represent all the measurements reported by the such to rest. |
| *101 | 19 | Arajs, S. and Dunmyre, G.R. | 1965 | ¥ | 300-318 | | The above specimen in the vicinity of the Néel temperature; duration of measurement 8 h. |
| 102* | 20 | Araja, S., DeYoung, T.F., and Anderson, E.E. | 1970 | ~ | 9-1035 | | From the same stock as the above. |
| 103 | 24 | Cox, J.E. and Lucke, W.N. | 1967 | t | 299-1281 | | 99.999 iodide chromium; melted 15 to 18 times in 2/3 atmosphere of ionization grade; 99.999 pure argon; spark eroded to cylindrical form; centerless-ground to 1/8 in. diam and 2 1/2 in. long; wrapped in molybdenum foil and annealed at 1523 K in 1/2 atmosphere of ionization grade helium; water quenched and etched; measured by a method by Dauphinee, T.M. and Mooser, E., Rev. Sci. Instr., 26, 660, 1955. |
| **01 | 25 | Taylor, M.A. | 1962 | | 17-359 | | 99.99 pure; 0.01 0, \sim 0.0001 N, C, S and Sn each, and <0.0001 others; electrolytic; supplied by the Aeronautical Res. Lab., Melbourne; smoothed values from curve. |
| 105* | 64 | Taylor, M.A. and Smith, C.H.L. | 1962 | v | 20-273 | | 99.99 pure; supplied by the Aeronautical Res. Lab., Melbourne; 1 mm wide, 1 mm thick, and 10 mm long; cut with carborundum slitting wheel; annealed at $1073 \times for 50$ h in vacuum; measurement ertor 1%. |
| 106* | 47 | Powell, R.W. and Tye. R.P. | 1956 | 4 | 94-1707 | | 99.965 pure; <0.01 N and <0.005 0 (as Cr ₂ 0 ₃); electrodeposited chromium 1.28 cm 0.D., 0.63 cm 1.D. and 18.05 cm long; prepared from chromium flakes supplied by Johnson Matthey Co.; enclosed in alwaina tube and heat-treated at 443, 486, 678, 818, 1133, 1327, and 1683 K, with the five last treatments done in vacuum; reductions of 0.010 cm in 0.D. and 1.D. are observed after final treatment; initial density 6.975 x 10^3 kg m^{-3} , after final treatment 7.15 x 10^3 kg m^{-3} . |
| 107* | 47 | Powell, R.W. and Tye, R.P. | 1956 | 4 | 273-333 | | The above in the vicinity of the Néel temperature. |
| #80I | 26 | Muheim, J. and Müller, J. | 1964 | t | 100-339 | | Cylindrical specimen l mus in diam and 50 cm long; measured by a com- pensation method. |

| (06) (1) (15) | Set a Set a | Ref. | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---|----------------|------|---|------|----------------|-------------------|-------------------------------------|---|
| 110 5 Tower, N. E., Gal'A, P. Y. E. 100 0.00 Instantion: p = 45 × 0.00 Not water end of a state of other and Gal'A, P. Y. E. 111 6 Newrer, N. E. 107 A 95-00 Phycrystation: p = 45 × 0.00 Not water and control of the state description: p = 45 × 0.00 Not water and control of the state description in the state, in an vide, in an intervision in the state description in the state description in the state description in the state description in the state control of the state description in the state d | 109* | 23 | DeVries, G. | 1959 | | 165-356 | | Prepared by Prof. Fast, Eindhoven. |
| 11. 6. Warreno, L.C. and Rouce, V.N 97 A 8-400 Dispersion in an end of a manufactural frame that, in which a distribution resonance and in an end of a manufactural frame that in a limit in transfer of resonance and in an end of a manufactural frame and in a frame that in a limit in transfer of resonance and in a manufactural frame and in a frame and in a frame and in a frame and resonance and in a manufactural frame and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and resonance and in a frame and in a frame and in a frame and resonance and in a frame and in a frame and in a frame and in a frame and resonance and in a frame and in a frame and in a frame and in a frame and resonance and in a frame and resonance and in a frame and in a fra | 110* | 65 | Zinowiev, V.E., Krentsis, R.P., and Gel'd, P.V. | 6961 | | 300-1800 | | 0.05 total impurity; residual resistance ratio = 65; values calculated from reported equations: $p = 4.8 \times 10^{-2}$ T, T < 800 K and $p = 4.8 \times 10^{-2}$ T + 3.1 x 10 ⁻⁶ (T-800) ² , T > 800 K. |
| 11 3 Stebler, B. 1970 A 29-344 3995 pure, 0.0002 N; single crystal; 7 m thtick, 8 m vide and restriction fullor structure transmission sequested with increasing temperature; restriction states to in the vicinized for severation sequested with increasing temperature; restriction sequested in sequested with sequested in sequested in sequested i | *111 | 66 | Maystrenko, L.G. and Polovov, V.M. | 1977 | ¥ | 89-400 | | Polycrystalline; appropriate dimensions 1 mm thick, 1 mm wide, and 10-15 cm long; annealed at 1273 K for 24 h in helium; furnace cooled; measurement error ±5%. |
| 113Stehler, B.1970A20-310The above speciaent in the vicinity of the Meil temperature: with increasing temperatures.1163Stehler, B.1970A30-316The above speciaent in the vicinity of the Meil temperature: with increasing temperatures.1133Stehler, B.1970A30-316The above speciaent in the vicinity of the Meil temperature: meanured vicinity interasing temperatures.11637Trego, A.L. and1968277-3200.0022 C, 0.0030 N, 0.0016 0 and 0.0001 N (at.3); lodide Cr supplied for prophosphoric acid; annual L: S on long, cut by spark recond net- top of preasilie temperatures.11637Trego, A.L. and1968277-3200.0022 C, 0.0030 N, 0.0016 0 and 0.0001 N (at.3); lodide Cr supplied for spark recond net- top of preasilie temperatures.11837Trego, A.L. and1968277-3100.002 N (at 0.001 N (at.3); lodide Cr supplied for spark recond net- top of spark recondent net- top of spark resonance of trop of spark recondent | 112 | ;E | Stebler, B. | 1970 | ۲ | 296-344 | | 99.996 pure, 0.0002 N ₂ ; single crystal; 7 mm thick, 8 mm wide and 25 mm long; specimen axis v 8 degrees of arc from the [100] direction; measured with increasing temperature; resistivity values calculated from reported $\Delta \rho / \rho_0$, where ρ_0 is the resistivity at 273.2 K, taken to be 11.687 x $10^{-8} \Omega m$. |
| 114 33 Stehler, B. 1970 A 305-316 The above speciaen in the vicinity of the Néel temperature; measured vith increasing temperature; 115 33 Stehler, B. 1970 A 305-316 The above speciaen in the vicinity of the Néel temperature; measured vith increasing temperature; 116 37 Trege, AL, and 1968 277-320 0.0072 c, 0.0030, 0.0016 0 and 0.0014 (at.7); iodda Cr supplied vited in the vicinity of the Néel temperature; 116 37 Trege, AL, and 1968 277-320 0.0072 c, 0.0030, 0.0016 0 and 0.0014 (at.7); iodda Cr supplied in the vicinity of the Néel temperature; 118 37 Trege, AL, and 1968 272-310 0.0072 c, 0.0030, 0.0016 0 and 0.0014 (at.7); iodda Cr supplied in the vicinity of the Néel temperature; 118 37 Trege, AL, and 1968 272-310 10.9013 dist; 10.011 dist; 10.013 dist; 10.001 dis; 10.001 dist; | 113 | 33 | Stebler, B. | 1970 | V | 287-350 | | The above specimen measured with decreasing temperature. |
| 115 33 Stebler, B. 1970 A 305-316 The above specimen in the vicinity of the Néel temperature: measured with decreasing temperature: 116 37 Trego, A.I. and the stand of the | 114 | 33 | Stebler, B. | 1970 | A | 305-316 | | The above specimen in the vicinity $\mathfrak{o}_{\tilde{\mathbf{i}}}$ the Néel temperature; measured with increasing temperature. |
| 11637Trego, A.L. and Mackintosh, A.R.1968277-3200.0072 C, 0.0030 N, 0.0016 0 and 0.0001 H (at. X); lodide Cr supplied by Otronalizy Corp.; arc matted: single crystal 2 ma square cross saction and 1.5 cm long, cut by spark erosion tech- nique from cross saction and 6 f.i. long ingo; electropolished in orthophosphoric action and and 0.0001 H (at. X); lodide Cr supplied for transing crystal and 0.0001 H (at. X); lodide Cr supplied for the product and 0.0001 H (at. X); lodide Cr supplied for the product and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for the phosphoric action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and 0.0001 H (at. X); lodide Cr supplied for transverse action and | 115 | 33 | Stebler, B. | 1970 | A | 305-316 | | The above specimen in the vicinity of the Néel temperature; measured with decreasing temperature. |
| 11737Trego, A.L. and Mackintosh, A.R.1968272-310The above specimen measured after cooled through the Néel temperature in a longitudinal magnetic field of 55 kG.11837Trego, A.L. and Mackintosh, A.R.1968275-311The above specimen but measured after cooled through the Néel temper- ature in a transverse magnetic field (either in [010] or [100] direc- tion) of 55 kG.11937Trego, A.L. and Mackintosh, A.R.1968270-310The above specimen but measured after cooled through the Néel temper- ature in a longitudinal magnetic field (either in [010] or [100] direc- tion) of 55 kG.11937Trego, A.L. and Mackintosh, A.R.1968270-31012037Trego, A.L. and Mackintosh, A.R.1968270-31012037Trego, A.L. and Mackintosh, A.R.1968270-31312037Trego, A.L. and Mackintosh, A.R.1968270-313 | 116 | 31 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 277-320 | | 0.0072 C, 0.0030 N, 0.0016 O and 0.0001 H (at.X); lodide Cr supplied by Chromalloy Corp.; arc melted and arc zone melted; single crystal 2 mm square cross section and 1.5 cm long, cut by spark erosion technique from 0.5 in. diam and 6 in. long ingot; electropolished in orthophosphoric acid; annealed in vacuum at 1273 K for 50 h; sample length parallel to crystal [001] axis; resistivity values calculated from reported resistance R(T) and R(320 K), with $\rho(320 \text{ K})$ taken to be 12.906 x 10 ⁻⁸ Ω m. |
| 11837Trego, A.L. and Mackintosh, A.R.1968275-311The above specimen but measured after cooled through the Néel temper- tion) of 55 kG.11937Trego, A.L. and Mackintosh, A.R.1968270-310The above specimen, but measured after cooled through the Néel temper- | 117 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 272-310 | | The above specimen measured after cooled through the Néel temperature in a longitudinal magnetic field of 55 kG. |
| 11937Trego, A.L. and1968 $270-310$ The above specimen, but measured after cooled through the Néel temper- ature in a longitudinal magnetic field of 40.5 kG; resistivity value calculated from reported $\Delta\rho/\mu(T_N)$, with $\rho(T_N)$ taken to be 12.70 x $10^{-8} \Omega m$.12037Trego, A.L. and Mackintosh, A.R.1968 $270-313$ 12037Trego, A.L. and Mackintosh, A.R.1968 $270-313$ 12037Trego, A.L. and Mackintosh, A.R.1968 $270-313$ | 118 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 275-311 | | The above specimen but measured after cooled through the Néel temper- ature in a transverse magnetic field (either in [010] or [100] direc- tion) of 55 kG. |
| 120 37 Trego, A.L. and 1968 270-313 The above specimen except strength of magnetic field is 28 kG. Mackintosh, A.R. | 119 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 270-310 | | The above specimen, but measured after cooled through the Néel temperature in a longitudinal magnetic field of 40.5 kG; resistivity value calculated from reported $\Delta\rho/\rho(T_N)$, with $\rho(T_N)$ taken to be 12.70 x 10 ⁻⁸ Ωm . |
| | 120 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 270-313 | | The above specimen except strength of magnetic field is 28 kG. |

| Data | Rof. | | | Method | Temp. | Non ine electron | |
|------|-------------------|---|--------------|--------|----------|------------------|--|
| 2 X | No. | AUCHOT (8) | lear | Used | Range, K | besignation | composition (weight percent), specifications and remarks |
| 121 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 275-307 | | The above specimen except strength of magnetic field is 15.6 kG. |
| 122 | 37 | Trego, A.L. and Mackintosh, A.R | 1968 | | 285-310 | | The above specimen but cooled through the Néel temperature in a transverse magnetic field of 47 kG. |
| 123 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 274-308 | | The above specimen except strength of magnetic field is 40.5 kG. |
| 1-4 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 274-310 | | The above specimen except strength of magnetic field is 28 kG. |
| 125 | 37 | Trego, A.L. and Mackintosh, A.R. | 1968 | | 275-307 | | The above specimen except strength of magnetic field is 15.6 kG. |
| 126 | 67 | Akiba, C. and Mitsui, T. | 1972 | ۲ | 294-320 | | 99.997 pure; iodide chromium supplied by A.D. Mackay Inc.; 0.77 mm thick, 0.7 mm wide and 10 mm long; single crystal, spark cut and chemically polished; specimen axis within ± 3 degrees from the crystalline <100> direction; $R(293 K)/R(4, 2 K) = 630$ without magnetic field cooling; specimen in single magnetic domain state (single q) prepared by heating to 329 K, applying a longitudinal magnetic field of 74 kG, then cooled to 273 K, and magnetic field of 74 kG, then cooled to 273 K, and magnetic field volues state values calculated from reported resistance, and with $\rho(320 K)$ taken to be 12.906 x 10 ⁻⁶ Am. |
| 127 | 67 | Akiba, C. and Mitsui, T. | 1972 | ۷ | 301-320 | | The above specimen except magnetically cooled with a transverse field of 74 kG. |
| 128 | 67 | Semenenko, E.E. and Tutov, V.I. | 1969 | | 1.5-6.8 | | Monocrystalline whisker specimen, $0.10-0.12$ mm in diam and $\circ 8$ mm long; $R(4,2 \text{ K})/R(300 \text{ K}) = 8 \times 10^{-3}$; resistivity values calculated from reported resistance and $\rho(300 \text{ K})$, taken to be $12.650 \times 10^{-6} \Omega \text{ m}$. |
| 129 | 89 | Semenenko, E.E. and Tutov, V.I. | 1972 | | 4.7-329 | | Primary impurity is iron; only resistance as a function of temperature reported; resistivity calculated by assuming $ ho(328.6~{ m K})$ = 13.177 x 10 8 G m. |
| 130 | 68 | Semenenko, E.E. and Tutov, V.I. | 1972 | | 280-330 | | The above specimen in the vicinity of the Néel temperature. |
| 131 | 68 . 74 | Semenenko, E.E. and Tutov, V.I. Semenenko, E.E. | 1972 1966 | | 4.4-16.1 | | Similar to the above; R(1.5 K)/R(300 K) = 8 x 10^{-3} ; resistivity values calculated from reported R/R(300 K) with $\rho(300$ K) taken to be 12.650 x 10^{-6} G.m. |
| 132 | 68 | Semenenko, E.E. and Tutov, V.I. | 1972 | | 1.7-14.8 | | Similar to the above; $R(1.5 \text{ K})/R(300 \text{ K}) = 7.6 \times 10^{-3}$. |
| 133 | 68 | Semenenko, E.E. and Tutov, V.I. | 1972 | | 2.0-7.1 | | Similar to the above; $R(1.5 \text{ K})/R(300 \text{ K}) = 6.8 \times 10^{-3}$. |
| Not | mode | in figure. | | | | | |

| Data Set No. | Ref. | Author (s) | Үеаг | Method Üsed | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--------------------|-------|--|------|----------------|------------------|-------------------------------------|--|
| 134 | 40 | Kostina, T.I., Ekonomova, L.N., and Kondorskii, E.I. | 1970 | | 103-130 | | Single crystal cut by electric spark method; 0.1 mm thick, 0.15 mm wide and 4 mm long; R(293 K)/R(4.2 K) = 500; TN 311 \pm 2 K; longitudinal axis of sample parallel to the [110] direction; resistivity values calculated from reported R/R(77 K), with $\rho(77$ K) taken to be 0.737 x 10 ⁻⁸ Ωm. |
| 135 | 40 | Kostina, T.I., et al. | 1970 | | 285-326 | | The above specimen. |
| 136 | 40 | Kostina, T.I., et al. | 1970 | | 106-131 | | The above specimen after magnetically annealed by an external field in the [100] direction of magnitude 34 kOe. |
| 137 | 40 | Kostina, T.I., et al. | 1970 | | 103-119 | | Similar to the above except external field is in the [110] direction. |
| 138 | 40 | Kostina, T.I., et al. | 1970 | | 121-153 | | Similar to the specimen of data set 134, except longitudinal axis of sample is parallel to the [100] direction. |
| 139 | 40 | Kostina, T.I., et al. | 1970 | | 287-329 | | The above specimen. |
| 140 | 40 | Kostina, T.I., et al. | 1970 | | 101-125 | | The above specimen after magnetically annealed by an external field in the [100] direction of magnitude 34 kOe. |
| 141 | 40 | Kostina, T.I., et al. | 1970 | | 111-133 | | Similar to the above except magnetic field is in the [110] direction. |
| 142 | 41 | Muir, W.B. and Strön-Olsen, J.O. | 1971 | | 76-326 | | Single crystal, 1 mm thick, 1 mm wide and 7 mm long; cut by spark erosion technique from vapor transport grown polycrystal ingot containing many large single crystals, supplied by Battelle Memorial Institute; annealed at 1470 K in argon for 50 h; strain free (found by x-ray technique; specimen axis parallel to the <100° direction; R(300 K)/R(4,2 K) = 350; in single magnetic domain state by cooling from 343 to 273 K in a longtudinal magnetic field of 60 k0e; measuring current parallel to the spin density wave vector Q; resistivit) values calculated from reported R/R(320 K) with $\rho(320 K)$ taken to 12.906 x 10 ⁻⁶ Ω m. |
| 143 | 41 | Muir, W.B. and Ström-Olsen, J.O. | 1971 | | 76-328 | | The above specimen in the multidomain state. |
| 144 | 41 | Muir, W.B. and Ström-Olsen, J.O. | 1791 | | 296-320 | | The above specimen, single domain state, in the vicinity of the Néel temperature; measuring current parallel to Q. |
| 145 | 14 | Muir, W.B. and Ström-Olsen, J.O. | 1791 | | 298-318 | | The above specimen, in the multidomain state after the above measure- ment. |
| 146 | 41 | Muir, W.B. and Ströa-Olsen, J.O. | 1971 | | 300-319 | | The above specimen, magnetically cooled to the single domain state again after the above measurement; measuring current again parallel to Q. |
| Not | shown | in figure. | | | | | |

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| Set No. | Ref. | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|------------|-------------|--|------|----------------|-------------------|-------------------------------------|--|
| 147 | 41 | Muir, W.B. and Ström-Olsen, J.O. | 1971 | | 295-312 | | The above specimen, in the multidomain state after the above measurement. |
| 871 | 41 | Muir, W.B. and Ström-Olsen, J.O. | 1971 | | 299-320 | | The above specimen, in single domain state after cooling from 343 to 273 K in a transverse magnetic field of 60 kOe; measuring current perpendicular to Q. |
| 149 | 41 | Muir, W.B. and Ström-Olsen, J.O. | 1971 | | 299-310 | | The above in the multidomain state. |
| 150 | 69 | Borovik, E.S. and Volotskaya, V.G. | 1959 | | 2.4-78 | | Vacuum distilled chromium; needle shaped; "0.35 mm across" and 8 mm long; "appear to be single crystal;" resistivity value calculated from reported $R/R(273 K)$, with $\rho(273 K)$ taken to be 11.687 x 10^{-6} Ω m. |
| 151 | 0/ | McWhan, D.B. and Rice, T.M. | 1967 | | 4.3-232 | Sample 2 | Battelle Iochrome; single crystal; R(298 K)/R(4.2 K) = 140; measured under a pressure of 26.5 kbar; AgCl used as pressure transmitting medium; resistivity values calculated from reported R/R(l atm. 298 K), with $p(l atm., 298$ K) taken to be 12.319 x 10 ⁻⁶ Ωm . |
| 152 | 70 | McWhan, D.B. and Rice, T.M. | 1967 | | 60-223 | Sample 2 | The above measured under a pressure of 45.7 kbar. |
| [53 | 70 | McWhan, D.B. and Rice, T.M. | 1967 | | 32.5-223 | Sample 2 | The above measured under a pressure of 64.9 kbar; data points below 30 K cannot be resolved from graph, and are not reported here. |
| 154 | 0/ | McWhan, D.B. and Rice, T.M. | 1967 | | 188-276 | Sample 2 | From the same ingot as the above specimen; $R(298 K)/R(4.2 K) = 275$ and 165 before and after pressure experiment respectively; measured under a pressure of 26.3 kbar; AgCl used as pressure transmitting medium; resistivity values calculated by the same method as for the above specimen. |
| 155 | 70 | McWhan, D.B. and Rice, T.M. | 1967 | | 59-262 | Sample 2 | The above measured under a pressure of 45.9 kbar. |
| 156 | 70 | McWhan, D.B. and Rice, T.M. | 1961 | | 70-262 | Sample 2 | The above measured under a pressure of 65.9 kbar. |
| 157 | 27 | Suzuki, T. | 1966 | | 216-331 | | 99.99 pure; electrolytic, supplied by Johnson and Matthey Co.; 0.5 mm thick, 0.5 mm wide and 20 mm long; degassed at 773 K; electropolished in a solution of 90% acetic acid and 10% perchloric acid; resistivity values calculated from reported $[\rho(T) - \rho(300 \text{ K})]/\rho(300 \text{ K})$, with $\rho(300 \text{ K})$ taken to be 12.650 x 10 ⁹ 0 m. |
| 158 | 32 | Ishikawa, Y., Ikeda, S., and Akiba, C. | 1975 | | 299-320 | | 99.997 pure; fodide chromium from A.D. Mackay Inc.; single crystal, 0.7 mm thick, 0.7 mm wide and 10 mm long; specimen axis along [100] direction; resistivity value calculated from reported resistance values and $\rho(370 \text{ K})$, taken to be 12.906 x 10 ⁻⁸ Ω m. |
| Not | shown | in figure. | | | | | |

* Not shown in figure.

value at Néel temperature not reported; measured with increasing temperature at ${}^{\rm AI}$ khr^1; resistivity values calculated from reported resistance ratios and an assumed $\rho(300.23~{\rm K})$ = 12.655 x 10⁻⁸ Ω m; because 0.3 0, <0.002 N and H each by chemical analysis; <0.03 Zn and <0.01 K by spectrographic analysis; polycrystalline specimen; 0.25 in. in diam and 1 in. long; annealed; resistivity values calculated from reported equations: $p = 0.1 + 1.58 \times 10^{-6} T^{3.02}$ for T < 109.5 K, and 310.79 K; resistivity value calculated from reported resistance ratio and an assumed $\rho(300.07 \text{ K}) = 12.651 \times 10^{-6} \Omega \text{ m}.$ 100 h, and water quenched; etched again in HCl to the suitable dimencooled in 24 h; "thermally cycled before measurement;" Ty determined by same method as above 310.77 K; resistivity values calculated from reported resistance ratio and an assumed $\rho(304.15 \text{ K}) = 12.733 \text{ x}$ Swaged rod supplied by P.H. Brace, Westinghouse Electric and Manufaca mai an<mark>harang sa</mark> na na na persebutuh dan tahun dan sebut da evacuated to about 0.1 Torr and encapsulated; annealed at 1250 K for sions; data reported as ratio of ρ to the ρ at the Néel temperature. Similar to the above except approximate dimensions 1 mm thick, 1 mm Similar to the above except approximate dimensions 1 mm thick, 1 mm turing Co., spectroscopic examination by Martin Graban show only a "doubtful trace of magnesium"; resistivity values calculated from reported R(T)/R(273 K) with $\rho(273 \text{ K})$ taken to be 11.687 x 10⁻⁶ Ω m. Specimen material same as for Data Set 100; approximate dimensions wide and 15 mm long, and annealed at 1250 K for 100 h and furnace-0.1 mm thick, 1 mm wide and 20 mm long; spark cut from arc-melted ingot, etched in HCl, placed in silica tube, flushed with helium, cooled in 12 h; T_N determined from a power law fit to $\rho^{-1} \propto d\rho/dT$ wide and 20 mm long, and annealed at 1250 K for 24 h and furnaceof graph reading difficulties, not all data points are included. Composition (weight percent), Specifications and Remarks x⁵ dx THE R. P. LEWIS CO., LANSING MICH. Designation Specimen Name and Cr (2) Cr(1) Cr (3) 300.2-315.0 300.1-313.5 304.2-313.4 Range, K 4-300 193-347 Temp. Method Used 4 × < < Year 1933 1978 1978 1978 1968 Rapp, Ö., Benediktsson, G., Clinard, F.W. and Rapp, Ö., et al. Rapp, Ö., et al. \uthor(s) Arajs, S., and Bridgman, P.W. Aström, H.U., Kempter, C.P. Rao, K.V. Ref. ź 7 31 31 72 31 Data 163* š 159 160 ź 161 162

Cr (continued) MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF CHROMIUM

TABLE 2.

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and

 $\rho = -1.08 + \left[\frac{C}{H0}\right] \times \left[\frac{T}{\theta}\right]^5 \sigma^{\theta/T} \frac{x^5 \, dx}{(e^x - 1)(1 - e^{-x})}, \text{ with } \theta = 357 \text{ K}$

 $C = 1.43 \times 10^{-6}$ (M = atomic weight).

| CHROMIUM |
|---------------|
| 0F |
| RESISTIVITY |
| ELECTRICAL |
| THE |
| NO |
| DATA |
| EXPER IMENTAL |
| TABLE 3. |

Cr.

0.0

[Temperature, T, K; Electrical Resistivity, $\rho,~10^{-8}\,\Omega\,m]$

| T | ٩ | ч | ď | н | ٩ | ч | d | ÷ | ٩ | F | ٩ |
|-----------|-----------------------|------|-------|----------|----------|----------|-----------|----------|-----------|----------|-----------|
| DATA | ser 1* | DATA | SET 6 | DATA SET | 6(cont.) | DATA SET | 7(cont.)* | DATA SET | 8(cont.)* | DATA SET | 9(cont.)* |
| 25.75 | 75.9 | 793 | 14.1 | 1753 | 112.8 | 1773 | 116.9 | 1793 | 120.7 | 1813 | 117.5 |
| 4.2 | 26.2 | 323 | 15.3 | 1763 | 113.8 | 1733 | 117.3 | 1803 | 121.1 | 1823 | 117.9 |
| 20.6 | 26.7 | 373 | 17.5 | 1773 | 114.7 | 1743 | 117.8 | 1813 | 121.6 | 1833 | 118.5 |
| 83 | 29.2 | 423 | 19.7 | 1783 | 115.8 | 1753 | 118.8 | 1823 | 122.0 | 1843 | 119.0 |
| 290 | 43.8 | 473 | 22.1 | 1793 | 117.0 | 1763 | 118.8 | 1833 | 122.5 | 1853 | 119.5 |
| | | 523 | 24.5 | 1803 | 118.2 | 1773 | 119.3 | 1843 | 122.8 | 1863 | 120.1 |
| DATA S | IET 2* | 573 | 26.7 | 1813 | 119.3 | 1783 | 119.8 | 1853 | 123.3 | 1873 | 120.7 |
| | | 623 | 29.4 | 1823 | 119.9 | 1793 | 120.3 | 1863 | 123.8 | 1883 | 121.3 |
| 2.20 | 26.5 | 673 | 32.0 | 1833 | 120.5 | 1803 | 120.7 | 1873 | 124.2 | 1893 | 122.0 |
| 3.01 | 26.6 | 723 | 34.8 | 1843 | 121.1 | 1813 | 121.2 | 1883 | 124.7 | 1903 | 122.7 |
| 4.2 | 26.7 | 773 | 37.6 | 1853 | 121.8 | 1823 | 121.7 | 1893 | 125.1 | 1913 | 123.5 |
| 20.6 | 27.0 | 823 | 40.4 | 1863 | 122.8 | 1833 | 122.1 | 1903 | 125.6 | 1923 | 124.3 |
| 83 | 28.8 | 873 | 43.3 | 1873 | 123.8 | 1843 | 122.6 | 1913 | 126.1 | 1933 | 125.2 |
| 290 | 43.8 | 923 | 46.1 | 1883 | 124.7 | 1853 | 123.0 | 1923 | 126.5 | 1943 | 126.0 |
| | | 973 | 49.0 | 1893 | 125.6 | 1863 | 123.4 | 1933 | 126.8 | 1953 | 126.8 |
| DATA S | 1ET 3* | 1023 | 51.8 | 1903 | 126.6 | 1873 | 123.8 | | | 1963 | 127.6 |
| | | 1073 | 54.9 | 1913 | 127.5 | 1883 | 124.3 | DATA S | SET 9* | 1973 | 128.5 |
| 20.6 | 0.90 | 1123 | 58.5 | 1923 | 128.5 | 1893 | 124.7 | | | | |
| 80 | 2.01 | 1173 | 61.8 | 1933 | 129.5 | 1903 | 125.2 | 1553 | 100.4 | DATA S | ET 10* |
| 292 | 17.2 | 1223 | 65.6 | 1943 | 130.5 | 1913 | 125.6 | 1563 | 101.4 | | |
| | | 1273 | 69.5 | 1953 | 131.5 | 1923 | 126.2 | 1573 | 102.4 | 1563 | 105.1 |
| DATA | SET 4 | 1323 | 73.6 | 1963 | 132.5 | 1933 | 126.8 | 1583 | 103.3 | 1573 | 106.5 |
| | | 1373 | 77.4 | 1973 | 133.5 | 1943 | 127.5 | 1593 | 104.3 | 1583 | 107.5 |
| 2.25 | 0.79 | 1423 | 81.8 | 1983 | 134.5 | 1953 | 128.2 | 1603 | 105.2 | 1593 | 108.5 |
| 4.2 | 0.79 | 1473 | 86.7 | 1993 | 135.7 | 1963 | 129.0 | 1613 | 106.2 | 1603 | 109.4 |
| 20.6 | 0.80 | 1523 | 91.4 | 2003 | 136.9 | 1973 | 129.9 | 1623 | 107.3 | 1613 | 110.4 |
| 80 | 2.01 | 1573 | 96.0 | 2013 | 138.2 | | | 1633 | 107.9 | 1623 | 111.2 |
| 293 | 17.2 | 1583 | 96.9 | 2023 | 139.5 | DATA S | ET 8* | 1643 | 108.5 | 1633 | 112.2 |
| | | 1593 | 97.8 | 2033 | 140.9 | | | 1653 | 109.1 | 1643 | 112.6 |
| DATA | SET S# | 1603 | 98.7 | 2043 | 141.3 | 1643 | 109.0 | 1663 | 109.7 | 1653 | 113.1 |
| | | 1613 | 9.66 | 2053 | 142.7 | 1654 | 110.3 | 1673 | 110.3 | 1663 | 113.6 |
| 373 | 17.501 | 1623 | 100.7 | 2063 | 144.1 | 1663 | 111.7 | 1683 | 110.9 | 1673 | 114.1 |
| 473 | 22.002 | 1633 | 101.6 | 2073 | 145.5 | 1673 | 112.9 | 1693 | 111.4 | 1683 | 114.9 |
| 573 | 26.702 | 1643 | 102.6 | | | 1683 | 114.2 | 1703 | 112.0 | 1693 | 115.4 |
| 673 | 32.000 | 1653 | 103.6 | DATA S | ET 74 | 1693 | 115.6 | 1713 | 112.6 | 1703 | 115.9 |
| 873 | 43,290 | 1663 | 104.5 | | | 1703 | 116.5 | 1723 | 113.1 | 1713 | 116.4 |
| 973 | 48.996 | 1673 | 105.4 | 1643 | 108.3 | 1713 | 117.0 | 1733 | 113.6 | 1723 | 116.8 |
| 1073 | 55.006 | 1683 | 106.3 | 1653 | 109.5 | 1723 | 117.5 | 1743 | 114.1 | 1733 | 117.3 |
| 1173 | 61.805 | 1693 | 107.2 | 1663 | 110.7 | 1733 | 118.0 | 1753 | 114.6 | 1743 | 117.7 |
| 1273 | 69.493 | 1703 | 108.2 | 1673 | 111.8 | 1743 | 118.4 | 1763 | 115.1 | 1753 | 118.2 |
| 1373 | 77.519 | 1713 | 109.4 | 1683 | 112.9 | 1753 | 118.9 | 1773 | 115.6 | 1763 | 118.6 |
| 1473 | 86.730 | 1723 | 110.0 | 1693 | 9.011 | 1763 | 119.3 | 1783 | 116.0 | 1773 | 119.0 |
| 1573 | 95.969 | 1733 | 110.0 | 1703 | 114.9 | 1773 | 119.8 | 1793 | 116.5 | 1783 | 119.4 |
| 1673 | 105.374 | 1743 | 111.9 | 1713 | 115.9 | 1783 | 120.2 | 1803 | 116.9 | 1793 | 119.9 |
| t Not abo | m in fiance | | | | | | | | | | |
| | ישוחקיו זיו זיוער ווא | | | | | | | | | | |

| T | ٩ | F | ٩ | Г | D | F | þ | L | J | L | d |
|------------|----------------|-----------------------|-----------------|----------|------------------|----------|----------------|----------|------------|---------|---------|
| DATA SET 1 | 0(cont.)* | DATA SET | 12(cont.) | DATA SET | <u>17(cont.)</u> | DATA SE | T 19* | DATA SET | 21(cont.)* | DATA S | ET 24* |
| 1803 | 120.3 | 281.3 | 9.96 | 82.7 | 0.967 | 200 | 8.16 | 310.7 | 13.015 | 288.7 | 12.478 |
| 1013 | 12U.8 | 300. / | 10.69 | 91.8 | 1.2/ | 204 | 8.51 | 511.4 | 12.964 | 6.767 | 12.024 |
| 1813 | 121.6 | 0.026 0.626 | 11 47 | 50T | 1.95 7 86 | 210 | 8.80 a 37 | 312.5 | 12.950 | 200.4 | 12.812 |
| 1843 | 122.0 | 378.4 | 12.87 | 133 | 1.72 | 215 | 0.76 | 313.7 | 12.983 | 302.7 | 12.871 |
| 1853 | 122.5 | 402.6 | 13.12 | 160 | 5.26 | 233 | 10.21 | 319.5 | 13.167 | 304.6 | 12.900 |
| 1863 | 122.9 | 485.1 | 16.27 | 192 | 7.63 | 238 | 10.44 | 324.4 | 13.339 | 305.8 | 12.912 |
| 1873 | 123.3 | 509.4 | 16.76 | 214 | 8.49 | 243 | 10.72 | 328.2 | 13.465 | 306.9 | 12.912 |
| 1883 | 123.8 | 538.5 | 18.22 | 237 | 10.25 | 251 | 11.09 | | | 308.1 | 12.903 |
| 1893 | 124.2 | 577.3 | 19.67 | 271 | 12.05 | 262 | 11.65 | DATA S | ET 22* | 309.4 | 12.903 |
| 1903 | 124.7 | 630.6 | 21.86 | 293 | 12.65 | 268 | 11.98 | | | 310.1 | 12.897 |
| 1913 | 125.2 | 698.5 | 24.77 | 298 | 12.83 | 279 | 12.44 | 291.5 | 12.721 | 310.5 | 12.885 |
| 6261 | 125.6 | 771.3 | 27.69 | 305 | 12.97 | 287 | 12.72 | 295.2 | 12.825 | 310.7 | 12.864 |
| 1933 | 126.0 | 853.7 | 31.57 | 308 | 12.96* | 294 | 12.93 | 299.1 | 12.922 | 310.9 | 12.800 |
| 1943 | 0.021 0.461 | 0.146 | 01.65 | 515 | 12.93 | 303 | 13.12 | 301.3 | 12.966 | 5.015 | 856.21 |
| 6641 | 1.011 | 111 | | 114 | C6.21 | 314 | 13.14 | 504.5 | 13.003 | 1.525 | 72. 22. |
| DATA SI | л ш* | VIVI | SET 13× | 110 | 13-00* | 321 | 13.30 13.47 | 1.905 | 13.024 | 1.826 | 13.134 |
| | | 4.2 | 0.255 | 2 | | 331 | 13.65 | 309.5 | 13.023 | DATA SE | r 25* |
| 87.3 | 0.56 | | | DATA SE | T 18* | 340 | 13.93 | 310.5 | 13.015 | | |
| 145.9 | 3.26 | DATA | SET 14* | | | 346 | 14.14 | 310.7 | 13.003 | 295 | 14.5 |
| 165.4 | 4.25 | | | 200 | 8.05 | | | 311.6 | 12.909 | 308 | 15.6 |
| 277.7 | 9.66 | 4.2 | 0.181 | 204 | 8.33 | DATA SET | r 20* | 311.8 | 12.909 | 325 | 16.1 |
| 292.4 | 16.6 | | | 209 | 8.61 | | | 314.6 | 12.984 | 357 | 16.9 |
| 316.8 | 10.41 | DATA | SET 15* | 215 | 8.91 | 93.5 | 2.6 | 320.0 | 13.163 | 382 | 18.6 |
| 326.6 | 10.41 | | | 219 | 9.16 | 133.2 | 5.1 | 325.8 | 13.362 | 477 | 23.2 |
| 380.4 | 12.38 | 4.2 | 0.125 | 224 | 9.47 | 166.4 | 7.8 | 328.2 | 13.439 | 668 | 33.2 |
| 487.9 | 15.83 | | | 230 | 9.84 | 196.7 | 9.8 | | | 745 | 37.3 |
| 561.2 | 18.54 | DATA | SET 16* | 239 | 10.28 | 222.2 | 11.0 | DATA S | ET 23* | 810 | 40.6 |
| 654.0 | 22.24 | | | 242 | 10.51 | 252.5 | 13.0 | | | | |
| 732.1 | 25.44 | 4.2 | 0.090 | 251 | 10.93 | 291.2 | 14.3 | 288.6 | 12.515 | DATA SE | r 26 |
| 810.2 | 28.89 | i | | 256 | 11.23 | 322.4 | 14.9 | 292.5 | 12.655 | | |
| 000.9 | 30.01 | VIVO | SET 1/ | 259 | 11.37 | 347.0 | 16.0 | 296.0 | 12.761 | 00 | 16.6 |
| 0.10K | | | | 267 | 11.79 | 367.8 | 16.9 | 298.6 | 12.824 | 489 | 24.0 |
| 1.0001 | 07.16 | 7.4 | ccu.u | 717 | 12.02 | 377.2 | 17.1 | 301.6 | 12.891 | 099 | 31.6 |
| 1049.4 | 12.04 | 11.8 | 0.056 | 278 | 12.26 | 389.5 | 17.6 | 303.1 | 12.918 | 868 | 39.2 |
| 1004.1 | 60.95 | 14.2 | 0.057 | 283 | 12.47 | | | 304.9 | 12.939 | 1069 | 47.1 |
| | | 18.0 | 0.062 | 290 | 12.72 | DATA SI | T 21* | 305.5 | 12.945 | 1285 | 57.4 |
| DATA | ET 12 | 21.6 | 0.065 | 310 | 13.23 | | | 306.7 | 12.945 | 1468 | 63.3 |
| - | ; | 26.7 | 0.075 | 316 | 13.37 | 300.8 | 13.014 | 308.0 | 12.937 | 1527 | 70.8 |
| 67.19 | 67.0 | 29.7 | 0.085 | 321 | 13.54 | 301.9 | 13.033 | 309.8 | 12.937 | 1607 | 76.9 |
| 1.79 | 1.22 | 31.3 | 0.093 | 324 | 13.88 | 304.1 | 13.057 | 310.4 | 12.924 | 1628 | 73.9 |
| 140./ | 2.68 | 42.9 | 0.151 | 336 | 14.05 | 305.5 | 13.069 | 310.6 | 12.907 | 1708 | 81.9 |
| 170 5 | 04.C | 4°70 | 0.264 | 939 | 14.16 | 307.2 | 13.069 | 311.0 | 12.827 | 1721 | 1.67 |
| C. 711 | 00.4 00 | 600 1. 1. | 0. 384 A 225 | 344 | 14.35 | 308.5 | 13.062 | 320.5 | 13.124 | 184/ | 85.4 |
| 2-1-4 | 70.0 | t . t . | C00.U | | | 309.9 | 13.03/ | 2.026 | 13.30/ | 1720 | 72.4 |

1.0

* Not shown in figure.

| Cr (continued) |
|---------------------|
| OF CHROMIUM |
| L RESISTIVITY |
| HE ELECTRICA |
| DATA UN 1 |
| EXPERIMENTAL |
| TABLE 3. |

| - | م | F | d | 1 | ٩ | F | ٩ | H | đ | F | đ |
|------------|---------------|------------|------------|------------|----------------|----------|----------------|----------------|--------------------|----------|-------------|
| DATA SET 2 | 6(cont.) | DATA SET 3 | 11(cont.)* | DATA SET 3 | 2(cont.)* | DATA SET | 33(cont.) | DATA SET | 34(cont.) * | DATA SET | 35(cont.)* |
| 2002 | 98.5 | 143 | 5.1 | 312 | 12.6 | 310.8 | 13.58* | 307.9 | 13.86 | 311.5 | 13.23 |
| 2015 | 95.4 | 146 | 5.4 | 318 | 12.5 | 311.3 | 13.58* | 309.1 | 13.83 | 313.2 | 13.28 |
| 2049 | 101.0 | 148 | 5.5 | 325 | 12.7 | 312.6 | 13.61* | 310.0 | 13.79 | 314.9 | 13.35 |
| 2065 | 99.9 | 154 | 5.8 9 | 341 | 13.2 | 314.0 | 13.67* | 310.6 | 13. / 2 | 316.8 | 13.42 |
| 2103 | 102.3 | 160 | 6.2 | 347 | 13.5 | 1.416 | 13.69 13.54 | 511.5 | 13.08 | 320.0 | 13.55 |
| 2103 | 7.011 | 181 184 | 0.4 | 166 071 | 13.8 14.2 | 1.016 | 13./5* | 1.216 | 00.01 | 525.0 | 13.6/ |
| 2196 | 9.111 | 189 | 0 | 111 | 14.5 | 320.2 | 13.88* | 317.2 | 13.86 | 127.65 | 11.84 |
| | | 192 | 8.3 | | • | 322.9 | 14.00* | 320.2 | 13.97 | 329.5 | 13.93 |
| DATA S | ET 27 | 208 | 9.4 | DATA | SET 33 | 326.3 | 14.15* | 322.3 | 14.06 | | k 1 1 |
| | | 216 | 6.9 | | | 328.7 | 14.22* | | | DATA S | ET 36* |
| 1673 | 80.3 | 219 | 9.9 | 242.9 | 11.49 | 330.8 | 14.35 | DATA S | ET 35* | | |
| 2053 | 100.0 | 219 | 10.1 | 247.4 | 11.63* | | | | | 243.0 | 11.34 |
| 2113 | 101.5 | 226 | 10.4 | 249.1 | 11.72* | DATA S | ET 34* | 243.0 | 11.34 | 247.0 | 11.51 |
| 2113 | 108.1 | 242 | 11.4 | 250.8 | 11.81* | | | 241.0 | 11.52 | 250.4 | 11.63 |
| | | 253 | 12.2 | 251.9 | 11.84# | 243.0 | 11.48 | 2.062 | 11.63 | 253.4 | 11.76 |
| DATA SE | r 28* | 259 | 12.3 | 254.8 | 11.95* | 247.2 | 11.65 | 253.4 | 11.79 | 258.2 | 11.95 |
| | | 261 | 12.5 | 258.4 | 12.10* | 249.1 | 11.72 | 258.0 | 11.96 | 262.0 | 12.13 |
| 2013 | 132 | 277 | 13.0 | 260.8 | 12.20* | 250.8 | 11.81 | 262.3 | 12.13 | 265.2 | 12.24 |
| | ; | 281 | 13.2 | 264.4 | 12.36* | 251.9 | 11.84 | 265.2 | 12.24 | 269.0 | 12.41 |
| DATA S | ET 29 | 285 | 13.4 | 266.7 | 12.45* | 254.6 | 11.95 | 269.3 | 12.42 | 274.2 | 12.55 |
| | | 288 | 13.5 | 268.8 | 12.52* | 258.2 | 12.12 | 273.9 | 12.55 | 278.6 | 12.70 |
| 1084 | 50.0 | 293 | 13.6 | 272.5 | 12.66 | 260.8 | 12.20 | 278.6 | 12.71 | 281.2 | 12.79 |
| 1292 | 59.1 | 294 | 13.6 | 272.1 | 12.74* | 264.4 | 12.36 | 280.9 | 12.80 | 284.5 | 12.89 |
| 1501 | 68.9 | 297 | 13.7 | 276.3 | 13.83* | 266.5 | 12.45 | 284.3 | 12.92 | 286.7 | 12.98 |
| 1702 | 79.6 | 302 | 13.9 | 278.8 | 12.95* | 268.8 | 12.52 | 286.7 | 12.99 | 289.2 | 13.11 |
| 1161 | 89.5 | 307 | 13.9 | 279.7 | 12.97* | 272.5 | 12.66 | 289.0 | 13.07 | 292.0 | 13.20 |
| 2051 | 97.1 | 310 | 13.9 | 281.4 | 13.03* | 273.9 | 12.74 | 292.0 | 13.16 | 294.1 | 13.26 |
| 2136 | 102.5 | 315 | 13.8 | 283.1 | 13.11* | 276.3 | 12.83 | 293.9 | 13.21 | 296.2 | 13.31 |
| 2152 | 108.7 | 325 | 14.0 | 285.8 | 13.22* | 278.8 | 12.94 | 295.4 | 13.25 | 297.9 | 13.32 |
| 2214 | 112.5 | 334 | 14.2 | 289.0 | 13.34 * | 279.7 | 12.97 | 296.9 | 13.26 | 299.0 | 13.34 |
| 2261 | 115.6 | 337 | 14.5 | 290.9 | 13.40* | 281.1 | 13.04 | 298.1 | 13.28 | 300.2 | 13.35 |
| | | 357 | 15.1 | 291.8 | 13.44* | 283.0 | 13.11 | 299.2 | 13.30 | 301.1 | 13.32 |
| DATA SI | 1 30* | 379 | 16.0 | 292.6 | 13.46 | 285.8 | 13.22 | 300.3 | 13.28 | 302.2 | 13.32 |
| | 0 00 F | 401 | 17.0 | 296.2 | 13.60* | 288.8 | 13.32 | 301.3 | 13.28 | 303.0 | 13.30 |
| 19/J | 8.021 | | | 299.6 | 13.72* | 290.5 | 13.40 | 101.9 | 13.26 | 303.9 | 13.27 |
| | | DATA | ET 32* | 105 | 13.//* | R-167 | 13.44 | 0.5U5 | 13.23 | 304.7 | 13.22 |
| C VIVO | 11 21- | 715 | | 4.202 | 13./9# | 9.262 | 13.40 | 4.505 0.505 | 13.20 | 304.7 | 13.18 |
| ģ | • | C/7 | 9.11 | 303.8 | -79.CI | 2.062 | 13.01 | 505.9 | 13.14 | 1.00 | 13.12 |
| 8, 5, | 1./ | 282 | 11.8 | 305.3 | 13.83* | 299.2 | 13.73 | 304.3 | 13.09 | 306.0 | 13.11 |
| 102 | 2.0 | 285 | 12.1 | 306.2 | 13.83* | 300.9 | 13.78 | 304.7 | 13.07 | 306.8 | 13.12 |
| 108 | 3.2 | 291 | 12.3 | 307.0 | 13.80* | 302.1 | 13.82 | 305.1 | 13.03 | 308.5 | 13.21 |
| 114 | 3.6 | 293 | 12.3 | 308.3 | 13.78* | 303.6 | 13.86 | 306.0 | 13.04 | 310.2 | 13.28 |
| 121 | 4.1 | 298 | 12.3 | 309.6 | 13.75* | 304.9 | 13.86 | 307.0 | 13.06 | 313.0 | 13.37 |
| 127 | 4.3 | 301 | 12.5 | 310.0 | 13.68* | 306.2 | 13.88 | 308.5 | 13.12 | 317.2 | 13.54 |
| 133 | 4.6 | 306 | 12.6 | 310.6 | 13.63* | 307.2 | 13.86 | 310.2 | 13.18 | 321.0 | 13.68 |
| | | | | | | | | | | 326.3 | 13.87 |
| * Not sho | wn in figure. | | | | | | | | | | |

36

12.2.70 10.30 10.44 10.55 10.55 10.60 10.73 10.75 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.60 10.95 10.99 10 43* a 42* SET SET DATA DATA 243.0 2552.1 2552.1 2552.1 2552.1 2552.1 2555.1 2555.1 2555.1 2555.1 2555.1 2555.1 2255.1 2273.1 227 320.6 323.0 325.1 243.0 247.5 251.5 255.7 255.7 259.5 259.5 259.5 H 40(cont.)* 10.78 10.82 10.82 11.15 12.38 12.48 12.66 12.66 12.78 12.89 13.00 13.08 41* a SET DATA SET DATA 243.0 243.0 2246.5 2246.5 2246.5 2253.0 2255.0 2255 310.0 312.1 316.2 316.2 316.9 321.1 321.1 323.6 н DATA SET 39(cont.)* 12.74 12.85 12.85 12.90 13.00 13.23 13.23 13.39 13.49 13.49 10.80 10.80 10.80 10.99 10 ٩ 40* SET DATA 311.7 314.3 316.0 316.0 318.3 321.1 321.1 322.9 322.4 332.6 330.0 ы DATA SET 38(cont.)* 13.18 13.31 13.49 13.63 11.68 11.75 11.75 11.90 11.90 12.03 12.14 12.26 12.28 12.31 12.45 12.45 12.45 12.45 12.45 12.45 12.45 12.45 12.25 12.55 11.02 11.44 11.61 12.37 39* ٩ SET DATA 317.2 321.0 325.1 329.1 243.0 2246.4 2246.4 2246.4 2251.3 2254.2 2254.2 2266.1 2266.1 2266.1 2266.1 2266.1 2266.1 2266.1 2266.1 2275.0 2277.0 200 H DATA SET 37(cont.)* 11.24 11.56 11.56 11.56 11.57 11.56 11.73 11.23 13.25 13.30 13.37 13.50 13.59 13.68 12.75 12.70 12.65 12.65 12.60 12.69 12.74 12.74 12.99 38# ٩ SET DATA 242.8 242.8 2251.0 2251.0 2255.9 2255 320.8 322.7 324.2 324.2 327.2 329.3 331.4 H $\begin{array}{c} 11.3\\$ a DATA SET 37* 242.8 251.0 2551.3 2551.3 2551.3 2551.3 2551.3 2551.3 2551.3 2551.3 2551.4 2551.3 2551.3 2551.4 2551.4 2551.4 2551.4 2551.4 2551.4 2551.3 2551.4 2551.4 2551.3 2551.4 2551.3 2551.4 2551.3 2555.3 2551.3 2555 315.5 319.6 113. H

Not shown in figure.

| (continued) |
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| Сr |
| CHROMIUM |
| OF |
| RESISTIVITY |
| ELECTRICAL |
| THE |
| NO |
| DATA |
| EXPERIMENTAL |
| TABLE 3. |

| - | ٩ | ÷ | đ | F | ٩ | T | ٩ | ÷ | a | ц | ٩ |
|----------|------------|----------|-------------|----------|-----------|----------|------------|--------|--------|-------------|----------|
| DATA SET | 43(cont.)* | DATA SET | i5(cont.)* | DATA SET | 46(cont.) | DATA SET | 49(cont.)* | DATA S | ET 52# | DATA SET 5. | (cont.)* |
| 264.0 | 10.76 | 1372 | 101.2 | 307.4 | 13.20* | 311.9 | 12.901 | 306.9 | 12.812 | 311.86 | 12.642 |
| 264.9 | 10.76 | 1447 | 113.0 | 308.2 | 13.31* | 313.6 | 12.895 | 307.1 | 12.800 | 311.98 | 12.643 |
| 265.9 | 10.74 | 1531 | 112.7 | 309.9 | 13.40* | 315.0 | 12.911 | 307.9 | 12.807 | 312.10 | 12.645 |
| 267.0 | 10.74 | 1605 | 119.1 | 313.4 | 13.52* | 316.5 | 12.953 | 310.1 | 12.786 | 312.21 | 12.646 |
| 268.0 | 10.72 | 1669 | 119.1 | | | 320.4 | 13.078 | 311.4 | 12.777 | 312.33 | 12.651 |
| 269.3 | 10.69 | 1724 | 140.9 | DATA S | SET 47* | | | 312.9 | 12.774 | 312.92 | 12.665 |
| 270.2 | 10.64 | 1869 | 140.6 | | | DATA | SET 50 | 313.6 | 12.774 | 313.70 | 12.689 |
| 270.4 | 10.60 | 1919 | 140.6 | 80 | 1.060 | | | 314.8 | 12.790 | 314.41 | 12.710 |
| 270.8 | 10.54 | 1976 | 148.6 | 90 | 1.445 | 80 | 0.860 | 316.4 | 12.811 | 315.29 | 12.736 |
| 271.0 | 10.49 | | | 100 | 1.860 | 90 | 1.225 | 320.3 | 12.945 | 316.01 | 12.759 |
| 271.9 | 10.50 | DATA | SET 46 | 120 | 2.860 | 100 | 1.630 | | | 317.07 | 12.793 |
| 272.5 | 10.53 | | | 140 | 4.050 | 120 | 2.605 | DATA S | ET 53* | 317.78 | 12.814 |
| 274.0 | 10.58 | 5.1 | 0.20 | 160 | 5.295 | 140 | 3.760 | | | 318.38 | 12.835 |
| 275.0 | 10.62 | 79.6 | 1.03 | 180 | 6.575 | 160 | 5.000 | 300.00 | 12.619 | 318.91 | 12.850 |
| 277.6 | 10.69 | 89.0 | 1.26 | 200 | 7.830 | 180 | 6.315 | 300.71 | 12.637 | 319.15 | 12.859 |
| 280.1 | 10.80 | 94.1 | 1.47 | 220 | 9.100 | 200 | 7.545 | 301.54 | 12.655 | | |
| 282.7 | 10.88 | 100.9 | 1.76 | 240 | 10.300 | 220 | 8.790 | 302.37 | 12.671 | DATA SE | :T 54* |
| 286.3 | 11.01 | 107.8 | 2.08* | 260 | 11.385 | 240 | 10.015 | 303.02 | 12.683 | | |
| 291.4 | 11.20 | 112.0 | 2.32* | 280 | 12.270 | 260 | 11.095 | 303.73 | 12.698 | 300.95 | 12.698 |
| 293.5 | 11.30 | 116.3 | 2.58* | 300 | 12.880 | 280 | 12.030 | 304.91 | 12.719 | 304.74 | 12.762 |
| 298.2 | 11.46 | 125.7 | 3.17 | 304 | 12.946 | 300 | 12.710* | 305.50 | 12.728 | 308.52 | 12.794 |
| 301.3 | 11.57 | 132.5 | 3 27* | 306 | 12.961 | 304 | 12.792* | 305.97 | 12.733 | 310.99 | 12.762 |
| 303.3 | 11.63 | 147.8 | 4.55 | 308 | 12.958 | 306 | 12.813 | 306.45 | 12.738 | 312.22 | 12.672 |
| 306.3 | 11.85 | 157.2 | 5.28* | 310 | 12.931 | 308 | 12.816* | 307.04 | 12.743 | 314.05 | 12.720 |
| 312.2 | 12.03 | 167.4 | 6.01 | 312 | 12.900 | 310 | 12 791 | 307.51 | 12.747 | 317.79 | 12.835 |
| 316.2 | 12.18 | 180.2 | 6.80 | 314 | 12.898 | 312 | 12.772* | 308.10 | 12.751 | | |
| 321.5 | 12.42 | 190.4 | 7.54* | 316 | 12.940 | 314 | 12.780* | 308.45 | 12.751 | DATA SE | IT 55* |
| 325.9 | 12.64 | 198.1 | 8.65* | 320 | 13.080 | 316 | 12.808* | 308.69 | 12.752 | | |
| | | 199.0 | 8.09* | 340 | 13.765 | 320 | 12.925* | 308.98 | 12.753 | 301.04 | 12.692 |
| DATA S | ET 44 | 206.6 | 8.97 | 360 | 14.470 | 340 | 13.605 | 309.10 | 12.753 | | |
| | | 211.8 | 8.94* | 380 | 15.200 | 360 | 14.340 | 309.34 | 12.753 | DATA SF | :T 56* |
| 1124 | 46.2 | 210.0 | 9.18* | 400 | 15.935 | 380 | 15.085 | 309.57 | 12.752 | | |
| 1206 | 54.7 | 218.6 | 9.62* | | | 400 | 15.845 | 309.69 | 12.751 | 301.28 | 12.703 |
| 1276 | 61.1 | 223.7 | 9.65 | DATA S | ET 48* | | | 309.93 | 12.749 | 301.16 | 12.704 |
| 1379 | 72.1 | 233.9 | 10.35* | | 1 | DATA S | ET 51* | 310.05 | 12.748 | 304.91 | 12.766 |
| 1466 | 90.2 | 245.9 | 11.03* | 310.4 | 12.937 | | | 310.16 | 12.746 | 308.79 | 12.795 |
| 1605 | 95.3 | 257.8 | 11.67 | 311.8 | 12.880 | 307.9 | 12.788 | 310.40 | 12.743 | 311.27 | 12.740 |
| 1761 | 112.5 | 268.0 | 12.26* | 312.6 | 12.853 | 310.3 | 12.795 | 310.52 | 12.740 | 312.63 | 12.678 |
| 1938 | 166.3 | 278.3 | 12.76* | 313.1 | 12.847 | 311.2 | 12.762 | 310.63 | 12.735 | 314.27 | 12.728 |
| | | 286.8 | 13.11 | 313.8 | 12.871 | 311.8 | 12.722 | 310.87 | 12.725 | 317.96 | 12.844 |
| DATA SL | T 45* | 291.9 | 13.28* | 314.6 | 12.896 | 312.9 | 12.716 | 311.16 | 12.696 | | |
| | | 297.1 | 13.37* | | | 314.6 | 12.759 | 311.45 | 12.662 | DATA SE | T 57* |
| 1120 | 68.6 | 297.9 | 13.37* | DATA S | ter 49* | 316.9 | 12.805 | 311.57 | 12.648 | | |
| 1160 | 72.4 | 300.5 | 13.34 | | | 317.9 | 12.851 | 311.57 | 12.645 | 301.28 | 12.699 |
| 1239 | 80.9 | 303.1 | 13.31* | 306.6 | 12.961 | 320.5 | 12.945 | 311.68 | 12.644 | | |
| 1284 | 95.7 | 304.8 | 13.28* | 309.5 | 12.937 | | | 311.74 | 12.643 | | |
| | | | | | | | | | | | |

* Not shown in figure.

70(cont.)* 12.920 12.920 12.909 12.906 12.906 12.938 12.889 12.889 12.889 12.889 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.887 12.897 12.9977 12.9977 12.9977 12.9977 12.9977 12.9977 12.9977 12.9977 1 Q. SET 71* SET DATA 311.8 312.0 312.1 312.1 312.3 312.5 312.6 312.7 312.9 313.0 313.3 313.6 313.3 313.8 314.0 314.3 314.7 314.7 315.4 315.6 315.9 315.9 316.6 316.6 100.0 102.6 104.9 107.6 109.2 110.2 111.3 1112.2 1113.9 1113.9 1113.9 1113.9 1113.9 1113.9 116.5 312.0 317.8 317.5 н DATA 317. 69(cont.) 12.859 12.868 12.875 12.875 12.892 12.892 12.900 12.937 12.937 12.960 12.888 12.900 12.957 12.957 12.957 12.957 12.956 12.9799 12.9799 12.9799 12.9799 12.9799 12.9799 12.9799 12.9799 12.9799 ٩ SET 70* DATA SET DATA 313.4 313.6 313.6 314.4 314.6 314.6 315.1 315.6 315.3 300.3 301.2 301.2 301.2 302.9 306.5 307.5 H 12.899 DATA SET 68(cont. 12.30 12.44 12.5.75 12.75 12.80 12.85 12.75 12.7 SET 69* đ DATA [H 53.64 56.88 60.41 63.07 65.72 2.51 19.70 20.11 20.11 20.16 21.12 21.12 21.10 21.02 21.02 21.07 21.07 21.13 21.17 21.26 0.36 1.83 2.57 2.57 2.57 2.57 2.57 2.21.93 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.22.57 2.2 DATA SET 65(cont. 23.21 12.07 23.11 67* DATA SET 68 đ **66** SET SET DATA DATA 78.9 273.2 279.1 279.1 283.6 294.5 301.1 309.6 311.8 313.9 315.1 316.5 317.5 319.1 278.4 20.8 77.7 90.1 192.3 273.2 273.2 273.2 273.2 273.2 273.2 273.2 205.4 205.4 300.4 300.4 310.2 310.6 319.6 319.6 325.0 327.8 373.2 1123 1175 1175 1224 1273 1319 н 12.630 12.680 12.680 12.841 12.841 12.841 12.845 12.845 12.845 12.845 12.855 12.773 12 15.25 16.14 16.14 24.13 30.92 35.94 44.20 55.71 21.47 39.48 44.79 ٩ SET 63* SET 64 SET 65 DATA DATA DATA 299.7 299.4 2006.4 2006.4 2006.4 2006.4 2006.4 2007.7 200. н 371 391 484 484 579 726 824 873 873 976 976 1077 518 875 968 12.710 12.712 12.709 12.709 12.704 12.704 12.704 12.704 12.685 12.736 12.718 12.720 12.720 12.770 12.776 12.776 12.699 12.699 12.752 12.867 12.853 12.714 12.88 13.19 17.92 17.92 221.17 221.17 221.17 221.17 321.17 321.17 332.85 226.49 226.49 226.49 227.97 277.97 DATA SET 59* DATA SET 60* DATA SET 61* a SET 58* DATA SET 62 302.10 DATA 301.43 301.54 301.56 305.21 305.21 305.11 311.51 312.81 314.59 318.32 301.98 302.10 302.21 305.91 305.62 309.62 311.99 313.39 315.09 318.72 H 293 325 432 432 475 475 636 636 677 777 777 777 777 890 890 800

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| TABLE |

| F | ٩ | F | ٩ | L | م | E- | d | H | d | T | d |
|------------|-----------|---|------------|----------------|----------------|----------|------------|----------|----------------|----------|------------|
| DATA SET 7 | I(cont.)* | DATA SET | 72(cont.)* | DATA SET | 74(cont.)* | DATA SET | '5(cont.)* | DATA SET | 76(cont.)* | DATA SET | 77(cont.)* |
| 118.6 | 2.66 | 122.3 | 3.012 | 108.7 | 2.186 | 120.7 | 2.766 | 126.1 | 3.020 | 123.6 | 2.888 |
| 119.3 | 2.70 | 122.8 | 3.025 | 110.8 | 2.270 | 121.3 | 2.783 | 126.7 | 3.074 | 123.8 | 2.897 |
| 120.2 | 2.75 | 123.8 | 3.058 | 112.7 | 2.362 | 121.3 | 208.2 | 121 6 | 3.1/2 240 | 124.2 | 2.918 |
| 121.6 | 2.84 | 125.3 | 1.160 | 114.7 | 2.452 | 121.8 | 2.831 | 135.3 | 3.590 | | |
| 122.0 | 2.86 | 126.2 | 3.208 | 116.2 | 2.535 | 122.4 | 2.860 | 136.4 | 3.655 | DATA S | ET 78* |
| 122.6 | 2.87 | 129.0 | 3.387 | 117.3 | 2.587 | 123.3 | 2.901 | 137.6 | 3.742 | | |
| 123.1 | 2.89 | 129.6 | 3.417 | 119.1 | 2.668 | 124.0 | 2.940 | 140.4 | 3.919 | 281.7 | 11.93 |
| 123.6 | 2.90 | 130.8 | 3.500 | 120.2 | 2.741 | 124.6 | 2.969 | | | 292.3 | 12.27 |
| 123.9 | 2.92 | 131.6 | 3.546 | 120.5 | 2.765 | 124.9 | 2.987 | DATA S | ET 77* | 298.7 | 12.45 |
| 124.4 | 2.95 | 132.5 | 3.616 | 121.3 | 2.784 | | | | | 302.0 | 12.52 |
| 125.2 | 3.00 | 133.5 | 3.672 | 121.7 | 2.834 | DATA S | ET 76* | 117.4 | 2.557 | 305.4 | 12.59 |
| 8.C21 | | 0.001 | 10/.C | 0.221 | 400.7 700 C | 100 8 | 1 817 | 117 7 | 2.203 | 1.100 | 12 61 |
| 127.8 | 3.15 | 136.9 | 410.0 | 124.1 | 2.956 | 101.7 | 1.848 | 117.7 | 2.572 | 308.4 | 12.57 |
| 129.4 | 3.25 | 138.0 | 4.000 | 125.0 | 2.983 | 102.7 | 1.889 | 118.1 | 2.587 | 309.4 | 12.57 |
| 130.1 | 3.29 | 139.1 | 4.080 | 125.8 | 3.036 | 104.1 | 1.944 | 118.2 | 2.593 | 311.0 | 12.57 |
| 131.8 | 3.40 | 140.3 | 4.171 | 126.5 | 3.084 | 105.1 | 1.987 | 118.4 | 2.607 | 311.4 | 12.51 |
| 132.8 | 3.46 | | | 127.4 | 3.133 | 105.9 | 2.014 | 118.6 | 2.613 | 311.6 | 12.47 |
| 133.7 | 3.52 | DATA S | ET 73* | 128.5 | 3.197 | 106.6 | 2.050 | 118.7 | 2.621 | 311.7 | 12.44 |
| 135.1 | 3.60 | | 1 | 129.8 | 3.298 | 107.4 | 2.077 | 119.1 | 2.642 | 312.5 | 12.42 |
| 135.8 | 3.66 | 116.3 | 2.669 | 131.4 | 3.403 | 108.0 | 2.110 | 119.2 | 2.650 | 313.3 | 12.44 |
| 136.9 | 3.74 | 116.8 | 2.699 | 133.3 | 3.504 | 108.7 | 2.138 | 119.5 | 2.662 | 314.2 | 12.47 |
| 138.3 | 3.82 | 117.3 | 2.722 | 135.4 | 3.665 | 109.3 | 2.162 | 119.6 | 2.673 | 315.5 | 12.52 |
| 138.8 | 3.87 | 118.2 | 2.770 | 137.7 | 3.825 | 110.3 | 2.200 | 119.8 | 2.678 | 318.0 | 12.59 |
| 140.1 | 3.95 | 118.9 | 2.810 | 139.5 | 3.965 | 111.1 | 2.240 | 119.9 | 2.684 | 319.9 | 12.65 |
| 141.7 | 4.07 | 119.3 | 2.834 | 140.4 | 4.028 | 112.0 | 2.280 | 120.0 | 2.692 | 328.7 | 12.93 |
| 144.5 | 4.25 | 119.9 | 2.876 | | | 112.5 | 2.305 | 120.1 | 2.699 | i | |
| | | 120.3 | 2.909 | DATA S | ET 75* | 113.1 | 2.336 | 120.3 | 2.705 | DATA | SET 79 |
| DATA SE | 1 72× | 120.8 | 2.928 | | | 113.5 | 2.357 | 120.5 | 2.717 | | |
| 0.000 | | 121.3 | 2.943 | 116.2 | 2.531 | 114.2 | 2.383 | 120.6 | 2.724 | 2.39 | 0.147 |
| 100.8 | 1.9/6 | 1.121 | 2.961 | 0./11 | 2.576 | 114.6 | 2.410 | 1.021 | 0//.7 | 3.03 | 0.135 |
| 105.01 | | 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 2 004 | 4./11 117 0 | 2,290 | 9.CTT | CC#.1 | 121.7 | 611.2 877 c | 4.00 | 0.144 |
| 108.0 | 2.280 | 122.7 | 3.020 | 118.2 | 2.634 | 117.8 | 2.565 | 121.3 | 2.785 | 5.38 | 0.135 |
| 111.5 | 2.440 | 123.4 | 3.050 | 118.5 | 2.652 | 118.6 | 2.611 | 121.4 | 2.791 | 5.49 | 0.153 |
| 113.2 | 2.520 | 123.9 | 3.083 | 118.9 | 2.673 | 119.6 | 2.670 | 121.6 | 2.803 | 9.74 | 0.147 |
| 114.2 | 2.558 | | | 119.4 | 2.695 | 120.6 | 2.724 | 121.7 | 2.815 | 10.8 | 0.153 |
| 115.3 | 2.608 | DATA S | ET 74* | 119.6 | 2.708 | 121.2 | 2.742 | 121.8 | 2.820 | 18.7 | 0.166 |
| 116.2 | 2.670 | | | 119.8 | 2.722 | 121.7 | 2.780 | 121.9 | 2.820 | 21.1 | 0.159 |
| 117.1 | 2.716 | 100.8 | 1.775 | 119.9 | 2.741 | 122.4 | 2.812 | 122.1 | 2.822 | 27.8 | 0.173 |
| 118.5 | 2.769 | 101.8 | 1.891 | 120.0 | 2.741 | 122.4 | 2.855 | 122.1 | 2.825 | 43.8 | 0.224 |
| 119.7 | 2.854 | 102.6 | 1.924 | 120.2 | 2.742 | 123.1 | 2.868 | 122.5 | 2.836 | 53.4 | 0.357 |
| 121.0 | 2.910 | 104.0 | 1.976 | 120.3 | 2.743 | 123.8 | 2.900 | 122.9 | 2.858 | 63.8 | 0.474 |
| 121.4 | 2.948 | 105.7 | 2.046 | 120.4 | 2.745 | 124.8 | 2.946 | 123.1 | 2.868 | 66.4 | 0.604 |
| 0.121 | 2.995 | 7. JUL | 2.110 | 120.5 | 2.741 | 125.4 | 2.986 | 123.4 | 2.877 | 10.5 | 0.941 |

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| 1 | T DATA SET 180 | p 81(cont.)* 6.830 | T Data Set 1764 | p 82(cont.) 82.6 | T DATA SE 1469 | p 1 86* 70.7 | T DATA SET | p 90(cont.)* 11.54 | T DATA SET 311.0 | p 91(cont.)* 13.98 |
|-----------|----------------------|--------------------------|-----------------------|------------------------|----------------------|--------------------|---------------|--------------------------|------------------------|--------------------------|
| 190 | | 7.480 | 1829 | 84.4 2 | 1520 | 74.0 | 244.3 | 11.78 | 313.9 | 14.05 |
| 210 | | 8.13U 8.805 | 1900 | 89.2 | 1570 | 4.17 | 254.6 | 12.31 | 323.0 | 14.33 |
| 220 | | 9.460 | 6661 | 93.1 | 1603 | 79.2 | 259.3 | 12.48 | | |
| 230 | | 10.125 | 1967 | 97.1 | 1633 | 81.3 | 265.9 | 12.80 | DATA | SET 92 |
| 760 | | 227.01 222.11 | E/6T | 5.94 | 1693 | 1.08 | 9.692 | 66.2T | 106 7 | 0, 0 |
| 260 | | C7C.11 | 0.4 T.A | cet 83 | DATA C | tr 074 | 0.010 | 13 33 | 203 2 | 9 77* |
| 270 | | 12.385 | UTUM | 0 140 | | 10 11 | 284.6 | 13.48 | 207.9 | *96.6 |
| 280 | | 12.840 | 391 | 12.8 | 285.4 | 14.16 | 290.3 | 13.62 | 215.3 | 10.33* |
| 290 | | 13.230 | 498 | 16.3 | 289.1 | 14.27 | 295.0 | 13.67 | 224.7 | 10.93* |
| 300 | | 13.480 | 595 | 20.1 | 292.9 | 14.38 | 300.7 | 13.74 | 228.4 | 11.13 |
| 310 | | 13.560 | 692 | 24.7 | 298.3 | 14.47 | 305.4 | 13.84 | 232.1 | 11.34* |
| 320 | | 13.745 | 800 | 29.3 | 303.4 | 14.52 | 308.2 | 13.87 | 239.6 | 11.68* |
| 330 | | 14.110 | 967 | 36.9 | 308.6 | 14.47 | 310.1 | 13.89 | 243.4 | 11.88* |
| 340 | | 14.460 | 1075 | 42.4 | 311.6 | 14.40 | 312.0 | 13.94 | 248.0 | 12.14* |
| 350 | | 14.830 | 1092 | 43.2 | 313.5 | 14.40 | 315.8 | 13.99 | 255.5 | 12.43* |
| 360 | | 15.190 | 1231 | 51.6 | 318.7 | 14.56 | 319.6 | 14.13 | 259.3 | 12.60* |
| | | | 1371 | 60.6 | 323.6 | 14.77 | 325.2 | 14.33 | 262.1 | 12.72 |
| DATA SI | 5 | ET 82 | 1469 | 66.1 | | | 330.8 | 14.47 | 265.9 | 12.87* |
| 066 | | | 1564 | 71.6 | DATA S | ET 88* | 334.6 | 14.67 | 273.5 | 13.23* |
| 000 14 | | 15.6 | 1750 | | 0 186 | 16 40 | 346.8 | 15,06 | 280.9 | 13.43* |
| 474 | | 17.6 | 1850 | 90.0 | 288.2 | 16.56 | 350.5 | 15.27 | 286.5 | 13.57* |
| 571 | | 21.3 | 1905 | 97.3 | 293.1 | 16.70 | 358.1 | 15.47 | 289.3 | 13.67* |
| 661 | | 24.7 | | | 298.3 | 16.79 | 363.7 | 15.76 | 295.0 | 13.79* |
| 151 | | 29.1 | DATA S | SET 84 | 303.5 | 16.74 | 369.3 | 15.93 | 299.7 | 13.84* |
| 765 | | 29.9 | | | 308.6 | 16.53 | 375.9 | 16.19 | 304.5 | 13.84 |
| 835 | | 33.1 | 1272 | 58.1 | 313.5 | 16.63 | 381.5 | 16.39 | 307.3 | 13.79* |
| 849 | | 33.8 | 1325 | 61.4 | 318.7 | 16.83 | 388.1 | 16.70 | 310.2 | 13.70* |
| 126 | | 37.3 | 1387 | 65.3 | 323.6 | 17.06 | 393.7 | 16.83 | 312.1 | 13,75* |
| 939 | | 37.9 | 1443 | 69.1 | | | 397.5 | 17.07 | 313.0 | 13.79* |
| 1025 | | 42.6 | 1498 | 72.5 | DATA S | ET 89* | 405.9 | 17.33 | 315.8 | 13,84* |
| 1047 | | 43.2 | 1560 | 76.5 | | | 411.5 | 17.60 | 320.5 | 13.99* |
| 1165 | | 49.5 | 1614 | 8.67 | 11 | 0.8 | 414.4 | 17.70 | 325.2 | 14.13* |
| 1264 | | 55.6 | 1664 | 83.0 | | | | | 335.6 | 14.47* |
| 1275 | | 56.2 | 1704 | 85.5 | DATA S | ET 90* | DATA S | ET 91* | 337.5 | 14.50* |
| 1360 | | 61.5 | 1724 | 86.7 | | | | | 137.5 | 14.52* |
| 1402 | | 63.9 | | | 198.5 | 9.48 | 283.0 | 13.51 | 338.4 | 14.62* |
| 1460 | | 67.5 | DATA S | ET 85* | 207.9 | 9.89 | 287.9 | 13.63 | 341.2 | 14.72* |
| 1510 | | 70.3 | | | 214.4 | 10.21 | 292.3 | 13.71 | 343.1 | 14.77* |
| 1542 | | 71.9 | 1482 | 71.4 | 218.1 | 10.50 | 298.0 | 13.79 | 348.7 | 14.96 |
| 1574 | | 73.7 | 1511 | 73.5 | 224.7 | 10.69 | 303.7 | 13.87 | 358.1 | 15.37* |
| 1652 | | 17.4 | 1651 | 82.4 | 230.3 | 11.00 | 305.7 | 13.91 | 9.512 | 16.07 |
| 1740 | | 80.8 | 1682 | 84.3 | 234.0 | 11.30 | 308.6 | 13.93 | 383.4 | 16.29* |
| | - { | | 1740 | 87.9 | | | | | | |

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|----------------|-----------|------------------|----------------|--------------|--------------|------------|---------------|----------|----------------|----------------|-----------|
| DATA SET 9 | 12(cont.) | DATA SET 5 |)5(cont.)* | DATA SET 9 | 9(cont.)* | DATA SET 9 | 9(cont.)* | DATA SET | 100(cont.) | DATA SET 10 | 2(cont.)* |
| 400.3 | 17.04 | 310.1 | 12.40 | 56.0 | 1.26 | 300.1 | 12.86 | 204 | 8.20 | 123.6 | 3.22 |
| 405.0 | 17.24* | 310.4 | 12.38 | 59.4 66.4 | 1.32 | 301.4 | 12.88 | 216 | 9.02* 0 60* | 132.1 | 3.65 |
| 406.7 | 17 77# | 0.01C | 12.30 85 11 | 100.4 | 1.63 | 10200 | 12 90 | 111 | 10.39* | 157 6 | 4.00 |
| 424.7 | 18.13 | 311.7 | 12.39 | 78.7 | 1.85 | 305.2 | 12.91 | 248 | 11.01 | 174.6 | 5.79 |
| | | 312.3 | 12.40 | 79.8 | 1.90 | 306.0 | 12.92 | 260 | 11.69* | 183.1 | 6.64 |
| DATA S | *C6 13 | 312.7 | 12.41 | 89.2 | 2.26 | 306.9 | 12.92 | 271 | 12.26* | 191.6 | 7.50 |
| | | 313.0 | 12.41 | 101 | 2.76 | 308.2 | 12.92 | 282 | 12.77 | 204.4 | 8.14 |
| 283.8 | 13.57 | 313.6 | 12.44 | 110 | 3.23 | 309.0 | 12.91 | 291 | 13.05* | 217.2 | 00.6 |
| 288.1 | 13.68 | 314.8 | 12.47 | 114 | 3.40 | 209.5 | 12.88 | 297 | 13.24* | 225.7 | 9.64 |
| 293.3 | 13.79 | 316.1 | 12.50 | 133 | 4.47 | 209.8 | 12.85 | | | 238.4 | 10.28 |
| 296.3 | 13.84 | 318.5 | 12.58 | 136 | 4.64 | 309.9 | 12.80 | DATA | ET 101 | 251.2 | 10.93 |
| 1.162 | 13.80 | 8.126 | 89.2T | 143 | 8 | 1.010 | 9/.21 | | | 1.402 | /c.11 |
| | 20.C1 | 0.020 7 7 7 5 | 17.06 | 151 | 07.0 07 3 | 1115 | 12./4 | 4 105 | 12 21 | 5 086 | 12.21 |
| 4.900 | 13.75 | C • 170 | 77.74 | 151 | 5 60 | 1111 | 12.76 | 302.5 | | 208.0 | 13 07 |
| 307.4 | 13.70 | DATA SI | ET 96# | 156 | 5.84 | 311.9 | 12.67 | 304.3 | 13.36 | 107.3 | 13.28 |
| 308.8 | 13.80 | | | 163 | 6.23 | 314.1 | 12.73 | 305.3 | 13.37 | 306.3 | 13.07 |
| 309.8 | 13.73 | 312.22 | 12.45 | 168 | 6.57 | 316.1 | 12.80 | 306.3 | 13.38 | 319.4 | 13.07 |
| 310.7 | 13.79 | | • | 173 | 6.84 | 319.7 | 12.93 | 307.7 | 13.38 | 327.9 | 13.50 |
| 313.6 | 13.89 | DATA | SET 97* | 179 | 7.17 | 325.0 | 13.13 | 308.6 | 13.38 | 336.4 | 13.93 |
| 318.0 | 13.98 | | | 184 | 7.45 | 330.1 | 13.30 | 309.6 | 13.37 | 349.2 | 14.14 |
| 323.2 | 14.15 | 78 | 1.635 | 189 | 7.78 | | | 310.2 | 13.36 | 349.2 | 14.36 |
| i | | | 4 | 195 | 8.11 | DATA | SET 100 | 311.0 | 13.34 | 362.0 | 14.79 |
| DATA S | **6 L3 | DATA | ET 98* | 200 | 8.41 | | | 311.3 | 13.31 | 374.8 | 15.22 |
| | | | | 205 | 8.69 | 4 | 0.0811 | 311.9 | 13.29 | 387.5 | 15.64 |
| 297.4 | 12.64 | 77.6 | 1.77 | 211 | 9.02 | 23 | 0.0811 | 312.2 | 13.27 | 400.3 | 16.07 |
| 305.3 | 12.78 | 85.9 | 2.10 | 217 | 9.35 | 40 | 0.16 | 313.0 | 13.27 | 417.4 | 16.72 |
| 1.95 | c/ . 71 | 5.26 | 2.51 | 222 | 9.62 | 51 | 0.25 | 313.4 | 13.28 | 434.4 | 17.36 |
| 2.705 2.905 | 12.72 | 106.3 | 10.5 | 227 | 9.90 | 3 3 | 0.41 | 314.2 | 13.30 | 451.5 | 17.79 |
| | 07.11 | 0.011 | | 233 232 | 10.23 | 6 | 80°0 | 6.CTC | 55.61 57 51 | 400.0 | 10.01 |
| 9.00 | 12.58 | 0.611 | 2 C | 467 440 | 10.01 | 4 C | c/ . n | 9./1C | 13.40 | 7.104 | 00.61 |
| 310.3 | 12.49 | 127.2 | 4.06 | 249 | 00 11 | 8 | 1.22 | 0.110 | 14.01 | 1.115 | 20.70 |
| 311.4 | 12.54 | 130.5 | 4.28 | 254 | 11.25 | 93 | 1.47 | DATA SI | ET 102* | 540.9 | 22.08 |
| 312.4 | 12.57 | 140.4 | 4.83 | 259 | 11.47 | 66 | 1.72 | | | 562.2 | 22.93 |
| 313.5 | 12.57 | | | 265 | 11.72 | 106 | 2.04 | 8.5 | 0.21 | 592.0 | 24.43 |
| 314.5 | 12.62 | DATA S | ET 994 | 271 | 11.94 | 114 | 2.54 | 21.3 | 0.21 | 604.7 | 25.29 |
| | | | | 276 | 12.19 | 126 | 3.18* | 34.1 | 0.21 | 630.3 | 26.36 |
| IS VIV | CL 95* | 4.19 | 1.04 | 282 | 12.39 | 134 | 3.67* | 46.9 | 0.22 | 664.3 | 27.86 |
| | | 10.3 | 1.04 | 290 | 12.61 | 139 | 3.97 | 64.0 | 0.43 | 685.6 | 28.93 |
| 9.606 | 12.21 | 17.0 | 1.02 | 293 | 12.69 | 148 | 4.52* | 68.2 | 0.65 | 719.7 | 30.43 |
| 8.605 | 12.52 | 24.2 | 1.03 | 295 | 12.72 | 159 | 5.21* | 85.3 | 1.08 | 749.5 | 31.93 |
| 2.00 B | 12 K7 | 33.2 61 0 | 90°T | 2.962 | 12.82 | 1/1 | 5.98 | 93.8 | 1.50 | 18/.8 | 33.86 |
| 110.1 | 12.45 | 41.0 | 1.15 | 270.2 | 12.84 | 101 | 6.69 7 2.7 | 100.0 | 1.93 | 813.5 477 A | 12.2E |
| | | •••• | ~ | 477.4 | 14.00 | 176 | | | 00.14 | | 1.47 |

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| T p | DATA SET 112 | 5.9 12.366 | 9.9 12.430 | 4.7 12.506 | 6.2 12.518 | 7.7 12.531 | 8.8 12.531 | 9.9 12.506 | 1.0 12.381 | 2.5 12.381 | 2.9 12.406 | 4.0 12.431 | 5.1 12.482 | 5.8 12.482 | 7.0 12.507 | 8.1 12.558 | 2.5 12.709 | 7.7 12.860 | 2.8 31.037 | 8.0 13.239 | 3.5 13.403 | 4.3 13.491 | | DATA SET 113 | | 7.0 12.152 | 9.2 12.215 | 1.8 12.290 | 5.1 12.391 | 9.2 12.480 | 4.3 12.581 | 5.5 12.606 | 6.9 12.619 | 7.7 12.619 | 8.8 12.607 | 9.2 12.594 | 9.9 12.582 | 0.6 12.557 | 0.7 12.481 | 1.4 12.481 | 2.1 12.481 | 2.5 12.507 | 2 9 12 512 | A.0 12.544 | 4.0 4 4. 7 1.7 5.87 | | | cca.21 6.0 |
|-----|----------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-------------|------------|------------|------------|------------|------------|------------|------------|------------|--------------------|---------|--------------|---------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|----------------|------------|------------------------|----------|-------|------------|
| م | ont.)* | .91 29. | .91 29 | .79 30 | .92 30 | .17 30 | .30 06. | .42 30 | .68 31 | .81 31: | .06 31: | 31/ | 31 | 31 | .4 31 | .2 31 | .0 32: | .8 32 | .6 33: | .4 33(| .231 343 | .124 34/ | .079 | .0960 | .175 | .316 28 | .519 28 | .784 29 | .111 29 | .500 29 | 30 | 11* 30 | 30 | .38 30 | .42 30 | .81 30 | .25 30 | .69 31(| .96 31 | .35 31 | .39 31 | . 36 | .16 | 19 | 10. | | | 170 |
| Т | DATA SET 109(c | 311.5 12 | 315.3 12 | 320.4 12 | 328.1 12 | 330.6 13 | 335.7 13 | 339.5 13 | 347.2 13 | 351.0 13 | 356.1 14 | | DATA SET 11 | | 300 14 | 400 19 | 500 24 | 600 28 | 700 33 | 800 38 | 900 43 | 1000 48 | 1100 53 | 1200 58 | 1300 63 | 1400 68 | 1500 73 | 1600 78 | 1700 84 | 1800 89 | | DATA SET 1 | | 89.4 1 | 110.0 2 | 134.5 3 | 172.2 6 | 204.0 8 | 240.0 10 | 266.3 12 | 290.7 13 | 316.9 13 | 227 6 16 | 367 6 15 | 100 C 16 | 01 (.766 | | |
| φ | 107(cont.)* | 13.86 | 13.86 | 13.99 | 14.25 | 14.44 | | SET 108* | | 2.01 | 2.28 | 2.98 | 3.50 | 4.47 | 6.93 | 8.59 | 10.43 | 11.49 | 12.80 | 13.07 | 13.24 | 13.51 | 13.50 | 13.50 | 13.68 | 13.94 | 14.29 | | SET 109* | | 5.44 | 5.82 | 6.58 | 7.33 | 8.09 | 8.60 | 9.23 | 9.87 | 10.62 | 11.13 | 11.51 | 12.15 | 10 27 | 13 40 | 17 25 | C0.21 | 12.00 | 12.91 |
| Т | DATA SET | 318.3 | 319.6 | 320.2 | 327.3 | 332.5 | | DATA | | 100.0 | 105.2 | 122.8 | 135.0 | 145.6 | 182.4 | 208.7 | 238.5 | 254.3 | 278.9 | 285.9 | 294.7 | 301.7 | 308.7 | 319.2 | 324.5 | 329.8 | 338.5 | | DATA | | 164.8 | 168.6 | 181.3 | 194.1 | 204.3 | 214.5 | 224.7 | 237.4 | 248.9 | 260.4 | 270.6 | 280.8 | 0.007 7 190 | 1.102 | 1 206 | 1.042 | 7.105 | 9./06 |
| ٩ | 106(cont.) | 39.30 | 45.38 | 47.41 | 51.21 | 55.51 | 62.86 | 65.64 | 70.96 | 77.04 | 81.85 | 83.62 | 85.90 | 86.91 | 88.68 | 90.46 | 93.24 | 94.00 | 94.51 | 95.52 | | ET 107* | 1 | 12.77 | 13.41 | 13.54 | 13.67 | 13.60 | 13.73 | 13.73 | 13.80 | 13.80 | 13.86 | 13.86 | 13.86 | 13.93 | 13.86 | 13.86 | 13.93 | 13.86 | 13.86 | 11.86 | 11 74 | 71.11 | 71. CT | 4/ · CT | 13.80 | 13.86 |
| T | DATA SET | 850.4 | 944.8 | 982.7 | 1046 | 1121 | 1235 | 1270 | 1354 | 1449 | 1524 | 1543 | 1575 | 1587 | 1612 | 1637 | 1675 | 1688 | 1700 | 1707 | | DATA S | | 273.2 | 288.0 | 291.2 | 292.5 | 294.4 | 294.4 | 296.4 | 298.3 | 300.2 | 301.5 | 302.8 | 304.1 | 304.7 | 306.0 | 307.3 | 308.0 | 309.2 | 311.2 | 312.5 | 312 5 | 1 211 | 1.110 | 0.010 | 1.010 | 316.4 |
| d | 04(cont.)* | 13.81 | 13.71 | 13.71 | 13.52 | 13.71 | 14.37 | 15.12 | 1 | ET 105* | | 0.10 | 0.83 | 12.49 | | ET 106 | | 1.29* | 2.05 | 2.81* | 4.07 | \$.09 * | 6.35 | 7.36 | 8.38* | 9.14 | *06.6 | 10.66 | 11.16* | 12.18* | 12.68* | 13.19 | 13.70* | 14.20* | 13.70 | 14.21* | 14.46 | 14.97* | 15.73 | 16.49 | 17,00# | 17.51 | 18 77 | 76.35 | 11.11 | 00.02 | 50.45 | c/.cc |
| T | DATA SET 1 | 303.8 | 307.7 | 310.6 | 313.5 | 318.4 | 335.8 | 359.1 | | DATA SI | | 20 | 11 | 273 | | DATA SI | | 93.5 | 112.5 | 125.1 | 150.3 | 162.9 | 169.1 | 194.3 | 213.2 | 219.5 | 225.8 | 244.8 | 251.0 | 269.9 | 276.2 | 295.2 | 301.4 | 307.7 | 307.8 | 326.8 | 4.055 | 345.7 | 364.6 | 389.9 | 196.2 | 415.2 | C | 1.042 | 1.001 | 0'010 | 0/3.0 | 181.0 |
| d | 02(cont.) | 38.57 | 40.71 | 42.00 | 43.71 | 45.00 | 46.71 | | ET 103 | | 13.00* | 14.52 | 18.15 | 22.38 | 26.31 | 29.93 | 33.85 | 37.17 | 42.00 | 46.82 | 51.04 | 54.96 | 57.97 | 60.39 | | ET 104* | | 1.04 | 1.13 | 1.32 | 1.70 | 2.46 | 3.59 | 4.63 | 5.96 | 7.09 | 8.23 | 9.93 | 10.98 | 11.83 | 12.20 | 12.68 | 12.96 | 13.24 | | | 70.61 | 12.11 |
| F | DATA SET 1 | 885.7 | 915.5 | 949.6 | 979.4 | 1004.9 | 1034.7 | | DATA SI | | 298.6 | 368.6 | 460.7 | 560.0 | 641.0 | 722.0 | 795.5 | 861.8 | 953.7 | 1042.0 | 9.1111 | 1181.8 | 1236.9 | 1281.1 | | DATA SI | | 76.9 | 83.6 | 90.4 | 100.1 | 113.7 | 131.2 | 146.7 | 166.1 | 182.6 | 200.1 | 224.3 | 242.8 | 257.3 | 266.0 | 272.8 | 281.6 | 287.4 | 203.7 | 100 | 1.142 | v.w. |

* Not shown in figure.

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| TABLE 3. |

| - | ٩ | H | d | н | ٩ | Т | d | F | d | F | d |
|----------------|------------------|-------|---------|-----------------|------------|----------------|------------|----------------|------------|---------------|-----------------|
| DATA SET 1 | <u>13(cont.)</u> | DATA | SET 116 | DATA SET | 119(cont.) | DATA SET | 122(cont.) | DATA SET | 126(cont.) | DATA SET | 126(cont.) |
| 317.7 | 12.658 | 277.1 | 12.109 | 284.8 | 12.954 | 302.3 | 12.594 | 294.6 | 12.764 | 306.1 | 12.891 |
| 322.5 | 12.809 | 282.4 | 12.307 | 289.8 | 12.916 | 305.1 | 12.611 | 294.8 | 12.768 | 306.4 | 12.889 |
| 327.6 | 12.948 | 286.4 | 12.460 | 292.1 | 12.901 | 307.2 | 12.634 | 295.0 | 12.774 | 306.8 | 12.888 |
| 332.4 | 13.087 | 292.4 | 12.610 | 294.9 | 12.883 | 309.9 | 12.659 | 295.3 | 12.776 | 307.1 | 12.886 |
| 338.0 | 13.276 | 294.0 | 12.669 | 297.4 | 12.863 | | | 295.5 | 12.780 | 307.4 | 12.882 |
| 350.2 | 13.667 | 300.5 | 12.789 | 299.9 | 12.857 | DATA | ET 123 | 295.8 | 12.786 | 307.6 | 12.879 |
| | | 305.4 | 12.837 | 302.4 | 12.833 | | | 296.0 | 12.789 | 8.100 | 17.8/7 |
| DATA S | ET 114 | 307.8 | 12.829 | 304.9 | 12.810 | 274.4 | 12.471 | 296.3 | 12.795 | 308.1 | 12.8/5 |
| | | 310.4 | 12.789 | 307.2 | 12.786 | 279.7 | 12.502 | 296.5 | 12.800 | 308.3 | 12.873 |
| 304.5 | 12.633 | 311.8 | 12.632 | 310.0 | 12.751 | 284.6 | 12.522 | 296-8 | 12.804 | 308.6 | 12.867 |
| 305.4 | 12.648 | 312.0 | 12.646 | | | 289.7 | 122.21 | 0.162 | 12.808 | 308.9 | 12.862 |
| 307.1 | 12.665 | 312.8 | 12.661 | DATA | SET 120 | 292.2 | 792.21 | 2.162 | 12.815 | 2.906 | 208-21 22 21 |
| 308.1 | 12.002 | 31/.5 | 818.21 | 0 076 | 010 01 | 0.042 | 12.5/4 | C.182 | 010 CI | 5.905 2005 | 100.21 |
| 0.600 5 005 | 10 202 | 1.026 | 006.21 | 6.602 0.75 0 | 12.0/9 | 2.142 200 0 | 160.21 | 201 0 | 010.21 | 2.000 A | 170.21 |
| | (70.71 | | 117 | 0 100 | 710 11 | 207.62 | 17 664 | 100 | 770.71 | 0.60C | 740.71 |
| 310.6 | 070.21 | NALA | 711 130 | 0.902 | 010.21 | 9.105 | +co.1 | 2.062 200 k | 070.71 | 1.600 | 10.21 |
| 510.0 | 12.000 | | | 9.402 | C6/ 71 | | | 4.047 | 12.630 | 4.40c | CC0.71 |
| 311.1 | 12.497 | 271.5 | 12.274 | 292.3 | 12.790 | DATA | SET 124 | 298.7 | 12.834 | 310.0 | 12.830 |
| 311.7 | 12.497 | 277.4 | 12.453 | 294.8 | 12.796 | | | 299.0 | 12.838 | 310.0 | 12.826 |
| 312.1 | 12.514 | 282.4 | 12.610 | 297.4 | 12.795 | 274.4 | 12.528 | 299.2 | 12.843 | 310.2 | 12.819 |
| 312.6 | 12.520 | 290.0 | 12.804 | 299.9 | 12.781 | 279.7 | 12.571 | 299.4 | 12.845 | 310.2 | 12.815 |
| 312.6 | 12.523 | 294.5 | 12.888 | 302.4 | 12.781 | 284.6 | 12.577 | 299.6 | 12.850 | 310.3 | 12.810 |
| 313.0 | 12.540 | 300.5 | 12.954 | 304.9 | 12.775 | 290.1 | 12.599 | 299.9 | 12.852 | 310.3 | 12.807 |
| 314.1 | 12.577 | 305.4 | 12.947 | 307.7 | 12.751 | 292.2 | 12.605 | 300.1 | 12.854 | 310.5 | 12.803 |
| 315.1 | 12.620 | 308.0 | 12.917 | 310.0 | 12.727 | 294.5 | 12.611 | 300.4 | 12.859 | 310.5 | 12.796 |
| 316.1 | 12.646 | 310.4 | 12.837 | 312.5 | 12.701 | 297.3 | 12.619 | 300.9 | 12.863 | 310.6 | 12.792 |
| | | | | | | 302.3 | 12.648 | 301.2 | 12.866 | 310.6 | 12.790 |
| DATA S | ET 115 | DATA | SET 118 | DATA | SET 121 | 307.4 | 12.674 | 301.7 | 12.870 | 310.7 | 12.787 |
| | | | | | | 309.9 | 12.696 | 301.9 | 12.873 | 310.7 | 12.785 |
| 305.0 | 12.519 | 275.2 | 11.769 | 274.9 | 12.808 | | | 302.1 | 12.876 | 310.7 | 12.784 |
| 306.0 | 12.539 | 277.6 | 11.871 | 279.9 | 12.790 | DATA | ET 125 | 302.4 | 12.877 | 310.7 | 12.780 |
| 306.8 | 12.554 | 280.7 | 12.010 | 284.7 | 12.778 | | | 302.7 | 12.881 | 310.7 | 12.776 |
| 308.0 | 12.551 | 287.3 | 12.270 | 289.8 | 12.764 | 274.7 | 12.665 | 302.9 | 12.882 | 310.7 | 12.775 |
| 0.905 | 12.542 | 293.1 | 12.464 | 294.8 | 12.749 | 279.5 | 12.671 | 303.0 | 12.884 | 310.7 | 12.772 |
| 1.906 | 12.534 | 297.3 | 12.592 | 299.6 | 12.743 | 284.6 | 12.671 | 303.4 | 12.884 | 310.8 | 12.766 |
| 309.9 | 12.517 | 302.1 | 12.705 | 304.7 | 12.736 | 289.7 | 12.668 | 303.6 | 12.886 | 310.8 | 12.762 |
| 310.5 | 12.500 | 306.8 | 12.756 | 307.2 | 12.728 | 294.5 | 12.668 | 303.8 | 12.887 | 310.9 | 12.756 |
| 311.0 | 12.383 | 308.0 | 12.753 | | | 299.6 | 12.677 | 304.1 | 12.888 | 310.9 | 12.752 |
| 311.4 | 12.372 | 310.4 | 12.738 | DATA | SET 122 | 304.6 | 12.688 | 304.4 | 12.889 | 310.9 | 12.742 |
| 311.7 | 12.377 | 310.9 | 12.716 | | | 307.4 | 12.696 | 304.6 | 12.889 | 310.9 | 12.739 |
| 312.1 | 12.380 | | | 284.8 | 12.477 | | | 304.8 | 12.890 | 310.9 | 12.732 |
| 312.7 | 12.395 | DATA | SET 119 | 289.7 | 12.511 | DATA | ET 126 | 305.0 | 12.891 | 311.0 | 12.724 |
| 313.0 | 12.403 | | | 292.2 | 12.522 | | | 305.3 | 12.892 | 311.0 | 12.722 |
| 314.2 | 12.437 | 269.7 | 13.098 | 295.0 | 12.534 | 293.8 | 12.749 | 305.5 | 12.890 | 311.0 | 12.721 |
| 315.3 | 12.475 | 275.0 | 13.040 | 297.5 | 12.557 | 294.1 | 12.753 | 305.6 | 12.889 | 311.0 | 12.716 |
| 316.1 | 12.503 | 279.8 | 12.004 | 300.0 | 12.574 | 294.3 | 12.759 | 305.8 | 12.892 | 311.0 | 12.711 |

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|--------------|------------|---------------|------------|----------|-------------------|--------------|------------|----------|-------------------|-----------|------------|
| DATA SET | 126(cont.) | DATA SET | 127(cont.) | DATA SET | <u>127(cont.)</u> | DATA SET | 128(cont.) | DATA SET | <u>129(cont.)</u> | DATA SET | 131(cont.) |
| 311.1 | 12.707 | 305.0 | 12.732 | 311.2 | 12.671 | 3.86 | 0.10101 | 277.8 | 11.938 | 9.58 | 0.96180 |
| 311.0 | 12.700 | 305.2 | 12.737 | 311.3 | 12.666 | 4.22 | 0.10100 | 282.4 | 12.225 | 10.17 | 0.96180 |
| | 12.696 | 20.00 2015 | 12 744 | C.11C | 12.000 12.000 | 4./9 5 57 | 0.10102 | 1.102 | 12 416 | 10.92 | 0.96170 |
| 311.1 | 12.693 | 306.3 | 12.748 | 312.0 | 12.671 | 6.25 | 0.10105 | 291.6 | 12.416 | 11.37 | 0.96167 |
| 311.2 | 12.687 | 306.4 | 12.753 | 312.2 | 12.674 | 6.83 | 0.10110 | 298.6 | 12.606 | 11.82 | 0.96180 |
| 311.3 | 12.685 | 306.7 | 12.753 | 312.5 | 12.679 | | | 300.9 | 12.606 | 12.42 | 0.96180 |
| 511.3 | 12.681 | 306.9 | 12.756 | 312.7 | 12.684 | DATA | SET 129 | 305.5 | 12.510 | 13.17 | 0.96202 |
| 311.4 | 12.676 | 307.1 | 12.758 | 312.8 | 12.689 | | | 310.1 | 12.605 | 13.77 | 0.96210 |
| 311.3 | 12.675 | 307.4 | 12.759 | 313.0 | 12.692 | 4.68 | 0.861 | 314.7 | 12.700 | 14.68 | 0.96237 |
| 311.5 | 12.671 | 307.7 | 12.760 | 313.1 | 12.698 | 11.6 | 0.956 | 319.4 | 12.795 | 15.75 | 0.96290 |
| 311.6 | 12.670 | 307.9 | 12.762 | 313.4 | 12.703 | 20.8 | 0.859 | 321.7 | 12.891 | 16.06 | 0.96343 |
| 111.7 | 12.670 | 308.1 | 12.762 | 313.7 | 12.709 | 20.8 | 0.955 | 328.6 | 13.177 | | |
| 911.9 | 12.671 | 308.4 | 12.765 | 313.8 | 12.716 | 27.8 | 0.859 | i | | DATA | SET 132 |
| 912.0 | 12.0/2 | 308.6 | 12.765 | 314.2 | 12.726 | 30.1 | 0.954 | DATA | SET 130 | | |
| 312.0 | 12.0/3 | 308.9 | 12.763 | 314.4 | 12.732 | 39.3 | 0.953 | | | 1.65 | 0.86027 |
| 11216 | 12.0/4 | 309.1 | 12.763 | 314.6 | 12.737 | 48.5 | 1.047 | 219.7 | 12.154 | 2.09 | 0.86024 |
| 912.4 | 17.6/7 | 309.3 | 12.763 | 315.1 | 12.752 | 57.8 | 1.046 | 282.1 | 12.229 | 2.54 | 0.86021 |
| 512.5 | 12.680 | 309.5 | 12.762 | 315.4 | 12.757 | 69.3 | 1.333 | 288.0 | 12.342 | 2.83 | 0.86022 |
| 312.0 | 12.683 | 309.6 | 12.761 | 315.6 | 12.765 | 74.0 | 1.523 | 289.2 | 12.530 | 3.28 | 0.86022 |
| 312.7 | 12.685 | 309.9 | 12.761 | 315.8 | 12.772 | 78.6 | 1.714 | 293.9 | 12.568 | 3.57 | 0.86018 |
| 512.8 | 12.089 | 309.9 | 12.756 | 316.1 | 12.780 | 90.1 | 2.001 | 299.8 | 12.681 | 19.0 | 0.86012 |
| 312.9 | 12.691 | 310.0 | 12.754 | 316.3 | 12.788 | 99.4 | 2.382 | 305.6 | 12.737 | 5.35 | 0.86007 |
| 0.410 | 97/.71 | 1.015 | 5C/ . 71 | 316.6 | 12./94 | 106.3 | 2.273 | 510.3 | 12.699 | 5.0 10 | 16668.0 |
| 314.8 | 12.741 | 310.1 | 12.751 | 316.8 | 12.800 | 111.0 | 2.764 | 315.1 | 12.737 | 6.53 | 0.85990 |
| 314.8 | 12.748 | 310.3 | 12.749 | 317.0 | 12.808 | 115.6 | 3.147 | 315.1 | 12.775 | 6.8. | 0.85984 |
| 316./ | 12.799 | 310.3 | 12.747 | 317.3 | 12.815 | 120.2 | 3.338 | 319.8 | 12.906 | 7.42 | 0.85980 |
| 31/.0 | 12.806 | 310.3 | 12.745 | 318.3 | 12.844 | 129.5 | 3.719 | 324.5 | 13.094 | 7.57 | 0.85984 |
| 317.5 | 12.822 | 310.4 | 12.741 | 318.5 | 12.852 | 134.1 | 4.102 | 330.4 | 13.208 | 8.01 | 0.85971 |
| 11/16 | 12.829 | 310.6 | 12.739 | 318.7 | 12.861 | 138.8 | 4.293 | | | 9.05 | 0.85977 |
| 0.010 | 12.03/ | 310.6 | 12./35 | 318.9 | 12.869 | 148.0 | 4.867 | DATA | A SET 131 | 9.49 | 0.85969 |
| 1.026 | 906.21 | 310.6 | 12./32 | 319.3 | 12.875 | 159.6 | 5.536 | | 100.0 | 10.09 | 0.859// |
| 0.17A | 117 | 0.012 | 12./31 | 4.910 | 12.862 | 100.0 | 0110 | 4. 59 | 17596.0 | 17.11 | 0.6594/5 |
| VIUN | 171 171 | 9.01c | 97/.71 | 1.416 | 168.21 | 1.8/1 | 0.000 | 4.40 | 10020 0 | 02.11 | 0.05900 |
| | 01, 0, | 310.7 | 12./23 | | | 8.281 | 0.8/3 | 51.C | 0.90304 | 10.21 | 0.629.2 |
| 9.10C | 7/0.71 | 310.8 | 12.720 | DATA | V SET 128 | 187.4 | 7.362 | 0.43 | 0.96298 | 13.50 | 01858.0 |
| 9.105 | 12.6/9 | 310.8 | 12.716 | | | 201.3 | 7.925 | 5.74 | 0.96317 | 13.80 | 0.86012 |
| 301.9 | 12.685 | 310.9 | 12.709 | 1.51 | 0.10106 | 203.7 | 8.308 | 6.02 | 0.96284 | 14.39 | 0.86021 |
| 302.1 | 12.689 | 311.0 | 12.703 | 1.77 | 0.10105 | 208.3 | 8.498 | 6.76 | 0.96260 | 14.84 | 0.86036 |
| 302.4 | 12.694 | 311.0 | 12.694 | 2.05 | 0.10105 | 217.6 | 9.072 | 7.21 | 0.96250 | | |
| 302.6 | 12.699 | 311.0 | 12.692 | 2.33 | 0.10104 | 229.1 | 9.645 | 7.50 | 0.96239 | DATA | SET 133 |
| 303.1 | 12.706 | 311.0 | 12.686 | 2.47 | 0.10103 | 238.4 | 10.315 | 7.95 | 0.96237 | | |
| 303.3 | 12.706 | 311.0 | 12.681 | 2.78 | 0.10102 | 247.7 | 10.888 | 8.10 | 0.96222 | 1.97 | 0.79508 |
| 303.6 | 12.711 | 311.1 | 12.677 | 3.01 | 0.10102 | 257.0 | 11.079 | 8.39 | 0.96197 | 2.56 | 0.67552 |
| 303.8 | 12.715 | 311.1 | 12.674 | 3.24 | 0.10101 | 266.2 | 11.556 | 8.99 | 0.96201 | 2.56 | 0.60725 |
| 1.406 | 12./30 | 311.2 | 12.673 | 3.40 | 0.10101 | 270.8 | 11.748 | 9.58 | 0.96170 | 2.86 | 0.46648 |
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| TABLE 3. |

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|----------|----------------|------------|--------------------|----------|--------------------|----------|------------|----------|------------|----------|------------|
| DATA SE | [133(cont.) | DATA SET 1 | 1 36(cont.) | DATA SET | 1 39(cont.) | DATA SET | 142(cont.) | DATA SET | 145(cont.) | DATA SET | [46(cont.) |
| 3.30 | 0.37245 | 121.4 | 1.141 | 313.9 | 6.676 | 311.3 | 12.816 | 299.4 | 12.725 | 311.8 | 12.687 |
| 4.20 | 0.34839 | 123.9 | 1.307 | 317.6 | 6.722 | 313.0 | 12.622 | 299.9 | 12.739 | 311.9 | 12.661 |
| 4.79 | 0.18398 | 126.3 | 1.426 | 320.0 | 6.814 | 320.8 | 12.958 | 301.0 | 12.777 | 311.9 | 12.648 |
| 5.70 | 0.39417 | 128.8 | 1.736 | 322.5 | 6.929 | 326.4 | 13.151 | 301.7 | 12.777 | 312.9 | 12.661 |
| | 0. /9188 | 130.0 | 1.9/3 | 326.0 | 1.06/ | - | | 302.4 | 12.790 | 316.7 | 12.790 |
| | T.26000 | 130.6 | 2.140 | DATA C | 071 140 | DATA | SET 143 | 303.2 | 12.816 | 318.5 | 12.854 |
| | | | | ALA S | 140 | | | 304.0 | 12.816 | | |
| DATA S | 134 | DATA S | ET 13/ | 101 | 1 17B | 76.1 | 0.929 | 305.4 | 12.841 | DATA S | ET 147 |
| | | | | C'101 | 0/077 | 1.02 | 1.4U/ | 6.105 | 17.841 | 1 | |
| 102.0 | 16/11 | 103.2 | 1.825 | 103.8 | 2.4/3 | 0.99.0 | 1.794 | 309.0 | 12.829 | 295.2 | 12.609 |
| 5.501 | 109.1 | 1.01 | 1.900 | 0.01 | 44C.2 | 123.6 | 3.239 | 310.0 | 12.816 | 297.1 | 12.674 |
| 100.0 | 1.697 | 1.101 | 2.100 | 100.3 | 2.039 | 1/5.6 | 6.376 | 310.6 | 12.803 | 299.0 | 12.725 |
| | 142.1 | 0.701 | 477.7 | 0.001 | 06/ 7 | 6.022 | 210.6 | 311.2 | 12./90 | 300.1 | 12.751 |
| 0.111 | 1.900 | 0.111 | 2.31/ | 111.3 | 276.2 | 275.0 | 12.003 | 311.4 | 12.700 | 303.0 | 12.803 |
| 113.8 | 2.034 | 113.5 | 2.411 | 0.611 | 3.091 | 311.3 | 12.764 | 311.5 | 12.738 | 305.2 | 12.829 |
| 110.4 | 161.2 | 116.7 | 2.598 | 116.9 | 3.115 | 312.4 | 12.570 | 311.7 | 12.661 | 307.5 | 12.841 |
| 1.9.1 | 2.291 | 119.3 | 2.785 | 118.8 | 3.138 | 320.8 | 12.958 | 312.7 | 12.635 | 309.6 | 12.816 |
| 120.4 | 2.409 | | | 122.5 | 3.281 | 327.5 | 13.151 | 313.4 | 12.661 | 311.8 | 12.700 |
| 124.3 | 2.572 | DATA S | ET 138 | 122.5 | 3.376 | | | 313.8 | 12.674 | | |
| 130.2 | 2.852 | | | 123.8 | 3.447 | DATA 5 | IET 144 | 314.2 | 12.700 | DATA S | ET 148 |
| | | 121.3 | 1.667 | 125.0 | 3.566 | | | 314.6 | 12.712 | | |
| DATA S | ET 135 | 122.0 | 1.739 | | | 296.1 | 12.880 | 315.2 | 12.725 | 299.4 | 12.545 |
| | | 124.0 | 1.788 | DATA S | ET 141 | 297.5 | 12.906 | 315.5 | 12.738 | 300.8 | 12.583 |
| 285.0 | 9.153 | 126.6 | 1.836 | | | 299.9 | 12.930 | 316.1 | 12.764 | 302.1 | 12.622 |
| 288.8 | 9.226 | 128.6 | 1.932 | 110.6 | 2.651 | 302.4 | 12.958 | 316.5 | 12.777 | 303.4 | 12.661 |
| 291.3 | 9.367 | 129.9 | 1.957 | 111.3 | 2.740 | 303.1 | 12.971 | 316.9 | 12.803 | 304.7 | 12.700 |
| 295.1 | 9.438 | 131.8 | 2.005 | 113.9 | 2.793 | 304.2 | 12.971 | 317.4 | 12.816 | 306.1 | 12.725 |
| 300.1 | 9.533 | 133.8 | 2.005 | 115.2 | 2.865 | 304.9 | 12.971 | 318.0 | 12.841 | 307.2 | 12.738 |
| 303.8 | 9.580 | 135.8 | 2.101 | 117.1 | 3.007 | 305.5 | 12.971 | | | 308.6 | 12.751 |
| 308.8 | 9.580 | 139.1 | 2.078 | 118.4 | 3.102 | 306.5 | 12.958 | DATA 5 | JET 146 | 309.9 | 12.751 |
| 308.8 | 9.532 | 140.4 | 2.294 | 119.7 | 3.197 | 307.4 | 12.958 | | | 310.6 | 12.751 |
| 312.6 | 9.461 | 141.7 | 2.391 | 122.3 | 3.269 | 308.3 | 12.945 | 300.0 | 12.919 | 311.1 | 12.738 |
| 315.1 | 9.532 | 145.0 | 2.511 | 123.6 | 3.411 | 309.2 | 12.919 | 301.9 | 12.932 | 311.3 | 12.725 |
| 317.6 | 9.627 | 148.3 | 2.559 | 126.2 | 3.625 | 311.3 | 12.880 | 302.9 | 12.945 | 311.4 | 12.712 |
| 322.6 | 9.722 | 150.2 | 2.632 | 130.0 | 3.791 | 312.3 | 12.622 | 303.8 | 12.958 | 311.8 | 12.648 |
| 326.3 | 9.793 | 152.9 | 2.704 | 130.7 | 3.886 | 314.1 | 12.687 | 304.8 | 12.958 | 311.9 | 12.635 |
| | | | | 132.6 | 4.028 | 314.9 | 12.725 | 306.5 | 12.971 | 312.3 | 12.635 |
| NAIA S | CL 130 | DATA SI | ET 139 | | | 315.9 | 12.751 | 307.7 | 12.958 | 313.1 | 12.648 |
| | | | | DATA S | ET 142 | 316.6 | 12.790 | 309.0 | 12.932 | 313.5 | 12.674 |
| 105.5 | 0.975 | 287.3 | 6.609 | | | 317.7 | 12.829 | 310.3 | 12.893 | 314.7 | 12.712 |
| 10/.3 | 0.975 | 290.9 | 6.655 | 76.1 | 0.929 | 319.6 | 12.893 | 310.9 | 12.854 | 317.1 | 12.816 |
| 8.601 | 0.999 | 295.8 | 6.701 | 0.0 | 1.988 | | | 1.110 | 12.829 | 318.7 | 12.854 |
| 111.6 | 0.999 | 299.4 | 6.746 | 124.7 | 3.536 | DATA S | ET 145 | 311.5 | 12.790 | 320.0 | 12.906 |
| 114.7 | 1.046 | 303.1 | 6.793 | 175.0 | 6.814 | | | 311.5 | 12.764 | | |
| 116.5 | 1.094 | 307.9 | 6.792 | 225.4 | 10.041 | 297.8 | 12.687 | 311.6 | 12.751 | | |
| 119.6 | 1.117 | 312.7 | 6.723 | 275.6 | 12.390 | 298.6 | 12.712 | 311.7 | 12.725 | | |
| | | | | | | | | | | | |
| * Not sh | own in figure. | | | | | | | | | | |

| F | d | F | Q | F | م | F | ď | T | ٩ | T | σ |
|-----------|-----------------|----------|----------------|----------------|------------|--------------------|-----------------|-------------|--------------|--------------|--------|
| DATA S | ET 149 | DATA SET | 151 (cont.) | DATA | SET 153 | DATA SET 1. | <u> (cont.)</u> | DATA SET 1. | 55(cont.) | DATA S | ET 157 |
| 299.1 | 12.725 | 163.6 | 5.273 | 32.5 | 0.0370 | 233.2 | 6.96 5 | 232.4 | 6.58 | 216.1 | 6.79 |
| 304.4 | 12.829 | 174.3 | 5.716 | 0.04 A AA | 0.062 | 0.121 0.72 0 | 81.7 | 236.0 | 0.82 7.07 | 228.4 | 1.8.1 |
| 307.0 | 12.854 | 178.5 | 5.852 | 49.8 | 0.123 | 247.1 | 7.61 | 247.3 | 7.23 | 252.3 | 9.83 |
| 309.6 | 12.829 | 183.9 | 6.049 | 55.2 | 0.172 | 251.4 | 7.83 | 252.6 | 7.48 | 263.9 | 10.65 |
| | | 193.5 | 6.209 | 59.5 | 0.259 | 256.7 | 8.06 | 256.9 | 7.70 | 274.0 | 11.40 |
| DATA | SET 150 | 198.9 | 6.344 | 63.8 | 0.370 | 262.0 | 8.28 | 262.2 | 7.92 | 280.5 | 11.87 |
| 2.4 | 0.0149 | 207.6 | 6.209 | 74.5 | 0.591 | 271.6 | 8.2U 8.75 | DATA S | SET 156 . | 286.3 | 12.13 |
| 4.2 | 0.0149 | 213.0 | 6.320 | 83.1 | 0.788 | 275.8 | 9.02 | | | 292.1 | 12.43 |
| 20.4 | 0.0157 | 218.3 | 6.517 | 84.1 | 0.899 | | | 70.2 | 0.505 | 295.7 | 12.52 |
| 78 | 0.0939 | 221.5 | 6.677 | 88.4 | 1.12 | DATA | ET 155 | 16.6 | 0.727 | 297.8 | 12.56 |
| DATA (| 267 151 | 221.0 | 6.936 7 005 | 93.7 | 1.26 | | 000 0 | 83.0 | 0.949 | 300.0 | 12.65 |
| VIUN | 101 101 | 7777 | 960.1 | 98.0 | 1.39 | 4.6C | 0.320 | 89.4 | 1.17 | 306.5 | 12.60 |
| 11.4 | 0.0616 | DATA C | 65T 153 | 112 0 | 9C.1 | 1.09 | 0.394 | 1.56 | 1.3/ | 308.6 | 12.60 |
| 9.73 | 0.0616 | WTIN | 717 176 | 118.4 | 1.86 | 1.60 | 0.127 | 113.0 | 1.72 | 320.0 | 00 11 |
| 15.1 | 0.0616 | 59.5 | 0.283 | 122.7 | 1.92 | 83.0 | 0.949 | 118.4 | 1.79 | 131.0 | 13.47 |
| 20.6 | 0.0616 | 64.8 | 0.394 | 129.1 | 2.12 | 89.4 | 1.17 | 128.1 | 2.08 | | |
| 24.9 | 0.0616 | 70.2 | 0.505 | 133.4 | 2.30 | 92.6 | 1.39 | 133.4 | 2.30 | DATA S | ET 158 |
| 29.2 | 0.0616 | 74.5 | 0.616 | 144.1 | 2.66 | 0.69 | 1.53 | 138.7 | 2.48 | | |
| 34.6 | 0.0862 | 75.5 | 0.702 | 149.4 | 2.83 | 0.92 | 1.61 | 144.1 | 2.66 | 298.5 | 12.712 |
| 0.04 | 0.123 | 78.8 | 0.788 | 154.7 | 3.06 | 103.2 | 1.84 | 149.4 | 2.83 | 299.6 | 12.720 |
| 47.4 | 0.148 | 82.0 | 0.702 | 159.0 | 3.24 | 108.6 | 2.08 | 152.6 | 3.02 | 300.6 | 12.742 |
| | 7/1.0 | 5.70t | 1.946 | 164.3 | 3.41 | 113.9 | 2.33 | 157.9 | 3.19 | 301.7 | 12.765 |
| 1.00 | 662.U | 113.9 | 2.193 | 168.6 | 3.63 | 118.1 | 2.55 | 163.3 | 3.41 | 302.8 | 12.789 |
| | 0.2.0 9.54 0 | 110.1 | 2.4LJ | 1.111 | 4.04 | C.621 | 2.11 | 168.6 | 5.03 202 | 304.0 | 12.809 |
| 10.0 | 0.616 | 0 001 | 2.297 2.027 | C.COI | 07.4 | 178.8 | 09.7 | 1/3.9 | 50.7 | 305.0 | 128.21 |
| 73.4 | 0.727 | 1 881 | 2.003 | 10/ 01 | 4.40 | 134.1 | 2.10 | 119.2 | 4.0/ | 306.0 | 12.843 |
| 77.6 | 0.899 | 138.4 | 3.289 | 7.941 | 4.00 | 1 1 1 1 1 | 3.29 | 0.401 | 4.40 | 307.4 207 | 12.045 |
| 84.0 | 1.121 | 144.8 | 3.462 | 202.7 | 5.06 | 1.941 | 1.51 | 194.7 | 49-4 | 208.40 | 12.853 |
| 89.4 | 1.281 | 149.1 | 3.622 | 209.1 | 5.31 | 153.5 | 3.46 | 198.4 | 4.84 | 308.8 | 12.853 |
| 93.7 | 1.528 | 153.4 | 3.683 | 217.6 | 5.73 | 158.9 | 3.57 | 203.8 | 5.06 | 309.3 | 12.849 |
| 100.0 | 1.749 | 158.8 | 3.622 | 222.9 | 5.94 | 163.1 | 3.73 | 208.0 | 5.28 | 309.7 | 12.845 |
| 104.3 | 1.971 | 164.2 | 3.794 | | | 173.8 | 4.15 | 212.3 | 5.47 | 309.9 | 12.845 |
| 108.5 | 2.242 | 173.8 | 4.152 | DATA SI | ST 154 | 179.1 | 4.35 | 217.6 | 5.69 | 310.5 | 12.837 |
| 8.511 | 2.20 | 180.2 | 4.349 | | | 183.4 | 4.56 | 222.9 | 5.89 | 311.0 | 12.831 |
| 7.021 | 179.2 | 184.5 | 4.570 | 188.2 | 6.07 | 187.6 | 4.82 | 227.2 | 6.11 | 311.2 | 12.823 |
| 4.47T | 3.043 | 198.3 | 5.174 | 192.5 | 6.18 | 194.0 | 4.98 | 232.5 | 6.27 | 311.5 | 12.805 |
| 9.071 | 165.6 | 202.6 | 5.359 | 197.9 | 6.23 | 198.3 | 5.09 | 236.8 | 6.47 | 311.9 | 12.791 |
| 0.4c1 | 770.C | 6.102 | 190.0 | 2.202 | 0.21 | 203.7 | 5.31 | 241.0 | 6.71 | 312.0 | 12.787 |
| 3 991 | 0000.C | 1.212 | 8//.0 | 8.802 | /0.0 | 207.9 | 5.58 | 247.4 | 6.94 | 312.2 | 12.763 |
| 148.8 | 4 447 | a | 212.0 | 5 715 5 715 | 01.0 | 7.717 | | 1.102 | (. LJ | 312.3 | (7/.71 |
| 156.2 | 4.780 | 0.111 | P01-0 | C./12 | 00 | 0.012 | | 0./02 | 1.32 | 9.216 | 61/-71 |
| 159.4 | 5.002 | | | 776 0 | 00 A 70 | 1.122 | 01.0 | 5.202 | PC .1 | 312.9 | A[/.7] |
| | | | | | | 7.177 | 00.0 | | | | |
| * Not sho | wn in figure. | | | | | | | | | | |

| , | a | T | ٩ | t. | ٩ | т | ٥ | ÷ | ٩ | н | ď |
|------------|-----------|----------|------------|----------|------------|------------|-----------|----------|------------|----------|------------|
| DATA SET 1 | 58(cont.) | DATA SET | 160(cont.) | DATA SET | 160(cont.) | DATA SET 1 | 61(cont.) | DATA SET | 161(cont.) | DATA SET | 162(cont.) |
| 313.0 | 12.727 | 302.65 | 12.689 | 311.25 | 12.680 | 304.65 | 12.716 | 311.10 | 12.599 | 308.77 | 12.737 |
| 313.3 | 12.735 | 302.80 | 12.692 | 311.33 | 12.679 | 304.76 | 12.718 | 311.22 | 12.596 | 308.89 | 12.735 |
| 1.616 | 10.21 | 202.205 | 12.696 | 87.115 | 12.675 | 10. 205 | 12.721 | 311.56 | 12.596 | 309.08 | 12.600 |
| 314.8 | 12.771 | 303.37 | 12.698 | 311.55 | 12.673 | 305.33 | 12.722 | 311.63 | 12.598 | 309.23 | 12.734 |
| 115.4 | 12.799 | 303.75 | 12.702 | 311.74 | 12.668 | 305.48 | 12.722 | 311.78 | 12.600 | 309.34 | 12.726 |
| 0.716 | 12.838 | 303.94 | 12.704 | 79.116 | 12.664 | 305.67 | 12.724 | 311.90 | 12.602 | 309.38 | 12.724 |
| 318.2 | 12.854 | 304.20 | 12.706 | 312.16 | 12.662 | 305.86 | 12.725 | 312.08 | 12.607 | 309.50 | 12.722 |
| 318.9 | 12.878 | 304.43 | 12.707 | 312.27 | 12.660 | 306.09 | 12.726 | 312.20 | 12.610 | 309.57 | 12.719 |
| 319.4 | 12.888 | 304.66 | 12.710 | 312.39 | 12.659 | 306.39 | 12.727 | 312.31 | 12.612 | 309.65 | 12.717 |
| 319.8 | 12.906 | 304.84 | 12.712 | 312.50 | 12.659 | 306.62 | 12.727 | 312.46 | 12.616 | 309.72 | 12.714 |
| | | 305.00 | 12.713 | 312.62 | 12.659 | 306.92 | 12.728 | 312.54 | 12.620 | 309.72 | 12.712 |
| DATA | ET 139 | 305.22 | 12.714 | 312.77 | 12.658 | 307.34 | 12.728 | 312.69 | 12.623 | 309.80 | 12.709 |
| | | 305.45 | 12.715 | 313.07 | 12.658 | 307.71 | 12,726 | 312.84 | 12.629 | 309.88 | 12.706 |
| 193.0 | 10.331 | 305.68 | 12.717 | 313.26 | 12.659 | 307.87 | 12.726 | 312.95 | 12.632 | 309.95 | 12.702 |
| 193.8 | 10.331 | 305.83 | 12.718 | 313.60 | 12.663 | 308.09 | 12.724 | 313.18 | 12.638 | 309.99 | 12.697 |
| 212.6 | 10.834 | 305.94 | 12.718 | 313.90 | 12.666 | 308.24 | 12.724 | 313.37 | 12.643 | 310.03 | 12.694 |
| 232.3 | 11.278 | 306.17 | 12.719 | 313.98 | 12.668 | 308.40 | 12.722 | 313.52 | 12.648 | 310.11 | 12.690 |
| 232.8 | 11.231 | 306.36 | 12.720 | 314.09 | 12.669 | 308.62 | 12.720 | | | 310.18 | 12.687 |
| 252.8 | 11.558 | 306.51 | 12.721 | 314.28 | 12.672 | 308.81 | 12.717 | DATA | SET 162 | 310.22 | 12.682 |
| 252.8 | 11.582 | 306.66 | 12.721 | 314.36 | 12.673 | 309.00 | 12.715 | | | 310.26 | 12.678 |
| 272.9 | 11.699 | 306.85 | 12.721 | 314.47 | 12.675 | 309.12 | 12.713 | 304.15 | 12.733 | 310.30 | 12.674 |
| 278.0 | 11.664 | 307.00 | 12.721 | 314.51 | 12.677 | 309.23 | 12.710 | 304.19 | 12.734 | 310.34 | 12.670 |
| 283.1 | 11.629 | 307.23 | 12.722 | 314.66 | 12.678 | 309.34 | 12.707 | 304.53 | 12.737 | 310.37 | 12.667 |
| 292.1 | 11.710 | 307.46 | 12.721 | 314.73 | 12.680 | 309.42 | 12.704 | 304.68 | 12.738 | 310.37 | 12.663 |
| 302.3 | 11.921 | 307.76 | 12.721 | 314.85 | 12.682 | 309.50 | 12.702 | 305.06 | 12.740 | 310.45 | 12.655 |
| 302.8 | 11.909 | 308.06 | 12.720 | 314.96 | 12.685 | 309.61 | 12.700 | 305.21 | 12.742 | 310.45 | 12.652 |
| 302.8 | 11.944 | 308.33 | 12.719 | | | 309.69 | 12.697 | 305.33 | 12.742 | 310.53 | 12.649 |
| 346.3 | 12.786 | 308.56 | 12.719 | DATA | SET 161 | 309.73 | 12.695 | 305.44 | 12.743 | 310.60 | 12.643 |
| 347.2 | 12.821 | 308.71 | 12.717 | | | 309.81 | 12.692 | 305.67 | 12.744 | 310.60 | 12.640 |
| | | 308.90 | 12.716 | 300.07 | 12.651 | 309.84 | 12.689 | 306.05 | 12.745 | 310.68 | 12.636 |
| DATA S | ET 160 | 309.16 | 12.714 | 300.49 | 12.658 | 309.92 | 12.687 | 306.27 | 12.745 | 310.68 | 12.632 |
| | | 309.31 | 12.713 | 300.75 | 12.663 | 310.00 | 12.682 | 306.35 | 12.746 | 310.76 | 12.628 |
| 300.23 | 12.655 | 309.54 | 12.710 | 301.02 | 12.668 | 310.11 | 12.677 | 306.50 | 12.746 | 310.83 | 12.624 |
| 300.42 | 12.658 | 309.66 | 12.709 | 301.24 | 12.671 | 310.15 | 12.672 | 306.73 | 12.746 | 310.91 | 12.623 |
| 300.57 | 12.660 | 309.81 | 12.708 | 301.47 | 12.676 | 310.26 | 12.668 | 307.03 | 12.746 | 310.99 | 12.616 |
| 300.72 | 12.662 | 309.88 | 12.705 | 301.74 | 12.679 | 310.26 | 12.663 | 307.11 | 12.746 | 311.06 | 12.612 |
| 300.91 | 12.665 | 310.00 | 12.704 | 302.15 | 12.685 | 310.34 | 12.658 | 307.33 | 12.746 | 311.10 | 12.609 |
| 301.06 | 12.668 | 310.26 | 12.701 | 302.30 | 12.688 | 310.41 | 12.651 | 307.56 | 12.745 | 311.21 | 12.608 |
| 301.25 | 12.671 | 310.34 | 12.699 | 302.53 | 12.692 | 310.49 | 12.646 | 307.67 | 12.745 | 311.33 | 12.606 |
| 301.40 | 12.674 | 310.41 | 12.698 | 302.83 | 12.695 | 310.57 | 12.641 | 307.75 | 12.744 | 311.56 | 12.606 |
| 301.55 | 12.675 | 310.53 | 12.696 | 303.10 | 12.699 | 310.64 | 12.631 | 307.83 | 12.744 | 311.63 | 12.609 |
| 301.74 | 12.678 | 310.76 | 12.690 | 303.29 | 12.701 | 310.68 | 12.626 | 307.90 | 12.743 | 311.74 | 12.611 |
| 301.93 | 12.681 | 310.87 | 12.688 | 303.51 | 12.704 | 310.76 | 12.619 | 308.05 | 12.743 | 311.82 | 12.613 |
| 302.12 | 12.683 | 310.95 | 12.687 | 303.66 | 12.706 | 310.83 | 12.613 | 308.36 | 12.741 | 311.97 | 12.617 |
| 302.35 | 12.685 | 311.02 | 12.684 | 304.27 | 12.702 | 310.91 | 12.608 | 308.47 | 12.740 | 312.08 | 12.620 |
| 302.50 | 12.688 | 311.14 | 12.683 | 304.38 | 12.714 | 310.99 | 12.603 | 308.55 | 12.739 | 312.16 | 12.621 |

. . .

* Not shown in figure.

| ٩ | cont.) | 2.624 2.626 | 2.628 | Z.634 2.638 | 2.642 | 2.650 | 2.658 2.658 2.662 | 163* | 0.101 | 0.102 | 0.107 | 0.126 | 0.209 | 0.314 | 0.690 | 0.983 | 2.37 | 3.35 | 4.92 - 48 | 9.01 | 9.51 | 0.99 | 3.90 | | | |
|---|------------|----------------|-------|----------------|-----------|-------|-------------------------|----------|-------|-------|-------|-------|-------|-------|-------|-------|------|----------|--------------|------|------|------|------|--|--|--|
| | A SET 162(| 12.20 | 12.52 | 12.56 I | 2.80 1 | | | DATA SET | | 0 | | | 00 | ••• | , 0 | 00 | | 5 | 0. | | 5.0 | a 12 | | | | |

3.2. Cobalt

There are 55 sets of experimental data available for the electrical resistivity of cobalt with purity higher than 99.9%. The information on specimen characterization and measurement condition for each of the data sets is given in table 5. The data sets are tabulated in table 6 and shown partially in figures 3 and 4.

Since cobalt is a transition element and is ferromagnetic, its electrical resistivity is expected to resemble those of nickel and iron. As it can be surmised from the size of the available data, the electrical resistivity of cobalt is not investigated as extensively as either that of iron or of nickel. Nonetheless, some features of the behavior of the electrical resistivity of iron and nickel have also been reported for cobalt, such as the T^2 variation in the temperature dependence of the electrical resistivity at low temperatures. The coefficient of this T^2 term becomes larger when measured in an applied magnetic field than when measured in the absence of an applied field [75].

Judging from the impurity analyses reported by some of the authors, cobalt specimens of purity higher than 99.999% are available commercially: Laubitz and Matsumura [76] (data set 43), White and Woods [77,21] (data sets 27, 28, 39), Kierspe et al. [78] (data set 16). However, there are wide disagreement between the reported residual resistivity ratios, even for specimens from the same manufacturer and having nearly the same impurities, as illustrated by the specimens of data sets 27 and 39. Since cobalt is nearly as strongly magnetic as iron (the spontaneous magnetization of 20.8 kG vs. 22 kG for iron), effects due to magnetic structure of specimens and due to the measuring current densities, etc. are expected to be significant. Unfortunately, there is very scarce information on these effects for cobalt specimens. In addition, the morphology of cobalt may have significant influence also. Even though the temperature of the α - β phase transformation of cobalt is greater than 700 K, this cph-fcc transformation is very sluggish, and the high-temperature fcc phase has been reported to persist at lower temperatures [79]. It is not unlikely for a specimen to contain a mixture of these two phases, depending on its thermal and mechanical history [76].

Amongst the available data for high-purity polycrystalline cobalt specimens, Laubitz and Matsumura [76] (data set 43) reported the highest residual resistance ratio ($\rho_{273} \text{ K}/\rho_{4} \text{ K}$) of 140 ± 10. The impurity analysis reported also indicated

that their specimen was one of the purest. For comparison, the residual resistance ratio of a whisker specimen by Marker et al. [75] (data set 19) was reported to be 388. There are available only a few data sets giving the electrical resistivity of high-purity cobalt over a temperature range extending from ~ 4 to 300 K: White and Woods [77] (data sets 27, 28), and Price and Williams [80] (data set 26). Aside from these data sets, White and Woods [21] (data set 39) reported data from 126 to 273 K, Semenenko et al. [81] (data set 3), Olsën-Bar [82] (data sets 4, 5), and Radhakrishna and Nielsen [83] (data set 9) reported data for low temperatures (<20 K) only. In addition, Loegel and Gautier [84] (data sets 47, 48) reported the temperature dependent part of the resistivity of specimens of unspecified purity for temperatures below 80 K. Most of these authors reported a T^2 dependence for the temperature dependent part of the resistivity for temperatures below 10 K. The coefficient of this T² component was reported to be 1.6 x $10^{-11} \Omega \text{ m K}^{-2}$ by White and Woods [77] and $\leq 1.0 \times 10^{-11} \Omega \text{ m K}^{-2}$ by Radhakrishna and Nielsen [83]. Loegel and Gautier [84] reported, together with a T^5 component, a coefficient of 1.06 x $10^{-11} \Omega \text{ m K}^{-2}$ for temperatures up to 30 K. Semenenko et al. [81] reported an additional T component for temperatures 1.4-4.2 K; however, Radhakrishna and Nielsen [83] concluded from their data that the T component, if present at all, was not significant. Marker et al. [75] also reported the T^2 dependence for their whisker specimen with a coefficient of 1.5 x $10^{-11} \Omega m K^{-2}$ in the temperature range 1.1-4.2 K.

The present analysis of the electrical resistivity of cobalt at low temperatures follows the same method as employed in the analysis of that of iron and nickel, i.e., by fitting the resistivity data to the expression

$$\rho = \rho_0 + \alpha T^2 + A \left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x^5 e^x}{(e^x - 1)^2} dx$$
(8)

However, because of the small number of available data sets and because of the apparent large deviation of the electrical resistivity of cobalt from the Mattheissen's rule, the coefficients α and A cannot be determined simultaneously with small uncertainties. Therefore, the value of α is taken to be 1.00 x $10^{-11} \Omega$ m K⁻², a value close to the mean of the coefficients reported by Radhakrishna and Nielsen [83] and by Loegel and Gautier [84]. Using a Debye

temperature of 445 K approximately as the value for $\theta_{\rm R}$, the value of A was determined from eq (8) with the data of White and Woods [77] (data sets 27, 28). A value of 70 x $10^{-8} \Omega {\rm m} {\rm K}^{-2}$ was obtained. With these values of α and A, the resistivity values calculated from eq (8) agree to within 2% with the experimental data for temperatures below ~ 25 K. For higher temperatures, the calculated values do not agree well with the experimental data, and therefore in the temperature range ~ 35 to 90 K, the recommended values were obtained by interpolating the low-temperature values calculated from eq (8) and the data of Laubitz and Matsumura [76] (data set 43).

Two data sets are available covering a very wide temperature range ($^{80-}$ 1700 K): by Laubitz and Matsumura [76] (data set 43) and by Kierspe et al. [78] (data set 16). Except for temperatures below ~ 200 K, where the latter data set appears to be in error, the agreement between these two data sets is within $\sim \pm 3\%$. The recommended values from 90 to 1700 K are therefore based on these, with more weight given to that of Laubitz and Matsumura, especially for temperatures below 250 K. In this temperature range, cobalt undergoes two transitions: one polymorphic at $\sqrt{715}$ K, from cph(α) to fcc(β), and one ferromagnetic-paramagnetic at ∿1395 K. The polymorphic transformation is martensitic and is very sluggish, due to the small associated free energy change. Thus the temperature range in which this transformation occurs has been reported to vary from about 660 K [85] (data set 14) to about 740 K [86] (data set 1), and thermal hysteresis is generally reported. The careful study of Laubitz and Matsumura [76] on a specimen which had been x-ray analyzed to contain no detectable fcc phase at room temperature showed that the range of transformation was about 703-710 K upon heating and about 686-693 K upon cooling (data sets 44, 45). The resistivity of the β phase is generally reported to be lower than that of the α phase. Kierspe et al. [78] did not report details of the transformation, even though their data appeared to have a strange behavior at the transformation, which occurred at $\sqrt{720} \pm 5.0$ K. These authors reported a temperature coefficient that shows a decrease ($\sqrt{30}$) at the transition, instead of the usual positive-negative-positive change in the temperature coefficient indicated by a number of the other works (see, e.g., Laubitz and Matsumura [76] (data sets 44, 45), Powell [85] (data sets 11-14), and Fraser et al. [86] (data sets 1, 2)). A possible reason for the behavior of the data of Kierspe et al. was that their specimen might have been heated or cooled at too fast a rate.

5.3

The α - β phase transition temperature of 715 K indicated in figures 3 and 4 is based actually on specific heat measurements. At temperatures above the α - β transition, the temperature coefficient reported by Kierspe et al. [78] showed a gradual rise to a flat maximum at \sim 1150 K, and decreased gradually again. It became almost constant at temperatures above \sim 1500 K. There was no sharp δ -function like maximum as in the cases of nickel and iron at the Curie temperature. This behavior of their data is consistent with the data of Laubitz and Matsumura [76] (data set 43), which appeared to have a change of slope at \sim 1250 K. At temperatures above the Curie temperature, the data of Seydel and Fucke [87] (data set 42) are in good agreement with those of Laubitz and Matsumura [76] and of Kierspe [78] and are also taken into account.

There are eight data sets for the electrical resistivity of molten cobalt [87-94] (data sets 7, 18, 40-42, 50-52). Of these, the data of Güntherodt et al. [92] (data set 41) and of Seydel and Fucke [87] (data set 42) agree to within $\pm 1\%$. In addition, their data for the solid phase at the melting point agree to within $\pm 1.5\%$ of the recommended value. The recommended values for the molten state are therefore based on their data. The linear temperature dependence of the electrical resistivity of molten cobalt was reported also by Ono and Yagi [89] (data set 18), and by Kita et al. [93] (data sets 50,51).

The recommended values both uncorrected and corrected for thermal expansion of the material are presented in table 4, while only the uncorrected values (except those for the liquid state) are shown in figures 3 and 4 along with the experimental data. The values are for polycrystalline cobalt of purity 99.99% or higher; however, those values for temperatures below 200 K are applicable only to cobalt having a residual resistivity of 0.0370 x $10^{-8} \Omega m$. The estimated uncertainty in the recommended values is about $\pm 5\%$ for the solid state and $\pm 7\%$ for the molten state.

As mentioned earlier, the electrical resistivity of cobalt appears to deviate from the Matthiessen's rule fairly large. For specimens with somewhat higher residual resistivities, the application of Matthiessen's rule is likely to underestimate the electrical resistivity by up to a few percent. For example, for the specimens of White and Woods [77] (data sets 27,28) which have residual resistivities of about 0.09 x $10^{-8} \Omega m$, Matthiessen's rule appears to be applicable for temperatures below ~15 K with resulting error less than -1%, but the error increases with temperature to -2% at ~20 K, -5% at ~35%, and -6% at 200 K and higher. For the specimen of Price and Williams [80] (data set 26) which has

a residual resistivity of $0.13 \times 10^{-8} \Omega$ m, the errors are approximately +2% at ~20 K, -6% from ~35 to 60 K, -5% at 100 K, and -4% from 200 to 300 K. Unfortunately, there are no available data sets for specimens of higher residual resistivity covering more or less continuously from low to room temperatures, so that a more extensive comparison could be made. The earlier measurement by McLennon et al. [50] (data set 30) on a specimen of residual resistivity 0.45 x $10^{-8} \Omega$ m indicates that the use of Mattheissen's rule yields an error of only -1% at 20.6 K, but the error jumps to -20% at 83 K and reduces to \sim -10% at 293 K. The more recent measurement by Wilkes [95] (data set 46), whose specimen has a residual resistivity of $\sim 0.17 \times 10^{-8} \Omega$ m, shows that the errors are -1% at ~ 77 K, +1% at \sim 200 K, and +1% at \sim 300 K. It is interesting to note that the total impurity content of this specimen, 0.08%, is more than ten times higher than that of the specimen of White and Woods [77] (data sets 27, 28). However, it has been determined by Laubitz and Matsumura [76] that the specimen of Wilkes contains approximately 33% of the fcc phase at room temperature. It is evident that the phase constitution of a specimen has significant influence on the resistivity of cobalt, especially below the α - β transition. The presence of the fcc phase below 7CO K is likely to lower the resistivity. On the other hand, the low-temperature cph phase is not likely to be stable at temperatures much higher than 700 K so that the higher temperature resistivity of cobalt of reasonable purity should not deviate by more than two or three percent from the recommended values.

The recommended values uncorrected for thermal expansion given in table 4 can be represented approximately by the following expressions to within $\pm 0.5\%$. 1-35 K:

$$\rho = 0.0370 + 1.00 \times 10^{-5} T^{2} + 70 \left(\frac{T}{445}\right)^{5} \int_{0}^{445/T} \frac{x^{5} e^{x}}{(e^{x} - 1)^{2}} dx$$
(19)

35-90 K:

$$\rho = 8.20 \times 10^{-2} - 5.261 \times 10^{-3} T + 1.477 \times 10^{-4} T^2 - 8.559 \times 10^{-8} T^3$$
(20)

90-700 K:

$$\rho = -9.98 \times 10^{-1} + 1.865 \times 10^{-2} \text{T} + 4.237 \times 10^{-6} \text{T}^2 + 3.777 \times 10^{-8} \text{T}^3$$
(21)
715-1250 K:

$$\rho = 31.71 - 1.0987 \times 10^{-1}T + 1.7872 \times 10^{-4}T^2 - 5.098 \times 10^{-8}T^3$$
(22)

1250-1400 K:

$$\rho = -117.61 + 1.8101 \times 10^{-1}T + 2.042 \times 10^{-8}T^2 - 1.773 \times 10^{-8}T^3$$
 (23)
1400-1767 K:

 $\rho = -342.15 + 7.2544 \times 10^{-1}T - 4.1393 \times 10^{-4}T^{2} + 8.201 \times 10^{-8}T^{3}$ (24) 1767-3000 K:

 $\rho = 94.80 + 1.128 \times 10^{-2} T$ (25)

It should be stressed that these expressions do not necessarily suggest any theoretical justification, and should be treated, most appropriately, as numerical aids only. It should also be understood that giving these expressions does not imply a recommendation for the temperature derivative of the electrical resistivity.

| TABLE | 4. | RECOMMENDED | VALUES | FOR | THE | ELECTRICAL | RESISTIVITY | OF | COBALT |
|-------|----|-------------|--------|-----|-----|------------|-------------|----|--------|
|-------|----|-------------|--------|-----|-----|------------|-------------|----|--------|

| Т | | þ | Т | | ρ |
|------|-------------|-----------|------|-------------|--------------------|
| | uncorrected | corrected | | uncorrected | corrected |
| 1 | 0.0370 | 0.0370 | 1100 | 59.26 | 60.05 |
| 4 | 0.0372 | 0.0372 | 1200 | 69.14 | 70.18 |
| 7 | 0.0375 | 0.0374 | 1300 | 78.79 | 80.11 |
| 10 | 0.0381 | 0.0380 | 1400 | 87.20 | 88.83 |
| 15 | 0.0396 | 0.0395 | 1500 | 91.46 | 93.34 |
| 20 | 0.0426 | 0.0425 | 1600 | 94.81 | 96.94 |
| 25 | 0.0481 | 0.0480 | 1700 | 97.76 | 100.15 |
| 30 | 0.0581 | 0.0580 | 1767 | 99.75(β) | 102.32(B) |
| 40 | 0.102 | 0.102 | 1767 | | 114.7b(l) |
| 50 | 0.178 | 0.178 | 1800 | | 115.1 ^b |
| 60 | 0.280 | 0.279 | 1900 | | 116.2 ^b |
| 70 | 0.408 | 0.407 | 2000 | | 117.4 ^b |
| 80 | 0.563 | 0.562 | 2100 | | 118.5 ⁰ |
| 90 | 0.742 | 0.740 | 2200 | | 119.6 |
| 100 | 0.947 | 0.945 | 2300 | | 120.7 |
| 150 | 2.02 | 2.02 | 2400 | | 121.9 ^b |
| 200 | 3.20 | 3.20 | 2500 | | 123.0 ^b |
| 250 | 4.52 | 4.52 | 2600 | | 124.1 ⁶ |
| 273 | 5.18 | 5.18 | 2700 | | 125.2 ^b |
| 293 | 5.78 | 5.78 | 2800 | | 126.4 |
| 300 | 6.00 | 6.00 | 2900 | | 127.5 ^b |
| 350 | 7.67 | 7.67 | 3000 | | 128.6 |
| 400 | 9.56 | 9.57 | | | |
| 500 | 14.11 | 14.15 | | | |
| 600 | 19.88 | 19.97 | | | |
| 700 | 27.09(α) | 27.25(α) | | | |
| 715 | 25.89(β) | 26.07(β) | | | |
| 800 | 32.09 | 32.36 | | | |
| 900 | 40.43 | 40.83 | | | |
| 1000 | 49.58 | 50.15 | | | |

[Temperature, T, K; Electrical Resistivity, ρ , $10^{-8} \Omega m$]

^a The values are for polycrystalline cobalt of purity 99.99% or higher, but those below 200 K are applicable only to cobalt having a residual resistivity of 0.0370 x $10^{-8} \Omega m$. The columns headed uncorrected and corrected refer to values uncorrected and corrected for thermal expansion, respectively. Solid line separating tabular values indicates solid to liquid state transformation, while dotted line indicates solid phase transition.

 α : cph; β : fcc.

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Provisional value.





99.9 pure; 99.5 Co + Ni, 0.07 Ni, 0.005 Fe, 0.001 Cu, 0.005 S, and 0.008 C by chemical analysis; <0.001 Ag, Al, B, Be, Ca, Cr, Hg, Mg, Mn₂ Mo, Pb, Sb, and Zn each by spectrographical analysis; 8.99 x 10° 40.2, $c_{24} \times 10^{-6} N_{23}$ and 1.9 x 10⁻⁰ Hz for specimen hot rolled to 0.127 cm (0.050 in.); 1.47 x 10⁻³ 02, 1.19 x 10⁻³ N2, and 4.3 x 10⁻⁶ Hz for specimen hot tolled to 0.127 cm (0.050 in.) and cold rolled to 0.0762 cm (0.030 in.); 1.31 x 10⁻³ 02, 4.8 x 10⁻⁶ N2, and 3.9 x 10⁻⁶ Hz for specimen annealed at 1273 K after hot and cold rolling; gas im-purities determined by gas analysis; strip specimens from Sherrit Gordon Mines; prepared from powder; rolled to desired thickness, and annealed at 1203 K for 1 h; density 8.85 x 10⁻⁶ Kg m⁻³ N2, and 668 K upon cooling; TC 1394 K; data extracted from heating and 668 K $3 \times 6 \times 120$ mm; magnetized along the long axis of a solenoid producing magnetic fields up to 3000 0e; data extracted from figure. Spectroscopically pure wire; obtained from Johnson Matthey Co.; 0.1 mm 5 mm in diam; cross section of $\sqrt{0.30} \times 0.25 \text{ mm}^2$ and $\sqrt{35} \text{ mm}$ long; residual resistivity ratio, R(273 K)/R(0 K) 26.19; values calculated from reported R(T)/R(273 K) with $\rho(273 \text{ K}) = 5.57 \times 10^{-8} \Omega \text{ m}$, taken from Bridgman, P.W., Proc. Am. Acad. Arts Sci., $\underline{79}$, 149, 1940; measured with terrestial magnetic field compensated by means of Helmhdtz at approximately two thirds of the melting temperature by passing a current through it; Debye temperature = 385 K; values calculated from reported $\rho(T)/\rho(90 \text{ K})$, with $\rho(90 \text{ K}) = 0.744 \times 10^{-6} \Omega \text{ m}$, taken from in diam and 3 to 5 cm long; annealed for several hours in high vacuum Cobalt samples consist of an orthogonal parallelepipe with dimensions Pure; polycrystalline wire from Johnson Matthey Co.; 1 mm in diam and 99.9984 pure; specimens prepared by electric-spark cutting from rod $^{\rm 0.6}$ cm long; annealed at 1313 K for 3 h at a pressure less than 4 x 10^{-5} PA; samples were demagnetized and the earth's field were 98.5-99.0% pure; electrolytic cobalt; data extracted from figure. 99.82 Co, 0.12 C, 0.008 M1, 0.004 Fe, 0.002 Cu, and 0.001 Mn and each; measured by a direct-heating method. Composition (weight percent), Specifications and Remarks The above specimen; data extracted from cooling curve. Same as above. Data Set 43. coilds. Designation Name and Spectmen 325-1020 293-1020 4.2-20.2 4.2-20.4 1433-1940 888-1673 Range, K 1.4-4.2 374-895 1.3-6.4 Temp. Method Used < U c æ ŧ ۵ Year 1956 1956 1965 1965 1963 1965 1964 1964 1964 Sudovtsov, A.I., and Redhakrishna, P. and Kovenskiy, I.I. and Chevemushkina, A.V. and Vasil'eva, R.P. Fraser, R.W., Evans, D.J.I., and Volkenshtein, N.V. Semenenko, E.E., Turov, V.D., and (a) (a) Ellutin, V.P., Samsonov, G.V. Fraser, et al. Maurakh, M.A. Olsën-Bär, M. Olsën-Bär, M. Mackiw, V.N. Nielsen, M. Ref. ż 88 88 8 82 82 8 8 8 6 Data *5 * š ż 2 ھ 80 •

ვ MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF COBALT TABLE 5.

* Not shown in figure.

compensated; data extracted from figure.

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| Composition (weight percent), Specifications and Remarks | 99.97% pure; 0.951 cm in diam and 4.346 cm long; supplied by Metallurgy Division of the National Physical Laboratory; data obtained from figure; resistivity measured by passing a measured current both forward and reverse through the sample; and using thermocouples as potential leads. | Similar to the above specimen except heated to 973 K. | Similar to the above specimen except cooled from 973 to 293 K. | The above specimen heated up to 973 K again. | The above specimen except cooled from 973 to 293 K. | 99.7 pure; samples in wire form; annealed in an intert gas atmosphere consists of 92% He and 8% H for 2 h at ${\rm vlSO}$ K above the Curie temperature; values calculated from reported resistivity ratio, $\rho(T)/\rho(T_C)=87.45\times10^{-6}$ R m taken from Data Set 16. | 99.999 ⁺ pure, <0.0001 Ag, Al, Ca and Cu each, 0.0003 Fe and Si each, 0.0002 Mn and 0.0001 Mg; supplied by Koch-Light Laboratories Ltd., England; a non-compensated Thomson bridge is used; values from table. | 99.998 ⁺ pure with major impurities of 0.002 C, 0.0001 to 0.02 0_2 , 0.004 N ₂ , and 0.001 H ₂ ; amorphous specimen with a cross section of $\sqrt{5} \times 10 \text{ mm}^2$; supplied by Koch Light Laboratories Ltd.; resistance measured by a standard four-terminal technique using thick silver lands evaporated on to the substrated prior to mounting in the ultrahild h vacuum system; a 0.03% Fe in gold-chronnel thermocouple from Johnson Matthey Co. was damped to the surface of the substrate for temperature measurement from 4 to 500 K. | 99.9 ⁺ pure; in molten state in a vacuum induction furnace; values calculated from the reported equation $\rho(\mu\Lambda-cm) = \alpha T(^{\circ}C) + \beta$ with $\alpha = 0.0384$ and $\beta = 69.07$. | Cobalt whisker grown by the hydrogen reduction of CoBr ₂ at 673-773 K in a reducing atmosphere of argon; residual resistance ratio $R(295 \text{K})/R(4.2 \text{K}) = 388; data extracted from figure of R(T)/R(295 \text{K}) as function of square of temperature; reference value of \rho(295 \text{K}) = 5.8 \mu\Omega cm, taken from White and Woods, Phil. Trans. Roy. Soc., London, A251, 273, 1959; used to calculate resistivity.$ | 99.999 pure Co; 0.0250 N, 0.0190 O, <0.0010 C, <0.0003 S1, Mg and Fe each; determined by emission spectrograph and vacuum fusion analysis; samples connist of 0.025 cm thick strips cold rolled to 0.011 cm, cut to \sim 20 cm in length by 0.25 cm in width; supplied by Johnson Matthey Co.; the center of the hysteresis gap found at 690 K; resistivity was monitored by superimposing an ac voltage on the ramp and measuring differentially the ac voltage drop across the speciaen against an 0.010 R standard using a phase sensitive detertion; reproducibility of measurement 0.12. |
|--|--|---|--|--|---|--|---|---|--|--|---|
| Name and Specimen Designation | 1 | | | | | | | Bulk Co | | Co DIM 20 | Spectmen No. 13 |
| Temp. Range, K | 293-427 | 290-965 | 290-923 | 290-955 | 384-756 | 1032-1483 | 77-1673 | 273 | 1768-1898 | 1.1-4.2 | 299 |
| Me thod Used | * * | A, + | A,+ | A.+ | A, + | | + | + * ^ | ĸ | | 9 |
| Year | 1964 | 1964 | 1964 | 1964 | 1964 | 1969 | 1967 | 1972 | 1972 1977 | 1971 | 1973 |
| Author (s) | Powell, R.W. | Powell, R.W. | Powell, R.W. | Powell, R.W. | Powell, R.W. | Schröder, K. and Giannuzzi, A.J. | Kierspe, W., Kohlhass, R., and Gonska, H. | Bennett, M.R. and Wright, J.G. | Onc. Y. and Yagi, T. Onc. Y. | Marker, D.L., Reichardt, J.W., and Coleman, R.V. | Pleves, J.T. and Bachmann, K.J. |
| ¥ | 85 | 85 | 85 | 85 | 85 | 86 | 78 | 66 | 89 . 90 | 75 | 8 |
| Data Set No. | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 11 | 18 | 19 | 20 |

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| K Set | Zo. | Author (s) | Үеаг | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------|----------|--|------|----------------|-------------------|-------------------------------------|---|
| 214 | 100 | Plewes, J.T. and Bachmann, K.J. | 1973 | ۵ | 299 | Specimen No. 13 | Similar to the above specimen except heated to 573 K for 46 h after cold rolled, representing a fully recovered structure. |
| 22 | 10 | Plewes, J.T. and Bachmann, K.J. | 1973 | Ð | 299 | Specimen No. 13 | The above specimen after 100 heat cycles carried out in a diffusion- pumped vacuum system which could be evacuated to 1.33 x 10 ⁻⁵ PA. |
| 234 | 100 | Plewes, J.T. and Bachmann, K.J. | 1973 | ۵ | 299 | Specimen No. 11 | Similar to the above specimen except only cold rolled. |
| 244 | 100 | Plewes, J.T. and Bachmenn, K.J. | 1973 | D | 299 | Specimen No. 11 | The above specimen heated to 1073 K for 10 minutes representing a fully recrystallized structure. |
| 25 | 100 | Plewes, J.T. and Bachmann, K.J. | 1973 | ۵ | 299 | Specimen No. 11 | The above specimen after 100 heat cycles carried out in a diffusion-pumped vacuum system which could be evacuated to 1.33×10^{-8} PA. |
| 26 | Q | Price, D.C. and Williams, G. | 1973 | > | 4.2-292 | | 99.9985% pure; dimensions of 10 cm x 0.2 cm x 0.15 cm; supplied by Johnson Matthey Co.; annealed in vacuo for 2 h at 1173 K and then quenched; ideal resistivity ρ_1 were reported from 22 to 292 K; data from table, uncorrected for thermal expansion; total resistivity calculated from data of ideal resistivity by the relation $\rho(T) = \rho_1(T) + \rho(4.2 \text{ K})$; temperatures stabilized and measured to better than 0.5%; area to length ratio determined to within 0.5%. |
| 5 | " | White, G.K. and Woods, S.B. | 1957 | U | 4.2-286 | Col. a | Pure; 0.0002 S1, <0.0005 Fe, \sim 0.0001 A1, and <0.0001 Mg and Cu each; by spectrographic analysis; rod specimen 5 to 8 cm long and 2 mm in diam; supplied by Johnson Matchey Co.; annealed in vacuum for \sim 2 h at 973 K; residual resistance ratio $p(295 K)/p(4.2 K) = 65.36$; total resistivity calculated using $p = p_1 + p_0$; ideal resistivity p_1 ex- tracted from figure; measurement error $\sim \pm 12$. |
| 28 | " | White, G.K. and Woods, S.B. | 1957 | G | 4.2-279 | Col. b | The above specimen remounted in a second cryostat and resistivity and thermal conductivity determined together; residual resistance ratio $p(295 \text{ K})/p(4.2 \text{ K}) = 64.52$. |
| 29 | 101 | Tsoukalas, I.A. | 1974 | | 273-1378 | | 99.99 (nominal) pure; polycrystalline; dimension 1 x 5 x 0.1 cm ³ ; martensitic transformation at 660 K form hcp to fcc; values extracted from figure. |
| 8 | 8 | McLennan, J.C., Niven, C.D., and Wilhelm, J.O. | 1928 | | 2.5-293 | Cobalt(aged) | Pure; supplied by Belga American Trading Corp., New York; cut into strip and annealed in vacuum for 4 h at a dull red heat; values ex- tracted from table. |
| 31 | \$ | McLennan, J.C., et al. | 1928 | | 4.2-293 | Cobalt (unaged) | Similar to the above specimen, unannealed. |
| 32 | 102 | Meissner, V. | 1928 | | 1.4-273 | CoI (27) | Specimen annealed for 2.5 h at 600 K; 50 mm in length and 2.5 x 0.5 mm cross section; resistance ratio reported; reference value of $\rho(273) = 5.57 \ \mu\Omega$ cm, taken from Bridgman, P.W., Proc. Am. Acad. Arts Sci., 79, 149, 1940, used to calculate resistivity from resistance ratio. |
| Kot | shown | in figure. | | | | | |

| Composition (weight percent), Specifications and Remarks | Polycrystalline; ∿5 cm long, 0.025 cm diam; annealed, values ex from table. | Sample in sintered polycrystalline form; 0.5 mm in diam and 57.4 in length; specimen obtained from Heraeus, von A.E.G.; sample at at 773 K in vacuum for 2.5 h; measured by compensation method; tive resistance data reported; reference value of $\rho(273) = 5.57$ taken from Bridgman (Proc. Am. Acad. Arts Sci., <u>79</u> , 149, 1940), to calculate resistivity. | Pure; 0.05 Cr, 0.01 Mn and <0.05 Fe; dimension 12.5 mm in length 2.5 mm thick; obtained from Kahlb; sample melted in vacuum; mean by compensation method; reference value of $p(273) = 5.57 \mu\Omega$ cm, from Bridgman (Proc. Am. Acad. Arts Sci., 79, 149, 1940), used calculate resistivity. | 99.998 pure; specimen in rod form 15 cm long and 0.5 cm in diam supplied by Koch Light Laboratories, United Kingdom; sample hea electric current; the potential drop across the length of the u temperature region was measured with a Tinsley ac/dc coordinate tentiometer type 4580; current through the sample determined by suring the potential difference across a non-inductive standard resistor type 660 of 0.001 Ω in series with the specimen; value tracted from graph. | Similar to the above specimen except contains a total impurity tration of about 0.001% of Si, Ni, Cu, Fe, Mg and Ag; sample su by Johnson Matthey Co. | 99.7 pure; 3 mm in diam and 30 cm long; annealed in vacuum for at 1273, oven-cooled; measured in a vacuum of 4 x 10 ⁻⁴ mmHg; me ment error: 1-1.5% in resistivity and 0.1 K in temperature; mi of resistivity versus temperature reported to occur at 655 K up heating and 655 K upon cooling; values extracted from figure. | 99.999 pure; 0.0002 Si, 0.0005 Fe, \sim 0.0001 Al, and <0.0001 Mg a wire specimen 0.05 mm in diam and about 6 to 8 cm long, from Jo Matthey Co. (JM9484); annealed in vacuum at 973 K; Debye temper reported to be 380 K; residual resistance ratio $R(295 K)/R(0 K)$ values calculated from reported ideal resistivity, extracted fr graph, and reported $\rho_{\sigma} = 0.062 \times 10^{-8}$ Gm from Table 1. | 99.98 pure; electrolytic. |
|--|--|---|--|--|---|---|---|---------------------------|
| Name and Specimen Designation | | Co 2 | Co 3 | Spectmen 1 | Specimen 2 | | C 0 2 | |
| Temp. Range, K | 4.5,295 | 1.5-273 | 1.3-273 | 1158-1496 | 1213-1468 | 373-773 | 4.2-273 | 1923 |
| Method Used | ۷ | • | † | + - | 8 | | U | 6 |
| Year | 1972 | 1930 | 1930 | 1969 | 1969 | 1969 | 1959 | 1972 |
| Author (s) | Horak, J.A. and Blewitt, T.H. | Meissner, W. and Voigt, B. | Meissner, W. and Voigt, B. | Jain, S.C., Narayan, V., and Goel, T.C. | Jain, S.C., et al. | Kirichenko, P.I. | White, C.K. and Woods, S.B. | levin, E.S., |
| Ref. | 103 | 104 | 104 | 105 | 105 | 106 | 71 | 6 |
| | | | | | | ~ | • | 2 |

* Not shown in figure.

TABLE 5. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF COBALT Co (continued)

| Dete | | | | Method | Tent | Name and | |
|-------|-----------------|--|--------------|--------|-----------|-------------------------|--|
| કે કે | 2 | Author (s) | Year | Used | Range, K | Specimen Designation | Composition (weight percent), Specifications and Remarks |
| 7 | 2 110 | Güntherodt, N.J., Hauser, E., Künzi, H.U., and Müller, R. Mueller, R. | 1975 1976 | × | 1720-1854 | | 99.999 pure from Johnson Matthey Co.; measured by a four probe method in which the sample material was enclosed in an alumina tube with four protrusion serving as current and potential contacts. |
| 5 | 87 | Seydel, U. and Fucke, W. | 1977 | + | 1205-3108 | | 99.99 pure, 0.0007 Fe, 0.0005 Si, 0.0003 Cu, 0.0002 Ag and Ni, 0.0001 Al, Ca, Mg, and Sn each, <0.0001 Bl, Cr, and Mn each; measured by an exploding wire technique; measurement error 4%; smoothed values from curve; values corrected for thermal expansion. |
| Ş | 9 | Laubitz, M.J. and Matsumura, T. | 1973 | ۲ | 90-1700 | | 99.999 pure, 0.00070 C, 0.00060 Ni, 0.00050 0 ₂ , 0.00016 Fe, 0.00010 K, 0.00008 N ₂ , 0.00007 Na, 0.00006 Ka, Cr, and Cu each, 0.00002 Ga and S each, 0.00001 P, 0.000007 CI, 0.00006 Ca, Cr, and Cu each, 0.00002 Ng, and 0.000008 Ag and Pd each (at.X), by semiquantitative mass spectrographic analysis; from Metals Research Ltd., England; material originally rod shape V2 cm in diam and 20 cm long; polycrystalline; annealed at 1500 K for 4 h in a vacuum of 5 x 10 ⁻⁵ Torr; cooled at 100 K hr ⁻¹ , except in the range 710 to 670 K, where it is cooled at 0.5 K hr ⁻¹ ; residual resistance ratio 140 ± 10; density 8.831 x 10 ³ kg m ⁻³ at 293 K; grain size V0.1 cm; specimen trimmed to a nominal diam of 2 cm and length of 20 cm with no machining of the region on which measurements were made; one specimen trimmed to a nominal diam of 2 cm and length of 20 cm vitth or machining of the region on which measurements were made; one specimen trimmed to a nominal diam of 2 cm and length no change in residual resistivity ratio, and in ice point resistivity were detected; the second specimen 1 201 a second specimen, 1 cm in diam and 10 cm long were cut from the first and measured from 90 to 370 K; no change in residual resistivity ratio unchanged; but speciment geometry is changed; monothed values from table, these values are reported to be averages in the temperature range where the two measurements overlap; values uncorrected for thermal expansion; values above 1300 K had been ad- justed by 40.8% by the authors to avoid discontinuity in resistivity values between the large and the small specimen; meaurement error reported 0.5%; smoothed values from table. |
| 495 | 76 | Laubitz, M.J. and Matsumwra, T. | £791 | ۷ | 680-710 | | The smaller of the above specimens, measured after the high temperature measurements; measured while heating. |
| 45# | 76 | Laubitz, M.J. and Mataumuta, T. | 1973 | V | 685-715 | | The above measured while cooling. |
| 4 | 8 | Vilkes, K.E. | 1968 | < | 78-300 | | 99.92 pure, 0.040 Fe, 0.012 Ni, 0.004 C, 0.001 Ca, Cu and Si each, 0.0008 S, 0.0003 Al and Mn each, 0.0002 Mg, and 0.0001 Pb; rod specimen 1.000 cm in diam and 10.05 cm long; supplied by Centre D'Information on Cobalt, Brussels, Belgium; density 8.805 x 10 ³ kg m ³ at 296 K; values from table; residual resistivity ratio measured by M.J. Laubitz and T. Matsumura, Can. J. Phys., $\underline{S1}(2)$, 1247, 1973, to be 31, and reported to change to 48 after being "carefully reannealed". |

* Not shown in figure.

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والمرجع بالقادي والأرقاب فالمنافق وأقدائهم والمحادث والمتعارفة

| 474 484 49 1 | 1 | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--------------------|----|---|------|----------------|------------------|-------------------------------------|---|
| +8+ +6+ | 5 | Loegel, B. and Gautier, F. | 1973 | | 6.8-79 | | "Pure cobalt," no other details reported; only temperature dependent part of resistivity reported. |
| 1 67 | 1 | Loegel, B. and Gautier, F. | 1973 | | 5.6-33 | | Similar to the above. |
| | 6 | zinov'yev, V.F., Krentsia, R.P., Perova, I.N., and Gel'd, P.V. | 1968 | А, Я | 296-1730 | | 99.95 pure; 0.2 mm thick, 8 mm wide and 8 mm long; ground from rolled stock; annealed at 1200 K for 7 h under a pressure of 1 x 10^{-5} mmHg; $\rho(288 \text{ K})/\rho(4.2 \text{ K}) = 86; \alpha^{-\beta}$ transition reported at 703 K; measured by potentiometric method below 1330 K, and by rotating field method above 1400 K; hysteresis at $\alpha^{-\beta}$ transition reported but resistivity values given for heating only; uncertainty in temperature measurement 10-15 degrees. |
| \$ | 6 | Kita, T., Ohguchi, S., and Morita, Z. | 1978 | t | 1658-1888 | | 0.137 Fe, 0.09 Ni ₂ 0.017 Si, 0.012 Mn, 0.011 S, and 0.008 C; measured in a vacuum of 10 ⁴ Torr, with a four probe method in which the electrodes are of the same material as the specimen; data points are taken at temperatures in the following sequence: 1788, 1811, 1829, 1850, 1870, 1888, 1881, 1867, 1846, 1820, 1801, 1781, 1765, 1755, 1735, 1711, 1694, 1678 and 1658 K; values from table supplied by authors. |
| - 21* | 93 | Kita, Y., et al. | 1978 | + | 1764-1895 | | Same as the above, a second meit; temperature sequence: 1795, 1809, 1823, 1843, 1863, 1878, 1895, 1883, 1869, 1854, 1836, 1819, 1801, 1782, and 1764 K. |
| 52* | 94 | S ama rin, A.M. | 1962 | £ | 1767-2000 | | Measured by the rotating field method; apparatus calibrated with iron using resistivity value reported by R.W. Powell, Philos. Mag., 44, 772, 1953; resistivity value calculated from reported conductivity (1.12-0.228 x 10^{-3} T(C)) x 10^{8} Ω^{-1} ; upper temperature limit issued to be 2000 K. |
| 53* I(| 8 | Shimank, H. | 1914 | < | 20.2-273 | | Wire specimen 1-2 m long; resistivity values calculated from reported R(T)/R(273 K) ratio, with $\rho(273$ K) taken to be 5.178 x 10^{-6} fm. |
| н 8 | 8 | Thomas, J.G. and Mendoza, E. | 1952 | | 1.2,4.2 | | 99.95 pure, from New Metals and Chemical Ltd., 0.13 mm in diam; drawn x -ray show hcp structure; resistivity value calculated from reported R(T)/R(273 K) with p(273 K) taken to be 5.178 x 10^{-6} fm. |
| 55 I(| 8 | Thomas, J.G. and Mendoza, E. | 1952 | | 0.06-4.2 | | Similar to the above except annealed for 3 h in vacuo at 1273 K; con- tains a small amount of fcc atructure. |
| | | Freitoco 4a , E. | | | | | tains a small amount of icc structure. |

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* Not shown in figure.

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| COBALT |
| 40 |
| RESISTIVITY |
| ELECTRICAL |
| THE |
| ð |
| DATA |
| EXPERIMENTAL |
| TABLE 6. |

[Temperature, T, K; Electrical Resistivity, p, 10^{-6} Ω m]

| | Ċ | 8 | 8* | * | R . | * . | m | * | ģ | 3* | 6 | 1 * | 6 | *6 | . 00 | | . 4 | | 4 | | | , | و م | Š | 7 | 1 | 2 | *6 | | . 9 | 4 | 5* | | 8# | 0 | 5# | L L | ~ | 4 6 | 80 | | | . * | | | • •• | . 0 | 5 |
|---|---------------|-------------|--------|----------|---------|------------|-------------|-----------|-----------|----------|-----------|------------|-----------|-----------|----------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-------------|----------|----------|----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|----------|-----------|-----------|------------|-----------|-----------|-----------|------------|-----------|----------|--------|--------|--------------|
| ٩ | 12 (cont | 23.1 | 23.5 | 23.8 | 24.0 | 24.1 | 24.0 | 24.5 | 25.0 | 25.7 | 26.2 | 27.0 | 27.5 | 28.3 | 30.0 | | 1.15 | | 45.4 | | SET 13 | | 9.0 | 7.3 | 10.5 | 14.7 | 22.0 | 23.3 | 25.6 | 26.7 | 27.1 | 27.7 | 27.8 | 27.8 | 28.0 | 28.0 | 27.5 | 27.7 | 27.5 | 27.8 | 28.1 | 28.6 | 29.1 | 20.7 | 30.5 | 37.9 | 43.8 | 47.1 |
| F | DATA SET | 644 | 650 | 655 2 | 100 | 666 (2) | 1/9 | . 686 | 694 | 705 | 713 | 724 | 732 | 742 | 767 | 805 | 852 | | 576 | | NAIA | | 067 | 327 | 410 | 498 | 626 | 644 | 619 | 695 | 101 | 705 | 711 | 714 | 718 | 718 | 721 | 721 | 725 | 130 | 735 | 742 | 749 | 151 | 768 | 860 | 919 | 955 |
| a | ET 10 | 6.46 | 6.27* | 7.43 | 1.03 | 8.64 | 2.03 | 10.28 | 11.41 | 11.56 | | ET 11 | | 6.45 | 8.19 | 12.66 | 17.71 | 77 75 | C/.77 | 22.02 | 40.12 | 400.02 | 28.00 | 28.00 | 27.38 | 28.43 | 28.93 | 29.00* | 30.05 | 31.43 | 34.33 | 38.74 | 44.36 | 47.16 | | ET 12 | | 5.9 | 10.6 | 11.62 | 13.47 | 14.24 | 14.66 | 16.13 | 20.47 | 21.42 | 22.53 | |
| T | DATA S | 293 | 294 | 324 | 32/ | 306 | 4 65 | 399 | 424 | 427 | | DATA S | | 290 | 339 | 444 | 542 | 603 | 170 | | | | | 107 | 722 | 738 | 747 | 749 | 760 | 776 | 814 | 869 | 166 | 965 | | DATA S | } | 290 | 401 | 435 | 476 | 490 | 505 | 526 | 596 | 613 | 633 | |
| ٩ | ont.) | 108.6 | 104.3 | 110.3 | 2.11 | 6 | • | | 59.4 | 63.4 | 64.7 | 68.9 | 74.0 | 79.7 | 83.3 | 88.9 | 92.2 | | 0 423 | 110 | 271200 0 | 0+T/00-0 | 0.06/151 | 0.087151 | 0.087162 | 0.087168 | 0.087176 | 0.087187* | 0.087200* | 0.087212 | 0.087223* | 0.087238 | 0.087248* | 0.087263* | 0.087281* | 0.087302 | 0.087337* | 0.087355* | 0.087381 | 0.087400* | 0.087423* | 0.087445* | 0.087468* | 0.087497# | 0.087521 | 1 | | |
| Ŀ | DATA SET 7 (c | 1765 | 1773 | 1868 | 194U | | DAIA 351 | | 888 | 939 | 986 | 1073 | 1188 | 1379 | 1478 | 1576 | 1673 | | DATA | NUTV | 1 20 | 07.1 | T.49 | 1.67 | 1.87 | 2.12 | 2.31 | 2.49 | 2.74 | 2.96 | 3.16 | 3.34 | 3.56 | 3.75 | 3.96 | 4.22 | 4.61 | 4.82 | 5.11 | 5.28 | 5.49 | 5.69 | 5.88 | 6.16 | 6.36 | 1 | | |
| d | ser 5 | 0.1499 | 0.1500 | 0.1501 | 1001.0 | 20110 | PUCL-U | 0.1504 | 0.1505 | 0.1506 | 0.1507 | 0.1507 | 0.1508 | 0.1511 | 0.1512 | 0.1519 | 0.1547 | • | | 21 | a a | | | 11.7 | 13.3 | 15.6 | 16.8 | 18.0 | 18.9 | 19.8 | 20.6 | 21.8 | 24.3 | 25.8 | 27.1 | 28.6 | 30.3 | 31.8 | 34.6* | 38.2 | 39.7 | 42.5 | | 2 | 1 | 91.8 | 101.4 | |
| F | DATA | 4.16 | 98.4 | 5.22 | | 01.0 | 70.0 | 1.24 | 7.92 | 8.54 | 9.08 | 9.54 | 10.15 | 10.83 | 11.56 | 12.43 | 20.38 | | DATA CP | | 476 | 100 | 160 | | 496 | 529 | 546 | 580 | 592 | 612 | 630 | 649 | 690 | 712 | 733 | 752 | 764 | 789 | 815 | 851 | 870 | 895 | | DATA SET | | 1433 | 1685 | |
| ٩ | (cont.) | 50.0 | 53.7 | | C 130 1 | 0 313766 | CC/717-0 | 0.212750* | 0.212765* | 0.212773 | 0.212817* | 0.212815 | 0.212812* | 0.212831* | 0.212855 | 0.212868* | 0.212893* | 0.212912# | 0 2129444 | 0 717044 | 044717.0 | CBT 44 | 190 | | 0.1578 | 0.1578 | 0.1576 | 0.1579 | 0.1581 | 0.1581 | 0.1581 | 0.1581 | 0.1581 | 0.1565 | 0.1566 | 0.1585 | 0.1589 | 0.1584 | 0.1595 | 0.1584 | 0.1585 | 0.1589 | 0.1594 | 0.1600 | 0.1604 | 0.1612 | 0.1622 | |
| F | DATA SET 2 | 58 3 | 1020 | | | 17 1 | | 1.61 | 1.78 | 1.99 | 2.22 | 2.36 | 2.60 | 2.80 | 3.19 | 3.38 | 3.57 | 1 77 | | 0.4 1 | 07.4 | 1474 | VIVA | : | 4.17 | 4.96 | 5.24 | 5.86 | 6.52 | 6.99 | 7.41 | 7.78 | 8.21 | 8.61 | 90.08 | 10.50 | 11.29 | 11.66 | 12.26 | 12.40 | 13.35 | 14.11 | 14.88 | 16.08 | 16.75 | 18.85 | 20.22 | |
| ٩ | 1 1 | 6.3 | 8.0 | 8.6 | 7.21 | 14.8 | 0./T | 20.2 | 22.5 | 24.2 | 25.7 | 27.0 | 28.2 | 29.2 | 29.4 | 30.9 | 32.5* | 14.64 | 49 22 | 11 74 | 44.72 | | | 33./ | | ET 2 | | 8.0 | 9.8 | 12.2 | 14.8 | 17.6 | 20.2 | 22.5 | 23.7 | 24.4 | 25.7 | 26.7 | 27.7 | 28.6 | 30.5 | 32.5 | 34.6 | 37.6 | 41.7 | 45.4 | | w in floure. |
| F | DATA SI | 293 | 325.15 | 0/6 | 774 | 0/4 | 22 | 573 | 611 | 638 | 999 | 682 | 869 | 715 | 133 | 161 | 788 | 814 | 178 | | 500 | | .010 | 1020 | | DATA SI | | 325.15 | 370 | 422 | 476 | 525 | 573 | 611 | 638 | 499 | 683 | 200 | 716 | 733 | 761 | 788 | 814 | 847 | 895 | 935 | | # Mor aho |

Co (continued) EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF COBALT TABLE 6.

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| | | | | | and the state of t | | | | an and a statement of the state of the | | |
|--------------|------------------|--------------|-------------|------|--|---------|---------|----------|--|---------|---------|
| F | ٩ | - | ٩ | F | ٩ | F | a | + | ٩ | F | ٩ |
| DATA | SET 14 | DATA SET | r 15(cont.) | DATA | SET 17 | DATA S | ET 20 | DATA SET | 26(cont.) | DATA | SET 28 |
| 384 | 9.44 | 1428 | 89.72 | 273 | 5.6 | 299 | 6.90 | 131.8 | 1.7419 | 4.2 | 0.0907* |
| 458 | 12.39 | 1455 | 91.04 | | | | | 141.9 | 1.9810* | 12.91 | 0.0922 |
| 559 | 18.15 | 1458 | 91.21* | DATA | SET 18 | DATA SI | ET 21* | 156.3 | 2.3355 | 15.31 | 0.0933 |
| 5 | 21.05 | 1461 | 91.82* | | | | | 171.8 | 2.7038 | 18.07 | 0.0958* |
| 626 615 | 22.14* | 1483 | 92.17 | 1768 | 126.478 | 299 | 6.25 | 182.0 | 2.9524* | 21.53 | 0.0991 |
| 040 6 4 4 | | 1111 | 26 76 | 29/1 | 047./2T | | | 191.4 | 3.21/8 | 24-83 | 0.1048 |
| 808 9 | 00.62 1480 FC | NIN | 2E1 10 | 1808 | 128.UI4 | DATA S | ET 22 | 206.5 | 3.5/10 | 21.42 | 0.1122 |
| 599 | 24.02 | " | V V | 070T | 120.702 | 100 | . 71. | 4.C12 | 4.236U | 50.16 | 0621.0 |
| 667 | 24.004 | | 2.65 | 1868 | 120.18 | 667 | 47.0 | 196 | 2102 5 | 19 05 | 0 1707 |
| 699 | 23.92* | 223 | 3.84 | 1888 | 131.086 | DATA SI | ET 23* | 271.0 | 5.4120 | 53.95 | 0.2786 |
| 671 | 23.89 | 273 | 5.25 | 1898 | 131.470 | | | 292.4 | 6.1254* | 63.10 | 0.3804 |
| 673 | 23.85* | 323 | 6.81 | | | 299 | 6.91 | | | 68.55 | 0.4726 |
| 674 | 23.87* | 373 | 8.52 | DA | VTA SET 19 | | | DATA | SET 27 | 76.38 | 0.6047 |
| 676 | 23.91* | 423 | 10.50 | | | DATA SI | ET 24* | | ł | 88.31 | 0.7970 |
| 677 | 24.02* | 473 | 12.80 | 1.18 | 0.013658 | | | 4.2 | 0.0902 | 143.5 | 2.032 |
| 680 | 24.22 | 523 | 15.45 | 1.31 | 0.013668 | 299 | 6.48 | 11.56 | 0.0914 | 279.3 | 5.688 |
| 684 | 24.63* | 573 | 18.38 | 1.39 | 0.013668 | | | 12.74 | 0.0921 | | |
| 692 | 24.97 | 623 | 21.48 | 1.49 | 0.013675 | DATA S | ET 25 | 12.88 | *6160.0 | DATA SI | ET 29 |
| 60/ | 26.16 | 673 | 24.72 | 1.60 | 0.013680 | | | 14.59 | 0.0926 | | |
| 725 | 27.29 | 698 | 26.55 | 1.69 | 0.013684 | 299 | 6.58 | 15.49 | 0.0933* | 273 | 7.1 |
| 734 | 28.00 | 723 | 28.00 | 1.78 | 0.013688 | | | 16.07 | 0.0943* | 317 | 8.7 |
| 756 | 29.45 | 748 | 29.25 | 1.88 | 0.013693 | DATA | SET 26 | 16.83 | 0.0942* | 362 | 10.2 |
| | | 773 | 30.65 | 1.97 | 0.013698 | | | 18.20 | 0.0958 | 479 | 15.5 |
| DATA | ET 15 | 823 | 34.72 | 2.08 | 0.013705 | 4.2 | 0.1275 | 20.28 | 0.0974 | 549 | 18.7 |
| | | 873 | 39.05 | 2.19 | 0.013711 | 22.1 | 0.1328 | 22.03 | 8660.0 | 668 | 26.4 |
| 1032 | 58.24 | 923 | 43.66 | 2.28 | 0.013715 | 25.2 | 0.1441 | 26.24 | 0.1088 | 684 | 26.8 |
| 1049 | 58.85 | 973 | 48.20 | 2.40 | 0.013732 | 27.9 | 0.1516 | 28.91 | 0.1172* | 698 | 26.8 |
| 1074 | 60.87 | 1023 | 52.85 | 2.50 | 0.013728 | 31.8 | 0.1660 | 32.06 | 0.1295 | 711 | 26.8 |
| 1114 | 64.10 | 1073 | 57.92 | 2.59 | 0.013740 | 35.3 | 0.1788 | 34.91 | 0.1495* | 745 | 28.7 |
| 5511 | 68.56 | 1123 | 62.95 | 2.69 | 0.013746 | 38.7 | 0.1965 | 37.84 | 0.1664 | 111 | 32.4 |
| • | 66.J0 | 1173 | 68.20 | 2.80 | 0.013758 | 43.1 | 0.2208 | 54.83 | 0.2972 | 815 | 35.3 |
| 1/11 | c0.0/ | 1223 | /3.48 | 2.89 | 0.013765 | 48.5 | 0.2662 | 59.70 | 0.3461 | 843 | 38.1 |
| 1711 | 76.60 | 5/7T | (0.4) | 3.8 | 0.013//2 | 53.5 | 0.3203 | 64.27 | 0.4145 | 882 | 40.8 |
| 1755 | 10.07 | C7CT | 16.20 | 60°C | 0.013/80 | 1.00 | 4C46.U | C4./0 | 0.4208 | 016 | 4.3.2 |
| | | 0401 0401 | 17.08 | 91.E | 0.013790 | 65.3 | 0.4726 | 74.30 | 0.5655 | 960 | 48.6 |
| 1200 | 75.71 | 13/5 | 8/.45 | 3.29 | 0.013797 | 11.6 | 0.5660 | 84.33 | 0.7359 | 1065 | 59.2 |
| 1205 | 80.03× | 86FT | 89.17 | 3.40 | 0.013810 | 73.3 | 0.5974* | 91.62 | 0.8827 | 1159 | 69.1 |
| 6671 | 71.20 | 1423 | 90.60 | 3.50 | 0.013822 | 77.4 | 0.6547 | 105.9 | 1.184 | 1246 | 76.6 |
| 9161 | 83.86 | 1448 | 91.62 | 3.59 | 0.013834 | 81.3 | 0.7177 | 122.2 | 1.563 | 1315 | 82.4 |
| 1321 | 83.86* | 1473 | 92.65 | 3.69 | 0.013843 | 84.7 | 0.7791* | 162.6 | 2.506 | 1378 | 88.5 |
| 1340 | 86.05 | 1523 | 94.35 | 3.79 | 0.013859 | 89.7 | 0.8671* | 187.5 | 3.159 | | |
| 1370 | 87.45 | 1573 | 96.52 | 3.89 | 0.013867 | 93.8 | 0.9612* | 205.6 | 3.646 | DATA | SET 30 |
| 13/3 | 87.45 | 1623 | 98.17 | 3.99 | 0.013875 | 100.0 | 1.0694 | 224.4 | 4.136 | | |
| 1041 | 66.65 00.02 | 1673 | 99.95 | 4.09 | 0.013888 | 105.2 | 1.1966* | 243.2 | 4.640 | 2.5 | 0.45 |
| 767. | 70.0% | | | 4.15 | 0.013898 | 113.2 | 1.3298 | 264.9 | 5.314 | 4.2 | 0.45 |
| 474T | -71.40 | | | | | 122.2 | 1.5207 | 285.8 | 5.992 | 20.6 | 0.46 |

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* Not shown in figure.

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| Co (continued) |
|---------------------|
| OF COBALT |
| RESISTIVITY |
| ELECTRICAL |
| ON THE |
| DATA |
| EXPERIMENTAL |
| TABLE 6. |

| Image: product in the second state of the | F | ٩ | 6- | ٩ | н | ٩ | F | ٩ | | •d - d |
|---|----------|------------------|------|--------------|-------------|---------------|----------------|------------------|----------|-----------|
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | DATA SET | <u>36(cont.)</u> | DATA | SET 41 | DATA SET | 43(cont.) | DATA SET | 45(cont.)* | DATA SET | 47(cont.) |
| 138 77.4 173 9.4 900 9.2.9 9.2.0 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.9 2.4.30 9.0.0 9.2.0 2.4.30 9.0.0 9.2.0 2.4.30 9.0.0 9.2.0 2.4.30 9.0.0 9.2.0 2.4.30 9.0.0 | 1261 | 75.2 | 1720 | 95.8 | 800 | 32.056 | 690.8 | 24.786 | 41.1 | 0.0701 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1284 | 77.4 | 1746 | 94.8 of a | 906 0001 | 40.377 | 691.0 691.4 | 24.561 24.481 | 44.1 | 0.0998 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1338 | 81.3 | 1765 | 97.8 | 1100 | 59.259 | 692.0 | 24.348 | 50.6 | 0.118 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1356 | 83.6 | 1769 | 109.3 | 1200 | 69.116 | 693.0 | 24.308 | 50.6 | 0.132 |
| 100 15.4 1136 116.1 1300 72.3 64.4 7.46 1430 86.1 115.3 116.0 77.3 66.0 24.463 1430 86.1 115.3 116.0 77.3 66.0 24.463 1440 89.1 115.3 116.3 116.0 77.3 66.0 24.463 1440 89.1 113.3 115.3 116.3 116.0 77.3 66.0 24.463 1133 85.3 113.3 113.3 113.3 113.3 113.3 113.3 114.3 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 77.3 114.4 | 1372 | 83.6 | 1780 | 115.1 | 1250 | 73.995 | 694.0 | 24.348 | 78.6 | 0.507 |
| [4,2] [6,3] [1,4] <th[1,4]< th=""> [1,4] <th< td=""><td>1407</td><td>85.4</td><td>1784</td><td>116.1</td><td>1300</td><td>78.78</td><td>694.8</td><td>24.467</td><td></td><td></td></th<></th[1,4]<> | 1407 | 85.4 | 1784 | 116.1 | 1300 | 78.78 | 694.8 | 24.467 | | |
| 1134 66.5 113.5 1500 91.37 66.0 24.653 51.14 71.5 1006 89.4 116.3 1100 97.65 70.2 24.793 54.65 1006 89.4 116.3 1100 97.65 70.2 24.793 54.65 1111 76.3 1105 71.2 69.8 25.316 71.5 1111 76.3 1105 71.2 69.4 55.95 100.0 25.316 71.5 1111 85.3 115 91.9 69.4 55.95 100.1 25.366 81.1 1112 81.3 110.3 71.4 700.1 25.366 81.1 11.6 1112 81.3 110.3 110.3 111.4 700.1 25.366 81.1 11.6 1112 81.3 110.3 111.6 701.1 26.32 77.46 25.366 81.1 1113 81.3 100.3 55.493 70.1 27.28 22 | 1423 | 86.3 | 1811 | 114.3 | 1400 | 87.17 | 696.0 | 24.493 | DAT/ | SET 48* |
| 1470 88.1 184.4 115.3 1500 97.65 70.2 2.4.737 5.4 1066 89.2 16.3 1100 77.62 25.114 77.50 25.114 77.50 5.114 77.50 5.114 77.50 5.114 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.214 77.50 5.216 77.5 17.5 | 1434 | 86.5* | 1828 | 115.3 | 1500 | 91.37 | 698.0 | 24.625 | | ĺ |
| 1066 99.6* 155 16.3 1700 97.62 703.0 25.114 77.5 MA SET J MA SET J MA SET 42 MA SET 44 700.0 25.146 77.5 MA SET J 1303 73.2 693.4 25.213 130.0 7.5.66 8.1 1121 76.3 1327 82.4 693.2 25.493 7.6.6 8.1 1121 76.3 91.3 1472 82.4 693.2 25.493 7.1.4 0.653 111.5 1129 81.0 25.1 100.1 26.632 27.3.4 7.5.66 8.1 1129 81.0 27.5 65.32 27.44 103.2 6.17 27.44 27.4 27.4 1129 81.0 27.6 27.5 27.44 27.5 27.4 27.4 27.4 27.4 27.4 27.4 27.5 1120 121.2 70.1 26.52 27.44 27.4 27.4 <th27.2< th=""> <th27.2< th=""> <th27.2< th=""></th27.2<></th27.2<></th27.2<> | 1470 | 88.1 | 1844 | 115.3 | 1600 | 94.86 | 700.2 | 24.757 | 5.61 | 0.00018 |
| 1066 09.2 MAX SET 21 MAX SET 22 MAX SET 24 713 MAX SET 31 MAX SET 42 MAX SET 42 MAX SET 44 700.0 25.144 77.4 1212 7.13 7.13 7.13 7.13 7.13 7.14 7.15.4 7.366 7.14 1212 7.13 7.13 7.13 681.8 7.5.493 7.14 7.15.4 7.366 7.15 1223 7.13 1173 7.13 681.8 7.5.493 7.14 7.15.4 7.166 7.15 1123 85.1 1173 114.7 700.1 2.6.493 7.14 7.15.4 7.156 1123 81.0 7.14 700.1 2.6.473 7.13.2 7.14 7.04 7.14 <td>1488</td> <td>89.6*</td> <td>1854</td> <td>116.3</td> <td>1700</td> <td>97.62</td> <td>702.0</td> <td>24.903</td> <td>6.44</td> <td>0.00054</td> | 1488 | 89.6* | 1854 | 116.3 | 1700 | 97.62 | 702.0 | 24.903 | 6.44 | 0.00054 |
| MAK SET 3 MAK SET 42 MAK SET 42 MAK SET 42 MAK SET 44 77.4 52.546 77.5 1212 79.1 1227 92.1 1227 92.4 699.8 52.346 91.9 1224 85.5 1157 1227 85.4 100.0 55.246 84.1 1224 85.5 1163 10.3 85.493 77.44 0.655 118.3 1123 85.5 1163 100.8 699.1 56.493 77.46 0.655 118.3 1123 86.3 10.3 56.793 21.44 70.3 56.793 21.33 21.84 1133 86.30 21.3 118.7 70.11 56.835 21.44 21.56 22.44 21.56 22.44 21.57 22.44 21.56 22.44 21.57 22.44 21.56 22.44 22.46 22.46 22.46 22.46 22.44 22.44 22.44 22.44 22.44 22.44 22.44 22.44 22.44 | 1496 | 89.2 | | | | | 705.0 | 25.114 | 7.40 | 0.00065 |
| MAX SET 31 MAX SET 31 MAX SET 31 121 6.1 25.395 DAX E_{11} 25.966 B_{11} 1222 79.1 1327 82.4 99.7 25.395 DAX 81.4 9.5 1222 85.5 1561 99.7 56.97 56.939 77.44 0.655 21.7 1373 86.5 1651 10.7 100.3 690.7 26.999 77.44 0.655 21.7 1427 91.1 116.7 70.11 26.955 21.7 21.2 21.7 1427 21.96 117.0 70.11 26.955 27.2 22.2 2 | | | DATA | SET 42 | DATA | SET 44* | 707.0 | 25.246 | 7.57 | 0.00083 |
| 1217 1205 73.2 619.8 25.32 MAA SET 46 91.3 92.3 93.4 94.4 | DATA S | SET 37 | | | | | 715.4 | 25.866 | 8.13 | 0.00062 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | 1205 | 73.2 | 679.8 | 25.212 | | | 8.51 | 0.00079 |
| I242 79.1 I452 89.7 688.2 25.86 77.8 0.65 11.1 11294 82.5 165 97.9 56.59 17.8 0.65 12.1 11295 86.8 1763 114.7 700.8 699.1 26.559 12.3 5.23* 23.1 1467 91.1 118.7 701.1 26.652 27.32 5.23* 23.1 1468 92.1 118.7 701.1 26.632 27.34 23.13 21.6 1468 21.1 118.7 701.1 26.825 23.92 10.4* 31.2 1461 118.7 701.3 26.932 23.4 31.4 31.4 7 22.50 23.4 13.3 703.5 24.4 31.4 32.4 7 22.50 703.5 26.925 74.4 0.0033 32.4 7 22.55 704.5 26.463 77.41 0.0033 32.4 7 22.55 | 1213 | 76.3 | 1327 | 82.4 | 684.8 | 25.595 | DATA : | SET 46 | 9.56 | 0.0001 |
| 1284 82.5 1561 93.9 696.7 26.493 77.84 0.655 18.1 1172 88.5 1653 10.6 114.7 700.3 26.744 273.2 5.23* 23.1 1187 91.1 116.3 106.3 106.3 106.3 56.599 114.7 700.3 26.744 273.2 5.23* 23.1 1187 91.1 118.7 700.3 26.744 273.2 5.23* 23.1 118.7 701.7 26.959 120.7 701.7 26.955 7.3.2 23.1 23.1 117.0 701.7 26.955 703.5 26.955 7.4 23.2 23.2 23.1 117.1 28.0 2862 123.4 703.5 26.943 24.4 31.6 30.4 7 28.50 28.64 26.43 26.64 24.4 31.6 30.4 77.3 28.50 28.64 26.43 26.64 26.43 32.4 7 | 1242 | 1.97 | 1452 | 89.7 | 688.2 | 25.846 | | | 11.5 | 0.00127 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1284 | 82.5 | 1561 | 93.9 | 696.7 | 26.493 | 77.84 | 0.655 | 18.3 | 0.00368 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1323 | 85.5 | 1675 | 97.8 | 647.9 | 26.599 | 194.4 | 3.158 | 21.0 | 0.00512 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 6/E1 | 88.8 | 1763 | 100.8 | 1.999 | 26.652 | 273.2 | 5.23* | 22.0 | 0.00604 |
| 166 92.7 199 117.0 701.1 26.923 239.7 6.02* 24.7 373 15.00 2395 117.0 701.1 26.929 299.7 6.02* 24.3 373 15.70 2442 123.9 170.1 26.942 7 9.0 6.02* 24.4 30.4 373 15.70 2393 123.6 703.9 26.942 7 9.0 6.02* 30.4 573 15.70 286 123.6 703.9 26.407 7 9.0 6.07* 30.4 573 26.107 703.5 26.407 7.5.50 299.0 6.07* 30.4 773 28.50 303 129.3 706.0 25.763 6.75 0.000357 9.0 7 26.107 7.41 0.000357 9.0 9.0 9.0 766 1.512 90 0.74 7.64 0.000357 9.0 126 1.512 100.0 < | 1427 | 1.19 | 1763 | 114.7 | 2007 | 26.744 | 273.2 | 5.23* | 23.1 | 0.00801 |
| DATA SET 38 2131 118.7 701.7 26.955 299.7 6.03* 21.3 373 8.00 2344 122.2 703.1 26.955 7 0.0^{+} 23.4 373 12.60 236 123.6 703.1 26.955 7 0.0^{+} 23.4 573 12.60 2384 127.2 703.1 26.955 7 0.0^{+} 23.4 733 15.70 2869 127.2 703.3 26.478 0.0^{+} 24.7 773 28.50 706.0 25.6478 76.478 D^{+} 0^{-} 0^{-} 773 28.50 706.1 25.6407 7.41 0.000357 296 973 28.6 706.0 25.6407 7.41 0.000357 296 9706.0 25.6407 7.41 7.06.0 25.6407 10.07 296 971 121.2 706.1 25.650 7.94 0.000033 395 16.1 | 1468 | 92.7 | 1959 | 117.0 | 701.1 | 26.823 | 273.2 | 5.26# | 24.7 | 0.00923 |
| Mrt SET 38 2295 120.1 703.5 56.95 29.7 6.00* 30.1 773 12.60 2584 123.9 703.5 56.955 7 | | | 1112 | 118.7 | 201.7 | 26.876 | 299.0 | 6.02* | 28.4 | 0.0196 |
| Mit Sec Sec <td>DATA</td> <td>SET 38</td> <td>2295</td> <td>120.7</td> <td>707.3</td> <td>26.929</td> <td>299.7</td> <td>6.04*</td> <td>30.4</td> <td>0.0273</td> | DATA | SET 38 | 2295 | 120.7 | 707.3 | 26.929 | 299.7 | 6.04* | 30.4 | 0.0273 |
| 373 8.00 236 12.6 703.5 5.942 T $p - p_0$ T 773 12.60 2718 125.6 703.5 26.478 DATA SET 4/2 $p - p_0$ T $p - p_0$ T 773 12.60 2718 125.6 703.5 26.107 6.75 0.000357 296 773 28.50 3057 129.3 706.6 25.550 7.41 0.000357 296 7 4.2 0.062 3057 129.3 706.4 25.550 7.41 0.000357 296 4.2 0.062 1.5112 90 0.744 710.0 25.510 9.56 0.000133 355 126 1.5112 90 0.744 710.0 25.497 10.7 0.00133 355 126 2.3112 100 0.354 704.4 0.00133 355 126 2.312 90 0.744 710.0 25.497 10.7 0.00133 | | | 2442 | 122.2 | 703.1 | 26.955 | | | 32.6 | 0.0314 |
| 473 12.60 2718 12.56 703.9 26.478 DATA SET 4/* DATA 773 15.70 2869 127.2 704.5 26.478 DATA SET 4/* DATA 773 15.70 2869 127.2 704.5 26.478 DATA DATA 773 28.50 305 129.3 706.4 25.630 7.41 0.000357 296 77.1 28.50 306 129.3 706.4 25.630 7.41 0.000357 296 4.2 0.662 25.550 704.0 0.000357 296 316 126 1.512 90 0.744 710.0 25.497 10.7 0.000383 366 126 2.312 100 0.939 10.7 25.497 10.7 0.000133 367 126 2.312 100.0 25.497 10.7 0.000133 366 126 2.312 100.0 25.497 10.7 0.00113 410 | 373 | 8.00 | 2584 | 123.9 | 703.5 | 26.942 | T | 0 - 0 | | |
| 573 15.70 2869 127.2 704.5 26.478 DATA SET 47* DATA 773 28.50 2982 127.2 704.5 26.478 DATA SET 47* DATA 773 28.50 3057 129.3 706.0 25.763 6.75 0.000357 296 773 28.50 3108 129.8 706.0 25.550 7.44 0.000357 296 4.2 0.062 DATA SET 43 707.2 25.550 7.44 0.000351 335 4.2 0.062 1.512 90 0.744 710.0 25.497 100.0 0.000381 335 126 1.512 90 0.744 710.0 25.497 100.0 0.000381 366 126 1.512 10 0.744 710.0 25.497 100.0 0.000181 366 128 1.512 10 0.744 710.0 25.497 100.7 0.000181 361 183 2.862 | 473 | 12.60 | 2718 | 125.6 | 703.9 | 26.862 | I | . | T | ٩ |
| 7/7 28.50 2982 128.4 705.3 26.107 6.75 0.000357 296 177 28.50 3057 129.3 706.0 25.5630 7.41 0.000357 296 126 $1.29.8$ 706.4 25.530 7.41 0.000357 296 4.2 0.062 90 774 707.2 25.550 7.41 0.000321 336 4.2 0.062 90 0.744 710.0 25.497 10.0 0.000984 366 126 1.512 90 0.744 710.0 25.497 10.7 0.000984 366 126 2.312 100 0.939 1.461 $D.7A$ 710.0 25.497 10.7 0.000984 366 126 2.312 1261 $D.7A$ 710.0 25.497 10.7 0.000113 410 190 2.312 1261 $D.25.452$ 0.0000984 <td< td=""><td>572</td><td>15.70</td><td>2869</td><td>127.2</td><td>704.5</td><td>26.478</td><td>DATA</td><td>SET 47*</td><td></td><td>L</td></td<> | 572 | 15.70 | 2869 | 127.2 | 704.5 | 26.478 | DATA | SET 47* | | L |
| 773 28.50 3057 129.3 706.0 25.763 6.75 0.000357 296 DATA SET 39 DATA SET 39 306 129.8 706.4 25.630 7.41 0.000357 296 4.2 DATA SET 39 DATA SET 43 706.4 25.550 7.41 0.000357 296 4.2 D .1062 DATA SET 43 706.0 25.550 7.41 0.000383 335 4.2 D .062 D .744 710.0 25.497 10.7 0.000983 355 126 1 .312 90 0 .744 710.0 25.497 10.7 0.000188 366 183 2 .862 12.61 D .747 710.0 25.497 10.7 0.00188 366 183 2 .862 12.61 D .744 710.0 25.497 10.7 0.00188 366 190 3 .214 6 .84.6 2 .5.497 10.7 0.00188 376 190 4 .4062 | 573 | 22.50 | 2007 | 128 6 | 502 | 26.107 | | | DATA SF | т 49 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | 1041 | | | 101-07 | 26.2 | 0 000167 | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 00.02 | 1000 | 129.5 | 0.00/ | co/.cz | | 100000 0 | 200 | |
| MAX SET 39 MAX SET 43 $0/1.2$ $2.5.50$ 1.34 0.000221 530 4.2 0.062 90 0.744 70.6 25.510 9.56 0.000983 355 126 1.512 90 0.744 710.0 25.497 10.7 0.000984 366 183 2.312 100 0.939 0.744 710.0 25.497 10.7 0.000984 366 190 3.052 125 1.461 $0.708.6$ 25.497 11.0 0.00161 556 230 3.052 125 1.461 $DATA$ SET $45*$ 12.6 0.00161 578 230 4.0022 25.018 0.542 0.516 0.00186 578 244 4.0022 250 4.527 685.4 25.515 0.00133 648 273 5.182 400 9.542 688.4 25.542 23.6 0.00133 677 < | | | 2102 | 8.41I | 100.4 | 050.02 | 14.7 | 1000000 | 067 | |
| 4.2 0.062 DATA SET 43 708.0 25.50 9.56 0.000963 550 126 1.512 90 0.744 710.0 25.497 10.0 0.000964 366 163 2.312 90 0.744 710.0 25.497 10.7 0.000964 366 163 2.312 100 0.939 0.744 710.0 25.497 10.7 0.000964 366 190 3.052 125 1.461 $DATA$ SET $45*$ 11.0 0.00161 556 230 4.062 2.018 $DATA$ SET $45*$ 12.6 0.00161 556 230 4.062 2.018 0.74 0.00186 578 244 4.062 2.500 4.527 685.4 25.515 0.00783 677 250 $4.982*$ 300 9.595 686.4 25.542 23.6 0.00173 648 273 5.182 300 9.595 688.4 25.545 20.7 | DATA | SET 39 | | | 7.10/ | 044.42 | +6./ | 170000.0 | 000 | 0 0 0 |
| 4.2 0.062 708.8 25.497 10.0 0.00094 366 126 1.512 90 0.744 710.0 25.497 10.0 0.000184 366 163 2.312 100 0.939 $DATA$ SET 45* 11.0 0.00108 391 163 2.862 125 1.461 $DATA$ SET 45* 12.6 0.00118 556 190 3.052 125 1.461 $DATA$ SET 45* 12.6 0.00186 578 230 4.062 2.018 0.546 25.516 15.5 0.00186 578 230 4.582* 300 5.995 686.4 25.515 21.5 0.00783 648 250 4.582* 300 5.995 686.4 25.515 27.1 0.00783 677 250 4.582* 5.995 686.4 25.515 27.1 0.00783 677 273 5.182 400 9.542 28.515 27.1 0.00783 677 273 5.182 5.097 689.4 25.515 <td></td> <td></td> <td>DATA</td> <td>SET 43</td> <td>708.0</td> <td>25.5U</td> <td>99</td> <td>0.000983</td> <td>5</td> <td>4.4</td> | | | DATA | SET 43 | 708.0 | 25.5 U | 99 | 0.000983 | 5 | 4.4 |
| 126 1.512 90 0.744 710.0 25.497 10.7 0.00108 391 163 2.312 100 0.939 $DATA SET 45^{4}$ 11.0 0.00113 410 180 2.362 125 1.461 $DATA SET 45^{4}$ 11.0 0.00161 556 190 3.052 125 1.461 $DATA SET 45^{4}$ 12.6 0.00161 556 230 4.062 200 3.214 684.6 25.515 14.2 0.00181 556 234 4.402 250 4.525 685.4 25.515 21.5 0.00135 647 250 4.582* 300 3.214 686.4 25.515 21.5 0.00135 647 273 5.182 300 5.995 686.4 25.515 21.1 0.0117 736 273 5.182 400 9.542 689.4 25.515 21.1 0.0125 795 273 5.182 500 14.118 689.4 25.462 29.7 0.0243 912 | 4.2 | 0.062 | | | 708.8 | 25.497 | 10.0 | 0.000984 | 366 | 11.0 |
| 163 2.312 100 0.939 \mathbf{MTA} SET 45^{\bullet} 11.0 0.00113 410 183 2.862 125 1.461 \mathbf{DATA} SET 45^{\bullet} 11.0 0.00161 556 190 3.052 125 1.461 \mathbf{DATA} SET 45^{\bullet} 12.6 0.00161 556 230 4.062 200 3.214 684.6 25.516 15.5 0.00135 648 244 4.402 250 4.527 685.4 25.515 21.5 0.00135 678 250 4.582* 300 5.957 685.4 25.515 21.5 0.00173 677 273 5.182 400 9.542 687.6 25.515 27.1 0.0117 736 273 5.182 400 9.542 689.4 25.462 27.1 0.0155 795 273 5.182 400 9.542 689.4 25.462 29.7 0.0239 677 273 5.182 400 9.542 689.4 25.462 29.7 0.0243 912 | 126 | 1.512 | 8 | 0.744 | 710.0 | 25.497 | 10.7 | 0.00108 | 391 | 11.7 |
| 183 2.862 125 1.461 DATA SET 45^{4} 12.6 0.00161 556 190 3.052 150 2.018 $$ | 163 | 2.312 | 100 | 0.939 | | | 11.0 | 0.00113 | 410 | 12.5 |
| 190 1.052 150 2.018 14.2 0.00186 578 230 4.062 200 3.214 684.6 25.516 15.5 0.00135 648 244 4.402 3.214 685.4 25.515 15.5 0.00783 648 250 4.527 685.4 25.515 21.5 0.00783 648 2750 4.527 685.4 25.515 21.5 0.00783 677 270 5.182 400 9.542 687.4 25.515 27.1 0.0117 736 271 5.182 600 9.542 687.4 25.515 27.1 0.0117 736 273 5.182 600 19.872 689.4 25.462 29.7 0.0243 912 2600 19.872 689.4 25.289 34.2 0.0389 1011 273 100 26.990 689.8 25.289 34.2 0.0389 1011 201 26. | 183 | 2.862 | 125 | 1.461 | DATA | SET 45* | 12.6 | 0.00161 | 556 | 19.7 |
| 230 4.062 200 3.214 684.6 25.516 15.5 0.00335 648 244 4.402 250 4.527 685.4 25.515 21.5 0.00783 677 250 4.582* 300 5.995 686.4 25.542 23.6 0.0117 736 273 5.182 400 9.542 687.6 25.515 21.1 0.0117 736 273 5.182 400 9.542 687.6 25.515 27.1 0.0155 795 271 5.182 400 9.542 688.4 25.515 27.1 0.0155 795 273 5.182 400 9.542 689.4 25.515 27.1 0.0155 795 271 5.182 500 14.118 689.4 25.462 29.7 0.0243 912 271 5.182 5690 689.4 25.589 34.2 0.0243 912 271 736 736 27.182 736 27.1 0.02399 1011 771 700 </td <td>190</td> <td>3.052</td> <td>150</td> <td>2.018</td> <td></td> <td></td> <td>14.2</td> <td>0.00186</td> <td>578</td> <td>18.9</td> | 190 | 3.052 | 150 | 2.018 | | | 14.2 | 0.00186 | 578 | 18.9 |
| 244 4.402 250 4.527 685.4 25.515 21.5 0.00783 677 250 4.582* 300 5.995 686.4 25.542 23.6 0.0117 736 273 5.182 400 9.542 687.6 25.515 27.1 0.0155 795 273 5.182 400 9.542 687.6 25.515 27.1 0.0155 795 200 14.118 688.4 25.515 27.1 0.0243 912 DATA SET 40* 600 19.872 689.4 25.462 29.7 0.0389 1011 00 26.590 689.4 25.289 34.2 0.0469 1114 1001 26.590 569.3 569.3 26.5 26.50 569.4 25.289 36.6 0.460 1114 | 230 | 4.062 | 200 | 3.214 | 684.6 | 25.516 | 15.5 | 0.00335 | 648 | 23.3 |
| 250 4.582* 300 5.995 686.4 25.542 23.6 0.0117 736 273 5.182 400 9.542 687.6 25.515 27.1 0.0155 795 273 5.182 400 9.542 688.4 25.515 27.1 0.0155 795 274 5.182 500 14.118 688.4 25.462 29.7 0.0243 912 275 500 14.118 689.4 25.482 34.2 0.0339 1011 273 103 10.1 25.182 34.2 0.0469 1114 273 103 26.590 689.8 25.289 36.6 0.0469 1114 | 244 | 4.402 | 250 | 4.527 | 685.4 | 25.515 | 21.5 | 0.00783 | 677 | 26.5 |
| 273 5.182 400 9.542 687.6 25.515 27.1 0.0155 795 DATA SET 40* 600 14.118 688.4 25.462 29.7 0.0243 912 DATA SET 40* 600 19.872 689.4 25.382 34.2 0.0389 1011 000 26.590 689.8 25.289 34.2 0.0469 1114 1031 1031 26.590 689.8 25.289 36.6 0.0469 1114 | 250 | 4.582* | 000 | 5.995 | 686.4 | 25.542 | 23.6 | 0.0117 | 736 | 26.9 |
| DATA SET 40* 500 14,118 688.4 25,462 29,7 0.0243 912 DATA SET 40* 600 19,872 689.4 25,382 34.2 0.0389 1011 Tool 26,590 689.8 25,289 36.6 0.0469 1114 Tool 700 26,590 689.8 25,289 36.6 0.0469 1114 | 273 | 5.182 | 400 | 9.542 | 687.6 | 25.515 | 27.1 | 0.0155 | 795 | 11.4 |
| DATA SET 40* 600 19.872 689.4 25.382 34.2 0.0389 1011 10.1 700 26.590 689.8 25.289 36.6 0.0469 1114 10.1 700 26.590 689.8 25.289 36.6 0.0469 1114 | | | 005 | 811.41 | 688 4 | 25.462 | 29.7 | 0.0243 | 619 | 43.1 |
| Total Total <thtotal< th=""> Total <tht< td=""><td>DATA SF</td><td>T 40#</td><td></td><td>10 877</td><td>680 4</td><td>201.22</td><td>14.7</td><td>0.0389</td><td>1101</td><td>0 15</td></tht<></thtotal<> | DATA SF | T 40# | | 10 877 | 680 4 | 201.22 | 14.7 | 0.0389 | 1101 | 0 15 |
| | | | 000 | 26.500 | 680 B | 25. 289 | 36-65 | 0.0469 | 1114 | 58.2 |
| | 1923 | 109 | 102 | 25.015 | 690.2 | 25.051 | 38.3 | 0.0567 | 1176 | 65.0 |

* Not shown in figure.

| C COB | EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVIT EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVIT 25 56 56 56 56 56 57 56 58 58 58 58 58 58 58 58 58 58 58 58 58 |
|-------|--|
|-------|--|

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* Not shown in figure.

3.3. Iron

The electrical resistivity of iron has been studied extensively. There are 223 sets of experimental data available for iron specimens of purity 99.8% or higher. The information on specimen characterization and measurement condition for each of the data sets is given in table 8. The data are tabulated in table 9 and shown partially in figures 5 and 6.

Because of magnetic effects, the residual resistivity of iron has been studied with intense interest. Berger and De Vroomen [111] suggested that the residual resistivity measured in the absence of an applied magnetic field is not an indication of the purity of an iron specimen. Fujii and Morimoto [112] suggested that the magnetic contribution to the residual resistivity is 0.02 x $10^{-8} \Omega$ m; a value also agreed upon by Volkenshteyn and Yakina [113]. Thus, even for zone-refined iron, the residual resistance ratio, RRR, has low values of \lesssim 400 as compared with values of a few thousand or even higher for other pure metals. The more recent results of Takaki and Igaki [114] seem to indicate that even for iron that has been highly purified by anion exchange separation, floating-zone melting and hydrogen treatment, the residual resistance ratio has a limiting value of about 500. It is worth noting, however, that the quantity RRR_H, the residual resistance ratio obtained as the minimum value from resistivity measurement as a function of an applied longitudinal magnetic field, of some of their specimens are greater than 2000. The same group of authors [115] later reported RRR_H values of over 10,000 on specimens that had been electrolytically polished to remove silicon contamination on the surface layer (of thickness $\sim 100 \ \mu\text{m}$). The resistivity of iron is also dependent on the density of the measuring current [114]. The results of Takaki and Igaki [114] on specimens of various purity showed that the current density dependence is negligible for specimens having RRR (or RRR_H) values of ≤ 100 . For RRR values higher than 200, or RRR_{μ} values of $\gtrsim 1000$, the resistivity may still be increasing with measuring current at current density values of $>6 \times 10^6$ A m⁻². The limiting RRR value of 500 quoted above was for a measuring current density of $\sqrt{5} \times 10^5$ A m⁻² [114]. This result appears to agree with that of Glaeser et al. [116], even though the magnetic field and current density dependences reported by these two works show some discrepancies. The recommended value for the electrical resistivity of iron at the temperature of 1 K is based on these

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references and subject to the condition that the measuring current is <1 x 10^{6} A m⁻² in the absence of an applied magnetic field. It should represent the value for the electrical resistivity of iron purified by modern electronbeam zone-refining techniques.

The electrical resistivity of iron is dependent on other factors. The most notable factors are the external magnetic field and the magnetic domain structure of the specimen itself. The effects of the former have been investigated mostly at 4 K [112,116-120], and those of the latter have been investigated chiefly for single crystal whisker specimens [121-125]. These effects, together with the effect of the measuring current, are inter-related and are not fully investigated. A resolution of these effects is clearly beyond the scope of this work. Hence, only the conditions "in the absence of an external applied magnetic field" and "with a measuring current of <1 x 10⁶ A m⁻²" are specified. The latter condition is chosen such that the (transverse) magneto-resistance due to the self-induction of the measuring current would not adversely affect the resistivity value.

The electrical resistivity of iron at low temperatures has been reported to contain a T^2 component; see, for example, White and Woods [21], Volkenshtein and Yakina [113], Semenenko and Sudovtsov [126], Fert and Campbell [127], Price and Williams [80], and Janos et al. [128]. However, Kondorskii et al. [129] reported $T^{1.5}$ and T^5 components. More recently, Isshiki and Igaki [115] reported that the temperature dependent part of the resistivity, when measured in a longitudinal magnetic field of 60 K A m⁻¹, can be fitted to a T^2 term and a Bloch-Grüneisen term with $\theta_R = 467$ K for temperatures 1 to 250 K.

A similar analysis [115] on the data of Kemp et al. [130] (data set 31), Kemp et al. [131] (data set 11), White and Woods [21] (data set 86), Fert and Campbell [127] (data set 119), Schwerer et al. [132] (data set 107), Volkenshtein and Yakina [113] (data set 209), and of Hust and Giarratano [133] (data set 47) indicates that, even without an applied longitudinal magnetic field, the electrical resistivity of iron can be represented by eq (8) for temperatures up to about 100 K. The values of A and θ_R in the Bloch-Grüneisen term were taken to be 58.1 x 10⁻⁸ Ω m and 467 K [115], respectively. The coefficient of the quadratic term varies approximately from 1.1 to 3.4 x 10⁻¹³ Ω m K⁻². There seems to be some correlation between the values of the coefficient and the residual resistivities, i.e., a specimen with a low residual resistivity seems

to have a low coefficient (data sets 11, 86, 209) and vice versa (data sets 31. 47). However, with only a few data sets available, a definite relationship between the residual resistivity and the coefficient in the quadratic term cannot be established. Furthermore, the reported T^2 dependence of the electrical resistivity extends probably to temperatures below 1 K [126], whereas most of the authors report data to 2 K or higher. One way of circumventing this problem is to assume that the resistivity can be fitted to a residual term plus a quadratic term below 20 K (the T⁵ or the Bloch-Grüneisen term is negligible compared with the other two terms at these temperatures), and the residual term, taken to be the value at 1 K, is obtained by extrapolation. The recommended values for the electrical resistivity of iron below 100 K are obtained by this procedure. The values of the quantities A and θ are taken to be the same as those given by Isshiki and Igaki [115], i.e., 58.1 x 10^{-8} Ω m and 467 K, respectively. The value of the coefficient of the T^2 term is 1.3 x $10^{-13} \,\Omega$ m K⁻². This was obtained both by a graphical method where the logarithm of the quantity

$$\left(\rho_{\text{measured}} - \rho_0 - A\left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x^5 e^X}{(e^X - 1)^5} dx\right)$$

is plotted against log T, and also by numerically fitting the same quantity to a quadratic function in temperature. This value is in agreement with that suggested by White and Woods [21], but is somewhat below the value of 2.2 x $10^{-13} \Omega \text{m K}^{-2}$ given by Isshiki and Igaki [115] for their highly purified specimens measured in an applied magnetic field of 60 KAm⁻¹.

At temperatures above ~ 100 K, there is a slight change in the temperature dependence of the electrical resistivity. A log-log plot of the quantity

$$\rho_{\text{measured}} - \rho_0 - A \left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x^5 e^x}{(e^x - 1)^2} dx$$

against T for the data of White and Woods [21] (data set 86), Richter and Kohlhaas [134] (data set 43), Moore et al. [135] (data set 17), Fulkerson et al. [136] (data set 16), Hust and Giarratano [133] (data set 47), Kohlhaas and Richter [137] (data set 34), and of Dewar and Fleming [138] (data set 53) shows a decrease from the T^2 line starting at \sim 100 K. This departure from the T^2 line is at a maximum of about 0.05 x $10^{-8} \Omega m$ at \sim 140 K. At higher temperature,

the temperature dependence becomes stronger, with a temperature dependence that approaches a T^3 function. It is interesting to note that the same plot on the data of Kemp et al. [130] (data set 31) shows a slight increase at \sim 100 K. It is not obvious whether this behavior is purely a magnetic effect or an impurity effect. The specimens of Isshiki and Igaki [115] (data sets 219-223) are supposed to be purged of metallic impurities and to contain approximately 0.001 at.% C, 0.0007 at.% O, and <0.0001 at.% N, whereas the specimen of White and Woods [21] (data set 86) contains about 0.03% of mostly metallic impurities. The electrolytic iron specimen of Hust and Giarratano [133] (data set 47) contains about 0.1% also of mostly metallic impurities. The specimen of Moore et al. [139] (data set 15) contains $\leq 0.01\%$ Ni, $\leq 0.01\%$ Si, and lesser amounts of other impurities, and the specimen of Fulkerson et al. [136] (data set 16) contains <0.02% Si, 0.014% C, <0.01% Ni, and lesser amounts of other impurities. On the other hand, the magnetoresistance of iron is positive at room temperatures (see, for example, Kornetzki [140], Schindler and La Roy [118]), and negative at helium temperatures (see, for example, Fujii and Morimoto [112], Glaeser et al. [116], and Arajs et al. [119]). From the only available data by Shirakawa [141] and by Matuyama [142] on electrolytic iron at intermediate temperatures, the magnetoresistance of iron changes sign at \sim 77 K. For the lack of definite conclusion, this behavior is ignored at the present, and the resistivity value is assumed to follow the relation

$$\rho = \rho_0 + \alpha T^2 + A \left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x e^x}{(e^x - 1)^2} dx$$
(8)

up to 200 K. This assumption may result in a maximum probable error of only -1% or -0.03 x 10^{-8} Ω m at \sim 150 K.

At temperatures above 150 K, and up to the Curie temperature, there are a number of data sets that agree with each other to within ±2%: Moore et al. [139] (data set 15), Fulkerson et al. [136] (data set 16), Wallace et al. [143] (data set 21), Pallister [144] (data set 22), Jaeger et al. [145] (data set 24), Kohlhaas et al. [137] (data set 33), Kierspe et al. [78] (data set 39), Richter and Kohlhaas [134] (data set 43), Powell et al. [146] (data set 77), and Lauchbury and Saunders [147] (data set 217). Among these sources, Fulkerson et al. [136] (data set 16) reported also the resistivity at 4 K, and Moore

et al. [135] (data set 17) reported the residual resistivity ratio. Greater weight is given to the data of Moore et al. Most of these data sets appear to have resistivity values slightly higher than 9 x $10^{-8} \Omega m$ at 273 K, except for data sets 17 and 22. Judging from the ice point resistivity values and from the temperature variation of the solute resistivities of various elements in iron (see, for example, Schwerer and Cuddy [148]), it appears that the specimen of Moore et al. [135] (data set 17) is the purest among these groups, and its resistivity values at 90 K are within 2% of the recommended values based on the analysis of the available low temperature data described earlier. The recommended values within the range of ±100 K of the ice point are, therefore, based on data set 17, and in the higher temperature range up to 900 K they are based on the data sets mentioned above. Both graphical and numerical methods in curve fitting are employed. It is found that the electrical resistivity of iron can be represented by a cubic polynomial at temperatures from about 200 to 900 K.

For temperatures higher than 900 K and up to the Curie temperature, the electrical resistivity of iron increases more rapidly with temperature. Even though there are detailed accounts on the temperature derivative of the resistivity, the agreement between them is not good (see, for example, Lauchbury and Saunders [147] and Seehra et al. [149], the values of $d\rho/dT$ from these two accounts differ by $\sim40\%$ at 1030 K). The value of the Curie temperature has been reported to be 1040.3 ± 1 K (Seehra et al. [149]), 1038-1043 K (Fulkerson et al. [136]), 1051-1055 K (Morris [150]), 1044 ± 2 K (Arajs and Colvin [151]), 1037 K (Richter and Kohlhaas [134]), 1027 K (Kohlhaas and Richter [137]), 1042.7 K (Lauchbury and Saunders [147]), and 1036 K (Wallace et al. [143]). The last authors also reported a Curie temperature of 1042 K from their specific heat measurements. In view of the wide spread of the reported values, a Curie temperature of 1043 K is adopted from the AIP Handbook [152]. The recommended values below this temperature are based on the data of Lauchbury and Saunders [147] (data set 217), with slight adjustments so that they would merge smoothly with the recommended values at lower temperatures. The recommended value at the Curie temperature, 101.1 x $10^{-8} \Omega m$, is within 0.3% of the values given by Lauchbury and Saunders [147].

At temperatures above the Curie point, the differences between reported resistivity values from the above references become greater, even though they

are generally still within 2% of each other. The recommended values from the Curie temperature to the α - γ transition are based mainly on the results of Fulkerson et al. [136] (data set 16), Wallace et al. [143] (data set 21), and also of Powell et al. [146] (data sets 75-77). There are other detailed accounts on the resistivity at temperatures close to the α - γ transition: Kohlhaas and Richter [137] (data sets 37-38), Arajs and Colvin [151] (data sets 57-58), and Bullock [153] (data sets 98-99). However, there are wide discrepancies among these data sets. The data of Bullock and of Kohlhaas and Richter are too high and too low, respectively. The specimen of Arajs and Colvin showed some unexplained behavior, its residual resistivity ratio changed by +13% after the high temperature measurement, and the resistivity value at room temperature appeared to be too high for a zone-refined specimen. The onset of the $\alpha-\gamma$ transition, Ac, point, has been reported at 1188-1189 K (Moore et al. [139]), 1189 K (Kohlhaas and Richter [137]), 1189.7 K (Richter and Kohlhaas [134]), and has been inferred from graphical illustrations at about 1182 K (Powell et al. [146] data set 75), 1183 K (Arajs and Colvin [151] data set 57), 1187 K (Kohlhaas and Richter [137] data set 37), and 1186 K (Bullock [153] data set 98). Because of the lack of general agreement, the transition temperature is taken to be 1185 K, a value deduced from thermal expansion data [42].

As mentioned earlier, there are detailed reports on the behavior of the electrical resistivity at the α - γ transition. Not surprisingly, all these reports show that the transition occurs over a finite temperature range: ~4 K according to Powell et al. [146], Arajs and Colvin [151], and Bullock [153], and \sim 5 K according to Kohlhaas and Richter [137]. All reported a hysteresis effect: in the transition region, the resistivity values measured at decreasing temperatures were lower than those measured at increasing temperatures. The temperature for the onset of the $\gamma-\alpha$ transition upon cooling, the Ar₃ point, is also reported to be somewhat lower than the Ac₃ point. The latter three groups of authors also reported that the resistivity of α -iron at temperatures about one degree below the Ar₃ point after being cooled from the γ phase is higher than that of the α -iron after being heated from lower temperatures. In view of these and of the lack of such evidence from the data of Powell et al. [24] (data sets 75-77), this behavior is ignored at the present time. It is probable that such behavior is dependent upon specimen purity and its thermal history and mechanical history as well. Even though recommended values are

given at a single transition temperature (for both the α and the γ phases), the transition for a given specimen may be expected to occur over a small temperature range of approximately 1180-1190 K. Its resistivity below 1185 K may be somewhat ($\leq 0.5 \times 10^{-8} \Omega$ m) lower than the recommended value and vice versa above 1185 K.

There are relatively fewer data sets available for temperatures above the α - γ transition. The data sets which are considered reliable and from which the recommended values are derived are generally for temperatures less than \sim 1300 K. For higher temperatures, close to the γ - δ transition, the data of Cezairliyan and McClure [154] (data sets 62-63) appear to merge well with extrapolations of the data of Fulkerson et al. [136] (data set 16) and of Wallace et al. [143] (data set 21). The recommended values from the α - γ transition to the γ - δ transition are based on these data sets. At temperatures immediately above the α - γ transition, the data of Powell et al. [146] (data sets 75-76) are also taken into account.

There are only a few data sets for the electrical resistivity of δ -iron. The recommended values are based on the results of Cezairliyan and McClure [154] (data sets 62 and 64), Güntherodt et al. [92] (data set 206), and Powell [155] (data set 138). The slight upturn in the resistivity value at temperatures close to the melting point is based on the latter two data sets. This upturn seems to be substantiated by the data of Baum et al. [156] (data set 114) and of Kita et al. [93] (data sets 212-214). There exists only two reports on the change of resistivity value at the γ - δ transition, by Cezairliyan and McClure [154] (data sets 62-65), and by Kierspe et al. [78] (data set 41). Both indicate a slight increase in resistivity from the γ to the δ phase. No hysteresis has been reported.

There are in excess of 10 data sets available for the electrical resistivity of molten iron. Some of these: Güntherodt et al. [92] (data set 206), Kita et al. [93] (data sets 211-213), Baum et al. [156] (data set 114), Arsentiev et al. [157] (data sets 215-216), Ono and Yagi [89] (data set 115), and Eliutin et al. [88] (data set 92) cover the transition from the solid to the molten state. The last authors reported a decrease in resistivity upon melting for an impure specimen (~99.0% purity), in agreement with an earlier measurement on Armco iron by Mokrovskii and Regel [158], whose result has been widely quoted. However, the more recent measurements on purer specimens reported

in the references mentioned above all show an increase. The majority of the reported data show a linear dependence on temperature, and the data of Seydel and Fucke [87] (data set 205) which were obtained by a pulse-heated exploding wire technique show that the linear dependence is applicable up to 3000 K. The recommended values are based on the data of Güntherodt et al. [92] (data set 206) and Kita et al. [93] (data sets 212-214), both of which are obtained by steady state methods. Values above 1900 K are extrapolated according to a linear temperature dependence. The value at 3000 K is about 7% higher than that of Seydel and Fucke [87]. A few of the available data sets are obtained by the rotating field method: Ono and Yagi [89] (data set 115), Levin et al. [91] (data set 112), Baum et al. [156,159] (data sets 114,121), and Samarin [94] (data set 137). The reported data among this group show relatively large variations, but are still within 4% of the recommended values.

The recommended values both uncorrected and corrected for thermal expansion of the material are presented in table 7, while only the uncorrected values (except those for the liquid state) are shown in figures 5 and 6 along with the experimental data. These values at temperatures above 200 K are for iron of purity 99.99% or higher, while those below 200 K are applicable only to highly purified zone-refined iron having a residual resistivity of 0.0200 x $10^{-8} \Omega m$. The estimated uncertainty in the recommended values is ±5% below 100 K, ±3% from 100 to 200 K, and ±2% above 200 K up to the melting point. The uncertainty at temperatures immediately above the melting point is about ±5%, increasing to ±10% at the highest temperatures.

For slightly less pure iron having different residual resistivity, its electrical resistivity values can be calculated from the recommended values using the Matthiessen's rule, which will not introduce serious errors. For example, using Matthiessen's rule for the specimen of Moore et al. [135] (data set 17) gives discrepancies of $\pm 1.7\%$ (compared with the measured data) at 90 K, -2% at 260 K, and <0.1\% at 400 K. That for the specimen of White and Woods [21] (data set 86) gives discrepancies of -0.5% at 11 K, -1.3% at 22 K, $\pm 1.6\%$ at 98 K, -1.8% at 178 K, and -1.4% at 273 K. And that for the specimen of Fulkerson et al. [136] (data set 16) gives -1% at 77.5 K, $\pm 0.6\%$ at 194 K, and -1% at 273 K. Thus, it does appear that using the Matthiessen's rule and the recommended values will give resistivity values for a specimen with residual resistivity lower than $0.4 \times 10^{-8} \Omega$ m to within $\pm 2\%$, subject to the uncertainties

in the recommended values specified in the preceding paragraph. The applicability of Matthiessen's rule, to within the possible error of ± 23 , also seems to be confirmed for a more commonly available material, the electrolytic iron. For example, using the rule and comparing with the data of Hust and Giarratano [133] (data set 47) for SRM Iron-1265 gives discrepancies of -13 at 100 K, -0.93 at 200 K, and -1.53 at 280 K. Since deviations from the Matthiessen's rule for dilute iron alloys are positive (see, for example, Bass [160]), its application in calculating the electrical resistivity of an iron specimen lower in purity is likely to result in an underestimate, especially around room temperature where the deviation from Matthiessen's rule approaches a maximum. At high temperatures, the relative error introduced by the application of Matthiessen's rule should diminish with increasing temperature.

The recommended values uncorrected for thermal expansion given in table 7 can be represented approximately by the following expressions to within $\pm 0.1\%$. 1-200 K:

$$\rho = 0.02 + 58.1 \left(\frac{T}{467}\right)^5 \int_0^{467/T} \frac{e^x x^5}{(e^x - 1)^5} dx + 1.3 \times 10^{-5} T^2$$
(26)

200-900 K:

$$\rho = -1.120747752 + 2.261529506 \times 10^{-2}T + 3.913892564 \times 10^{-5}T^{2} + 2.952608182 \times 10^{-8}T^{3}$$
(27)

900-1020 K:

$$\rho = -513.9789758 + 1.70577020 \text{ T} - 1.804410343 \times 10^{-3} \text{T}^2 + 7.034546961 \times 10^{-7} \text{T}^3$$
(28)

1020-1143 K in the vicinity of the Curie temperature, T_c :

$$\rho = 101.13 - 2.984305206 \times 10^{-1} (T_C - T) + 1.905714112 \times 10^{-3} (T_C - T)^2 - 1.3355493086 \times 10^{-5} (T_C - T)^3$$
(29)

1043-1070 K:

$$\rho = 101.13 + 2.020277018 \times 10^{-1} (T-T_C) - 5.420505212 \times 10^{-3} (T-T_C)^2 + 1.294364953 \times 10^{-4} (T-T_C)^3 - 1.243596538 \times 10^{-6} (T-T_C)^4$$
(30)

1070-1185 K:

$$\rho = -1309.064808 + 3.419572717 T - 2.773870769 \times 10^{-3}T^{2} + 7.595259559 \times 10^{-7}T^{3}$$
(31)

1185-1667 K:

$$\rho = 55.0861977 + 5.289665269 \times 10^{-2}T + 9.77621850 \times 10^{-12}T^2 - 4.0798019 \times 10^{-9}T^3$$
(32)

1667-1811 K:

$$\rho = -11976.94918 + 21.0981583 \text{ T} - 1.226701138 \times 10^{-2} \text{T}^2 + 2.378811917 \times 10^{-6} \text{T}^3$$
(33)

1811-3000 K:

$$\rho = 135.2 + (T - 1811) \times 1.545 \times 10^{-2}$$
(34)

It should be emphasized that these expressions do not necessarily suggest any theoretical justification, and should be treated, most appropriately, as numerical aids only. It should also be understood that giving these expressions does not imply a recommendation for the temperature derivative of the electrical resistivity.

| T | (|) | T | | p |
|-----|-------------|-----------|------|--------------------|------------------------|
| | uncorrected | corrected | | uncorrected | corrected |
| 1 | 0.0200 | 0.0200 | 800 | 57.14 | 57.56 |
| 4 | 0.0202 | 0.0202 | 900 | 72.46 | 73.11 |
| 7 | 0.0206 | 0.0206 | 1000 | 90.80 | 91.76 |
| 10 | 0.0213 | 0.0212 | 1043 | 101.1 ^b | 102.2 ^b |
| 15 | 0.0232 | 0.0231 | 1100 | 107.0 | 108.3 |
| 20 | 0.0262 | 0.0261 | 1150 | 110.1 | 111.5 |
| 25 | 0.0313 | 0.0312 | 1185 | <u>111.9(a)</u> | <u>113.4(α)</u> |
| 30 | 0.0396 | 0.0395 | 1185 | 111.0(Y) | <u>112.1(y)</u> |
| 40 | 0.0733 | 0.732 | 1200 | 111.5 | 112.6 |
| 50 | 0.145 | 0.145 | 1300 | 114.9 | 116.4 |
| 60 | 0.268 | 0.267 | 1400 | 117.9 | 119.7 |
| 70 | 0.449 | 0.448 | 1500 | 120.7 | 122.8 |
| 80 | 0.690 | 0.689 | 1600 | 123.0 | 125.4 |
| 90 | 0.964 | 0.962 | 1667 | $124.4(\gamma)$ | 127.0(γ) |
| 100 | 1.28 | 1.28 | 1667 | 124.6(ð) | |
| 150 | 3.16 | 3.16 | 1700 | 125.4 | |
| 200 | 5.20 | 5.19 | 1800 | 127.9 | |
| 250 | 7.44 | 7.44 | 1811 | 128.6(δ) | |
| 273 | 8.57 | 8.57 | 1811 | | 135.2 ^c (l) |
| 293 | 9.61 | 9.61 | 1900 | | 136.6 ^c |
| 300 | 9.98 | 9.98 | 2000 | | 138.2 ^c |
| 400 | 16.08 | 16.10 | 3000 | | 153.6 |
| 500 | 23.66 | 23.72 | | | |
| 600 | 32.92 | 33.06 | | | |
| 700 | 44.02 | 44.27 | | | |

TABLE 7. RECOMMENDED VALUES FOR THE ELECTRICAL RESISTIVITY OF IRON^a

[Temperature, T, K; Electrical Resistivity, ρ , $10^{-8} \Omega m$]

а The values are for iron of purity 99.99% or higher, but those below 200 K are applicable only to iron having a residual resistivity of 0.0200 x 10^{-8} Ω m. Columns headed uncorrected and corrected refer to values uncorrected and corrected for thermal expansion, respectively. Dotted lines separating tabular values indicate solid phase transitions and solid line indicates solid to liquid state transformation.

b α : bcc; γ : fcc; δ :bcc. b Value at the Curie temperature. c Provisional value.



2

3

56

2 3 FIGURE 5

4 5 6 8 103

205

82

4 5 6

CINDAS

8 1

2 3 4 5 6

8 10

2

3 4

TEMPERATURE , K



| 927 21-273 Iron 1 T 959 A 4.2-293 c |
|---|
| 227 21-273 Iron 1 559 A 4.2-293 667 A 323-523 Pure iron |

* Not shown in figure.

TABLE 8. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF IRON Fe (continued)

.

| E S E | žż | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---------|-----|---|------|----------------|------------------|-------------------------------------|---|
| 61 | 165 | Powell, R.V. and Tye, R.P. | 1967 | < | 323-1073 | Pure iron Sample No. 2 | 0.0055 Ni, 0.0053 Si, 0.0038 Ai, 0.0035 S, 0.002 Co, 0.0017 P, 0.0014 C, 0.001 Cr, °0.001 Mn, 0.0008 0, 0.0007 N, and 0.000016 H; short rod 1.27 cm diam prepared by Metallurgy Division of National Physical Lab.; machined from a disk. |
| • • • • | 165 | Powell, R.V. and Tye, B.F. | 1967 | ۲ | 323-523 | Purefree iron Sample No. 6 | 0.08 Si, 0.03 C, 0.015 P, 0.01 Mn, and 0.01 S; 2.54 cm in diam and 20 cm long; supplied by Low Moor Best Yorkshire Iron Ltd.; 1) the above specimen measured at increasing temperatures; 2) the above specimen measured at decreasing temperatures. |
| 51 | 139 | Moore, J.P., Fulkerson, N., and McElroy, D.L. | 1964 | ~ | 73-1273 | High purity iron | 0.001-0.01 Ni, 0.001-0.01 Si, 0.003 S, 0.003 C, 0.0025 O, 0.0011 P, 0.0001-0.001 Ai, 0.0001-0.001 Ca, 0.0001-0.001 Cu, 0.0005 N, and 0.0001 H; atomic percent, data here rounded off; prepared by arc melting Armco iron stock in pure inert atm to produce pancake shaped billets, rolled into sheets and cut to make feed stock for electron beam melting, then cast into 10.16 cm (4 in.) in diam and 15.24 cm (6 in.) in diam and 7.62 cm (3 in_1) long, cut from center portion of billet; measured in vacuum at 10^{-5} to 10^{-7} Torr; data corrected for thermal expansion except points at 7.3, 189, and 273 K. |
| 16 | 136 | Fulkerson, W., Moore, J.P., and McElroy, D.L. | 1966 | ۲. | 4.0-1273 | High purity iron | 99.95 Fe, 0.002-0.02 S1, 0.014 C, 0.00095-0.0095 N1, 0.0088 0, <0.0056 H, 0.0022 S, 0.0021-0.0021 A1, 0.002 P, 0.002 N, 0.00014- 0.0014 Ca, and 0.00009-0.0009 Cu, in atomic percent; obtained by electron beam melting of Armco iron; homogeneous to 10.19; rod specimen 38:10 cm (0.15 in.) in diam and 7.62 cm (3 in.) long; free of voids; immersion density 7.881 g cm 3 ; smoothed data extracted from table; data corrected for thermal linear expansion; resistivity measured with current densities of 6.8, 11 and 11 A cm ⁻² at 4, 77.5 and 194.1 K respectively. |
| 11 | 135 | Moore, J.P., McElroy, D.L., and Barisoni, M. | 1966 | X | 90-40 | Grade 1 | Cylindrical specimen machined from electron beam zone-refined iron (3-page); produced by Materials Research Corp.; density 7.824 g cm ⁻¹ ; electrical resistivity ratio $\rho(273 \mathrm{K})/\rho(4.2 \mathrm{K}) = 201$; smoothed data from table. |
| 18 | 166 | McDonald, W.J., Jr. | 1962 | < | 1.63-80.7 | | Cut from a zone-refined ingot; prepared at BMI; machined into a rec- taugular parallel piped 0.157 x 0.157 x 0.381 cm (0.062 x 0.062 x 1.5 in.). |
| 19 | 167 | Bungardt, K. and Spyra, W. | 1965 | | 293-1373 | | 0.03 Ni, 0.015 C, 0.007 S, and traces Al, Mo, P, and Si; cylindrical specimen. |
| 8 | 168 | Bohm, R. and Machtel, E. | 1969 | | 196-406 | | 0.005 N, 0.004 C, and 0.003 0; cylindrical specimen 10 mm in diam. |

* Not shown in figure.

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Fe (continued) MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF IRON TABLE 8.

| R Set R | Ref. | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---------|-------|--|------|----------------|-------------------|-------------------------------------|--|
| 21 | 143 | Wallace, D.G., Sidles, P.H., and Danielson, G.C. | 1959 | £ | 298-1323 | High purity iron | 0.03 C, 0.01 N and O each, <0.0005 Ni, 0.0001 Cu, <0.0001 each of Mg. Si, Ag, and Na; wire specimen 0.0254 to 0.0346 cm in diam and 4 to 7 cm long; from Johnson and Matthey Co.; drawn and annealed at 1273 K for 1 h, cooled at a rate of 40 kh ⁻¹ while measurement was made; with some specimens, measurements here made upon reheating, and data "accurately reproduced"; smoothed values from table, representing data for two specimens; uncorrected for thermal expansion; values do not reflect a discontinuity of 0.6% upon cooling at 1173 K. |
| 22 | 144 | Pallister, P.R. | 1949 | V | 273-1548 | | 99.99 ^{\pm} Fe; 1 cm in diam and 30 cm long; density 7.87 \pm 0.005 g cm ⁻³ ; uncorrected for thermal expansion; data extracted from table. |
| 23* | 169 | Bäcklund, N.G. | 1961 | < | 90290 | Pure iron Data Set 1 | Three types of specimens: 1) "very pure iron" wire; 2.5 mm in diam; from Phillips Research Lab., 2) spectroscopically standardized pure iron wire; 5 mm in diam; from Johnson and Matthey Co., 3) pure iron wires; 1.0 and 2.0 mm in diam; from Heraeus Inc.; all specimens an- nealed at 773.2 K for 10 h; data reported as average of all three types. |
| 24 | 145 | Jaeger, F.M., Rosenboha, E., and Zuithoff, A.J. | 1938 | | 293-1243 | Pure iron | Pure; 0.25 mm in diam and 925 mm long; data corrected for thermal expansion. |
| 25* | 170 | Cleaves, H.E. and Hiegel, J.M. | 1942 | | 293 | Ingot #2 | 0.002 S, <0.002 Cu, 0.001 C and Si each, <0.001 Be, and <0.0005 P; 2 mm in diam and about 1 meter long; ingots produced by recrystalli- zation of ferric nitrate, conversion to ferric oxide, reduction to sponge fron, and meiting under hydrogen and in a vacuum, forged, cold- rolled, swaged, and drawn; annealed in vacuum for 15 min at 1123 K. |
| 26* | 170 | Cleaves, H.E. and Biegel, J.M. | 1942 | | 293 | Ingot #7 | 0.002 O and S each, <0.002 Cu, 0.001 Si, and <0.001 C; dimensions, fabrication method, and heat treatment same as the above specimen. |
| 27# | 170 | Cleaves, H.E. and Hiegel, J.M. | 1942 | | 293 | Ingot #14 | 0.002 O and S1 each, 0.002 Cu, 0.001 C and S each; dimensions, fabri- cation method, and heat treatment same as the above specimen. |
| 28* | 170 | Cleaves, H.E. and Hiegel, J.M. | 1942 | | 293 | Ingot #11 | 0.004 0, <0.002 Cu, and 0.001 S; dimensions, fabrication method, and heat treatment same as the above specimen. |
| 29# | 170 | Cleaves, H.E. and Hiegel, J.M. | 1942 | | 293 | Ingot #19 | 0.004 0, 0.002 S, <0.002 Cu, and <0.001 C; dimensions, fabrication method, and heat treatment same as the above specimen. |
| 304 | 170 | Cleaves, H.E. and Hiegel, J.M. | 1942 | | 293 | Ingot #6 | 0.004 0, <0.002 Cu, 0.001 S and Si each, and <0.001 Be and C each; dimensions, fabrication method, and heat treatment same as the above specimen. |
| 11 | 130 | Kemp, W.R.G., Klemens, P.G., and White, G.K. | 1956 | < | 4.2-293 | JM 5092 | 99.99 Fe, 0.005 Ni, 0.0002 Cu, 0.0001 Ag, and traces Mg and Mn; 2 mm in diam rod; supplied by Johnson and Matthey Co.; annealed at 1023 K (750 C) for 4 h in vacuum; resistivity values calculated from reported ideal electrical resistivity and $\rho_0 = 0.248 10^{-8} \mathrm{Gm}$. |
| * Not | shown | in figure. | | | 1 | | |

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|-------|-------|---|------|--------|-----------|-------------------------|---|
| k set | 2 | Author (s) | Year | Used | Range, K | Specimen Designation | Composition (weight percent), Specifications and Remarks |
| 32 | 171 | Yoshida, I. | 1965 | | 0.5-1.1 | | No details given. |
| 8 | 137 | Kohlhaas, R. and Richter, F. | 1962 | £ | 293-1523 | FeL | 0.064 0, 0.0027 C, 0.002 S, 0.001 Mn, N, and Si each; 0.5 cm in diam and 25 to 30 cm long; turned from square bar, transition temperatures: $Ac_2 = 1027 K (754 C)$, $Ac_3 = 1189 K (916 C)$ and $Ar_3 = 1175 K (902 C)$; smoothed data from table. |
| 34 | 137 | Kohlhaas, R. and Richter, F. | 1962 | а, | 90-291 | Feµ | The above specimen. |
| 35* | 137 | Kohlhaas, R. and Richter, F. | 1962 | £ | 969-1080 | Feµ | The above specimen at temperatures about the Curie point; measured while heating. |
| 36* | 137 | Kohlhaas, R. and Richter, F. | 1962 | £ | 972-1079 | Fe | The above specimen at temperatures about the Curie point; measured while cooling. |
| 37* | 137 | Kohlhaas, R. and Richter, F. | 1962 | £ | 1176-1198 | Feu | The above specimen at temperatures about the $\alpha\text{-}\gamma$ transition; measured while heating. |
| 38* | 137 | Kohlhaas, R. and Richter, F. | 1962 | £ | 1164-1195 | Feµ | The above specimen at temperatures about the $\alpha\text{-}\gamma$ transition; measured while cooling. |
| 39 | 78 | ^v ierspe, W., Kohlhaas, R., and Gonska, H. | 1967 | 8 | 73-1715 | | 0.0060 S, 0.0050 C, 0, and S1 each, 0.0016 M, 0.0010 N, and P each; wire specimen from Prof. W.A. Fischer, Max-Planck-Institute for Iron Research; smoothed values from figure. |
| 40 | 78 | Kierspe, W., et al. | 1967 | 80 | 1103-1283 | | The above specimen at temperatures about the $lpha-\gamma$ transition. |
| 41 | 78 | Kierspe, W., et al. | 1967 | g | 1553-1713 | | The above specimen at temperatures about the $\gamma-\delta$ transition. |
| 42* | 208 | Kohlhaas, R. and Kierspe, W. | 1965 | | 83-353 | | 0.0027 C, 0.002 S, 0.001 Mn, N, and Si each, and trace of Cr. |
| 43 | 134 | Richter, F. and Kohlhaas, R. | 1964 | | 93-1273 | | 0.012 0, 0.008 P, 0.007 C, and Al each, 0.004 S, and 0.002 N; disk specimen 63 mm outer diam; annealed for several hours at 1193 K (900 C); Curie point 1037 K (764 C); α - γ transition: Ac ₃ = 1189.7 K (916.7 C), Ar ₃ = 1186.3 K (913.3 C). |
| *** | 172 | Jaeger, W. and Diesselhorst, N. | 1900 | | 291-373 | Eisen I | 0.1 C, metallic impurities not determined; 1.3007 cm in diam and 27.0 cm leng; density 7.84 g cm ^{-3} . |
| 454 | 173 | Lorenz, L. | 1881 | | 273-373 | | No details reported. |
| 464 | 174 | Brown, H.M. | 1928 | ¥ | 312 | | 0.0794 cm ² x 10 cm. |
| | | | | | | | |
| * Not | shown | in figure. | | | | | |





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TABLE 8. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF IRON Fe (continued)

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| 3 - | j | Author (s) | Year | Method | Temp. | Name and Spectmen | (nannafring (usish pernant) Cnanffingting and Basaka |
|-----|-----|------------------------------------|------|------------|----------|-----------------------------|--|
| | ż | | | Used | Range, K | Designation | COMPOSITION (NEIBHT PERCENT), SPECIALCELIONS AND NEMATING |
| | 133 | Hust, J.G. and Giarratano, P.J. | 1975 | | 4-280 | uBS electrolytic iron | 99.9 ⁺ Fe. 0.041 Ni, 0.0080 Si, 0.0072 Cr, 0.007 Co, 0.0067 C, 0.0059 S, 0.0058 Cu, 0.0057 Mh, 0.0005 No, 0.0023 P, 0.0007 Al, 0.0006 Ti and V each, 0.0002 As, 0.00013 B, 0.00002 Pb; chemical composition certified by NBS, SRM 1265; grain size 0.05 am for annealed condition; rod spectimen 3. 6 mm in diam and 23 cm long, apparently annealed; density 7.867 \pm 0.0003 cm ⁻³ , for annealed condition; Rockwell hardness B24, for annealed condition; mockwell resistivity Tatio p(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity 0.385 x 10 ⁻⁶ Am, average p1(273 K/p(4 K)) is 23; residual resistivity resistive of the subord of the subord point and bi. = -1.52095464 x 10 ⁻⁶ bis = -2.5955461 x 10 ⁻⁶ bis = -2.595519976 x 10 ⁻⁷ bis = -2.595519976 x 10 ⁻⁷ bis = -2.5095564 x 10 ⁻⁶ bis = -2.595519976 x 10 ⁻⁷ bis = -2.595519976 x 10 ⁻⁷ bis = -2.595519976 x 10 ⁻⁷ bis = -2.59551976 x 10 ⁻⁷ bis = -2.59551976 x 1 |
| • | 138 | Dewar, J. and Fleming, J.A. | 1893 | P 2 | 76-471 | Iron A | 0.25 Mn, 0.01 S, very free from C, S1, and P; wire specimen 0.02657 cm mean diam and 100 cm long; from Armstrong's works, sent by Colonel Dyer of Elswick Ordnance Works; resistance 0.4223, 1.1909, 1.5086, 1.9104, 2.0737, 2.4167, 2.8368, 3.4091, and 4.1935 ft at 76.1, 191.3, 229.3, 274.55, 291.65, 325.25, 363.7, 412.0, and 470.5 K, respectively; temperature below 273 K (0 C) measured by platinum resistance ther- mometer; data uncorrected for thermal expansion, length and mean diameter measured at 288 K; data extracted from table. |
| | 138 | Devar, J. and Fleming, J.A. | 1893 | R. | 54,76 | Iron A | Longer specimen cut from the same piece as Data Set 48; resistance 2.983 and 3.834 Ω at 53.8 and 76.1 K, respectively; data uncorrected for thermal expansion, length measured at 288 K; data extracted from text; temperatures measured by platinum resistance thermometer. |
| | 136 | Dewar, J. and Fleming, J.A. | 1893 | <u>م</u> | 76-469 | Iron H.W. | High degree of purity; wire specimen 0.023078 cm mean diam and 100 cm long; from Messrs. Hopkins and Williams; very soft and veil annealed, cold worked under the hammer and drawn without heating, into a very uniform wire; resistance 0.2918, 1.2713, 1.7137, 2.1791, 2.3940, 2.9546, 3.4976, 4.2536, and 5.1395 R at 76.1, 191.3, 234.0, 273.85, 291.40, 333.40, 371.25, 418.6 and 469.3 K, respectively: mean temper- ature coefficient between 273 and 373 K, 0.00625; data uncorrected for thermal expansion. length and mean diameter measured at 288 K; data extracted from table; temperature below 273 K (0 C) measured by platinum resistance thermometer. |

* Not shown in figure.

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| Re t B | | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------------|-------|-------------------------------------|------|----------------|-------------------|-------------------------------------|---|
| 51* | 138 | Dewar, J. and Fleming, J.A. | 1893 | 2 | 51-76 | lron H.W. Coil (a) | Longer coil cut from the same wire as the above specimen, 2600 cm long; resistance 3.839, 4.154, and 7.091 Ω at 51.0, 54.0 and 76.1K, respec- tively; data uncorrected for thermal expansion, length measured at 288 K; data extracted from table; temperature measured by platinum resistance thermometer. |
| 52* | 138 | Dewar, J. and Fleaing, J.A. | 1893 | 2 | 51-76 | Iron H.W. Coll (b) | Still longer coil cut from the same wire as the above specimen; wire specimen 3700 cm long; resistance 5.222, 5.257, and 9.875 ß at 50.5, 50.8, and 76.1 K, respectively; data uncorrected for thermal expansion. length measured at 288 K; date extracted from table; temperature measured by platinum resistance thermometer. |
| 33 | 130 | Devar, J. and Fleming, J.A. | 1892 | 2 | 76-370 | | Pure soft iron; wire specimen had probable dimensions of 0.0076 (0.003 in) in diam and 50 or 100 cm long; from Messrs. Griffin and Co.; annealed; mean diameter of wire measured to nearest 0.000254 cm (0.0001 in); measurement of resistance repeated several times; mean observed specific resistance reported; data uncorrected for thermal expansion; data extracted from table. |
| 3 | 175 | Honde, K. and Simidu, T. | 1917 | 4 | 302- 1174 | Swedish iron | Cylindrical specimen, 0.5 cm in diam and 20 cm long. |
| 55* | 151 | Arajs, S. and Colvin, R.V. | 1964 | ~ | 300-1291 | | 0.00300 0, 0.0015 Ni, 0.0012 Co, 0.0005 C and Ge each, 0.0004 Cr, 0.0003 N, 0.00015 Cu, 0.00008 Zn, 0.00004 Ga, 0.00003 Nb, 0.000025 Ti 0.00002 V, 0.000009 As, <0.000004 Mn, and <0.000007 Others; zone re- fined; 0.1 x 0.3 x 2.0 cm; $p(4,2 K)/p(298 K) = 3.76 x 10^{-3}$ before high temperature test and 4.30 x 10^{-3} after test; Curie temperature 1044 \pm 2 K; measured with a current density of v12.9 x 10^8 Am ² ; corrected for thermal expansion; data extracted from figure. |
| 56# | 151 | Arajs, S. and Colvin, R.V. | 1964 | V | 1018-1068 | | The above specimen in the neighborhood of Curie temperature; corrected for thermal expansion; data from figure. |
| 57* | 151 | Arajs, S. and Colvin, R.V. | 1964 | ۲. | 1151-1197 | | The above specimen measured through $\alpha-\gamma$ transition; temperature in- creasing; uncorrected for thermal expansion; data from figure. |
| 1 2 | 151 | Arajs, S. and Colvin, R.V. | 1964 | * | 1150-1186 | | The above specimen measured while cooling through 0-Y transition; tem- perature decreasing; uncorrected for thermal expansion; data from figure. |
| 594 | 176 | Kondorskii, E.I. and Sedov, V.L. | 1960 | × | 4.2 | | Technically pure; 0.59 cm in diama and 11.2 cm long; vacuum annealed at 1273 K for 8 h; oven cooled; measured under saturation magnetiza- tion 1751 g. |
| 3 | 177 | Ibragimov, Sh.Sh. | 1962 | ۷ | 293-1698 | Iron | 0.06 Si, 0.04 C, 0.02 Mn and Cr each; annealed at 1033 K. |
| e 19 | 178 | Butler, E.H., Jr. and Pugh, E.M. | 1940 | | 313-343 | | Electrolytical iron; annealed in hydrogen. |
| Kot | shown | on either figure. | | | | | |

| R Se ta | Ref. | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------------|------|--|------|----------------|-------------------|-------------------------------------|---|
| 62 | 151 | Cesairliyan, A. and McClure, J.L. | 1973 | | 1500-1660 | Y iron l | Tubular specimen $6.3 \text{ mm} 0.0$., 0.5 mm thick and 102 mm long; fabricated from rods by electro-erosion technique; $\gamma-6$ transition reported at 1682 K; melting point 1808 K; specimen heated to measuring temperature in one second by passing current through; uncorrected for thermal expansion; smoothed data from table. |
| 63 | 154 | Cezairliyan, A. and McClure, J.L. | 1973 | | 1500-1660 | Y iron 2 | Similar to the above specimen (one of this or the above specimen has an electrical resistivity value of 10.2 x 10^{-6} M m at 273 K). |
| 3 | 154 | Cezairliyan, A. and McClure, J.L. | 1973 | | 1700-1800 | ő iron l | The same specimen as for Data Set 62. |
| 65 | 151 | Cesairliyan, A. and McClure, J.L. | 1973 | | 1700-1800 | ô iron 2 | The same specimen as for Data Set 63. |
| 99 | 179 | Miccolai, G. | 1908 | £ | 84-673 | | 0.5 mus in diam and 5 mms long; from Firma C.A.F. Kahlbaum. |
| 674 | 180 | Wruck, D. and Wert, C. | 1955 | Λ | 293 | | 99.95 pure; 0.04 0, little metallic impurity. |
| 48 9 | 180 | Wruck, D. and Wert, C. | 1955 | > | 93 | | Same as above; foil polycrystal, 0.008 cm x 0.2 cm x 4 cm; Run II. |
| # 69 | 180 | Wruck, D. and Wert, C. | 1955 | Α | 93 | | Same as above; Run II. |
| 10* | 180 | Mruck, D. and Mert, C. | 1955 | Δ | 93 | | Same as above; Run IV. |
| 71* | 180 | Wruck, D. and Wert, C. | 1955 | > | Ľ | | Same as above except wire specimen; 0.0762 cm in diam and 15 cm long; grain size ~0.6 cm; decarbonized. |
| 72* | 180 | Wruck, D. and Wert, C. | 1955 | > | 11 | | Same as above. |
| 73* | 180 | Mruck, D. and Wert, C. | 1955 | Λ | μ | | Same as above. |
| 74* | 181 | Rosenberg, H.M. | 1955 | ~ | 1.8-77 | JM 4975 (Run 2) | 99.99 pure (excluding gases); from Johnson and Matthey Co.; polycrys- talline; 0.202 cm in diam and 2.89 cm long; annealed in vacuum for several houra. |
| 75 | 146 | Powell, R.W., Tye, R.P., and Woodman, M.J. | 1961 | ~ | 1088-1196 | 18 AF 3 | 0.007 Cu and Ni each, 0.0058 C, 0.004 Mn and Si each, 0.003 S, 0.0023 N, 0.002 Cr, <0.001 Al, <0.001 P, 0.0008 O, and <0.000005 H; measured during heating of the sample at a rate of 0.25 K min ⁻¹ , data uncorrected for thermal expansion. |
| 764 | 146 | Powell, R.W., et al. | 1961 | × | 1160-1191 | 18 AF 3 | The above specimen measured during cooling. |
| " | 146 | Powell, R.W., et al. | 1961 | ~ | 4-1073 | 18 AF 3 | The above specimen measured at lower temperatures; smoothed values from table. |
| Mot | ahow | on either figure. | | | | | |

| | | | | IN THE NEW YORK | | AN INE PLANTAN | Presiditition the (continued) |
|-------------|-----|--|------|-----------------|------------------------------------|-------------------------------------|--|
| k sta | | Author (s) | Year | Me thod Used | T em p. Range , K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
| 184 | 123 | Taylor, G.R., Isin, A., and Coleman, R.V. | 1963 | ¥ | 191-191 | Specimen #25 | One of iron whisker specimens 100-300 µ in diam and about 2 cm long. |
| #6L | 123 | Taylor, G.R., et al. | 1963 | | 77-300 | | Same as the above; resistivity values calculated from reported resistance ratios $R(T)/R(77 K)$ and $p(77 K)$ given in the above data set; average of seven specimens. |
| 8 | 182 | Soffer, S., Diessen, J.A., and Pugh, E.M. | 1965 | 4 | 76-300 | | <0.0185 metallic impurities; zone-refined; 0.1 cm x 1 cm x 10 cm. |
| 81* | 183 | Yoshikawa, A. and Okamoto, M. | 1967 | ۲ | 77,273 | | Zone refined iron (total impurity less than 0.001X); grain <70 μ in diam; decarburized at 973 K for 7 days in wet hydrogen stream; ultrasonically cleaned; chemically polished with HF + H50; heat treated at 773 K for 14 days in hydrogen purified by zirconium hydride; annealed at 773 K for 30 min; then cooled at 15 K hr ⁻¹ ; room temperature value calculated from reported resistance ratio (p_{223} K/ p_{77} K). |
| 82* | 184 | Takamura, S., Maeta, H., and Okuta, S. | 1968 | 4 | 4.2,293 | | 99.996 pure, 0.0008 C, 0.007 N and O each, from Materials Research Corp.; wire specimen 0.12 mm in diam; as received condition: value at room temperature calculated from reported resistivity ratio and re- sidual resistivity. |
| 8 3# | 184 | Takamura, S., et al. | 1968 | × | 4.2,293 | | Same as the above specimen except annealed at 773 K for 1 h in vacuum and then at 973 K for 1 h. |
| 5 | 184 | Takamura, S., et al. | 1968 | ۲ | 4.2,293 | | Similar to the above. |
| 85# | 184 | Takamura, S., et al. | 1968 | ¢, | 4.2,293 | | Similar to the above. |
| 8 | 31 | White, G.K. and Woods, S.B. | 1959 | ۲ | 4.2-295 | Fe 2 | 99.97 pure, ~0.004 S1, <0.004 Co, Cu, and Ni each, ~0.003 Mo and Mn each, <0.00015 N, and traces Pb and Zr; 0.05 mm x 1 mm x 6-8 cm; from Vacuum Metals Co.; zone-melted in wet hydrogen to obtain large crystals; electrically annealed at 873 K to remove hydrogen; resignivity calculated from reported $\rho_1(T)$, $\rho(4.2K)/\rho(295K) = 9.61 \times 10^{-3}$, and $\rho_1(295K) = 9.62 \times 10^{-6}$ Cm. |
| 874 | 165 | Smith, A.W., Gregory, J.H., and Lynn, J.T. | 1946 | 6 | 293 | | "Chemically pure"; wire specimen 0.1019 cm in diam and 15.2 cm long. |
| 1 | 165 | Smith, A.W., et al. | 1946 | Ξů | 293 | | "Chemically pure"; wire specimen 0.0823 cm in diam and 15.5 cm long. |
| ŝ | 185 | Smith, A.W., et al. | 1946 | £ | 293 | | "Chemically pure"; wire specimen 0.0406 cm in diam and 5.0 cm long. |
| 2 | 165 | Seith, A.V., et al. | 1946 | œ | 293 | | "Chemically pure"; wire specimen 0.0201 cm in diam and 3.4 cm long. |
| let l | For | on either figure. | | ļ | | | |

| Manden, F.M., 191) A. 28-1167 CO. Standard Lice and L | 1220 | 18 | anther(s) | Ĭ | | įį | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--|------|-----|--|----------|-----------|-----------------------|-------------------------------------|--|
| 0 Interts, V.V., INJ 1441-204 Inter-School (1994) 1441-204 Inter-School (1994) | | 1 | | (141 | ~ | 288-1167 | | 0.03 impurities; well annealed iron supplied by Johnson and Matthey Co.; average grain size 2 um; measured in vacuum (~10 ⁻⁵ mmHg) under quasistatic condition with heating rate not more than 1 K/min. |
| 1 10 C 100 C 000 S 000 | 2 | 8 | | 1963 | - | 1448-2094 | | 99.0 pure; by carbonyl method or electrolytically; liquid state ob- tained by meiting in graphite crucible either in a helium atm or in vacuum. |
| mediate 1.1. 191 M-H-1013 99.9 ⁺ press frame Goodfallow Metala Left. Equal 11.0 cm x 2.0 cm x 1.0 cm x 1.0 cm x 2.0 cm x 1.0 cm x 1.0 cm x 2.0 cm x 1.0 cm x 1.0 cm x 2.0 cm x 1.0 cm x | 8 | Â | Anthread, 1.1. and | 6791 | υ | 1808 | | 99.998 pure, frow Johnson and Matthey Co., in liquid state; tempera- ture = 1808 K assumed. |
| 9.131hulkeek, G.1954V328-11300.027 Nu, 0.027 Nu, 0.027 Nu, 0.007 St, 0.007 S | 1 | Ĩ | | 1974 | ۲ | 344-1015 | | 99,99 ⁺ pure; from Goodfellow Metals Ltd., England; 1.0 cm x 2.0 cm x 4.0 cm; annealed at 1473 K for 24 h under vacuum. |
| We 13 Malleel, G. 1936 V 1004-121 The above speciaen while feating. 91 133 bulleel, G. 1936 V 1003-1230 The above speciaen while feating. 91 133 bulleel, G. 1936 V 1003-1230 The above speciaen while feating. 91 133 bulleel, G. 1936 V 1163-1186 The above speciaen backing at a rate of 0.23 K ath ⁻¹ . 91 133 bulleel, G. 1936 V 1163-1186 The above speciaen backing at a rate of 0.23 K ath ⁻¹ . 91 bulleel, G. 1935 V 1163-1186 The above speciaen backing at a rate of 0.23 K ath ⁻¹ . 91 bulleel, G. 1935 Y 1163-1186 The above speciaen for functing have volt 1961; 1960; 1961; 196 | 8 | 5 | hai bach, c. | 10% 1 | > | 92 8- 1150 | | 0.027 Mm, 0.02 C, 0.018 P, 0.017 S, 0.007 S1, 0.005 N and traces Ni; Armeco from manufactured by the basic 0.H. technique; inclusions not detectable by microscope; 1.3 cm in diam and about 15 cm long; measured with a current of 20-30 A, and in vacuo; this curve represents coinci- dent values during both heating and cooling (rate 1-1.5 K/min). |
| 13 malack, G. 1956 V 1003-1220 The above speciaen while heating. 13 malack, G. 1956 V 1174-1136 The above speciaen bating at a rate of 0.25 K min⁻¹. 199 13 malack, G. 1956 V 1163-1136 The above speciaen cooling at a rate of 0.25 K min⁻¹. 100 130 malack, G. 1956 V 1163-1136 The above speciaen cooling at a rate of 0.25 K min⁻¹. 101 130 Landmarry, E.V., and Barvey, J.S., Popeciaen ane as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen ane as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Popeciaen asse as used in Kaufmann, L., Løyenaar, A., and Barvey, J.S., Sani, Popeciaen assertional area to 100207 (J-0.00207); values from tron from Actin, Poh. 2007 (J-0.0029); values apeciaen assertion, P.N., P.N. | ž | 153 | Buildech, G. | 1956 | * | 1004-1221 | | The above specimen while cooling. |
| 13 Malaet, G. 1936 V 1174-1196 The above specimen heating at a rate of 0.25 K min⁻¹. 14 Malaet, G. 1956 V 1163-1136 The above specimen could at rate of 0.25 K min⁻¹. 16 Malaet, J. 1956 V 1163-1136 The above specimen could at rate of 0.25 K min⁻¹. 16 Martie, L., 1956 V 1163-1136 The above specimen could at rate of 0.25 K min⁻¹. 16 Martie, L., 1951 32-1425 Specimen asse a used in Kaufmann, L., Løyenar, A., and Marvey, J.5., progress in Very High Pressure Kasserch, p. 89, Miley, New York, 1961; assetting the search of 0.25 K min⁻¹. 16 Martie, D.M. 1897 3 273-1036 Specimen asse a used in Kaufmann, L., Løyenar, A., and Marvey J.5., progress in Very High Pressure Kasserch, p. 89, Wiley, New York, 1961; assetting the search of 0.25 K min⁻¹. 10 Mortis, D.M. 1897 3 273-1036 Specimen Asset assetting to 113 K; realizated fram frames reporting attent progress actional area 0.131 K⁻¹ and mean ring diameter 2.135 cm⁻¹ assetting to 1.11 m⁻¹ and mean ring diameter 2.135 cm⁻¹ assetting to 1.11 m⁻¹ and the mating the rate of 0.123 K; relating the rate of 0.131 K⁻¹ and the search of 0.132 K; relating the rate of 0.132 K; relating to 1.11 m⁻¹ and the rating diameter 2.135 cm⁻¹ and the rate of 0.133 K; relating to 1.11 m⁻¹ and the rate of 0.133 K; relating to 1.113 K⁻¹ and the rate of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating the rate of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating the rate of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating the rate of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating the rate of 0.133 K; relating to 1.113 K⁺¹ and trace of 0.133 K; relating the rate o | | 661 | muldet. G. | 1956 | > | 1003-1220 | | The above specimen while heating. |
| Mallack, G. 1956 V 1163-1166 The above specimen cooling at a rate of 0.25 K afn⁻¹. Referent, L., Leyenar, A., and Marvey, J.S., Specimen and an automative section. P. 89 villey, Ward Vork, 1961; Progress in Very High Prenuce Research, p. 89 villey, Ward Vork, 1961; Progress in Very High Prenuce Research, p. 89 villey, Ward Vork, 1961; Progress in Very High Prenuce Research, p. 89 villey, Ward Vork, 1961; Progress in Very High Prenuce Research, p. 89 villey, Ward Vork, 1961; Progress in Very High Prenuce Research, p. 89 villey, Values from reported under the statistic villed from reported magnetic restatistic on 1133 K; restatistic villed from reported magnetic restatistic on 1133 K; restatistic villed from reported magnetic restatistic on 1133 K; restatistic on 1029 (1-0,027); values from table. Norris, D.M. 1897 B 273-1036 Specimen A Charcoal Iron; from Meser, Jos. Sanky and Sons; ridg shape specimen of corns section. Besource during cooling after heated to 133 K; density 7,775 g cm²; secured during cooling after heated to 133 K; during 100 110 100 100 110 100 100 110 100 110 100 100 110 100 100 100 100 100 | • | 51 | Bulleck, G. | 1956 | > | 1174-1198 | | The above specimen heating at a rate of 0.25 K min ⁻¹ . |
| 19 kurfman, L., Leyenaar, A., and Marvey, J.S., Cloumberty, L.V., and Misa, R.J. 1943 kurfman, L., Leyenaar, A., and Marvey, J.S., Frogress in Very High Pressure Research, p. 89, villey, Worked angestic resistivity: plangestic) = p - 0.0297 (1-0.0029); values from table. 101e 130 Morris, D.M. 1897 B 273-1036 Specimen A Charcoal Iron; from Messr. Jos. Sankey and Sons: ring shape specimen of cross sectional area 0.131 cs⁻¹ and mean ring diameter 2.35 cs; density 7.775 g cs⁻¹; measured during heating. 102e 130 Morris, D.M. 1897 B 273-1323 Specimen A Charcoal Iron; from Messr. Jos. Sankey and Sons: ring shape specimen of cross sectional area 0.131 cs⁻¹ and mean ring diameter 2.35 cs; density 7.775 g cs⁻¹; measured during to 1193 K; measured during cooling after heated to 1321 K; Curis temperature 1068 K. 102 130 Morris, D.M. 1897 B 273-1323 Specimen A choce specimen after reheating to 1193 K; measured during cooling after heated to 1321 K; Curis temperature 1068 K. 104 130 Morris, D.M. 1897 B 273-1099 Specimen B constituent in for Messr. Indiang cooling after annealing at 1113 K; Curis viab cross sectional area 0.143 cs⁻¹ and santed during cooling after annealing at 1113 K; Curis canter into for Messr. | 1 | 5 | Buildet, G. | 1956 | > | 1163-1186 | | The above specimen cooling at a rate of 0.25 K min ⁻¹ . |
| 101e 130 Morris, D.M. 1397 B 273-1036 Specimen A Charcoal Iron; from Messr. Jos. Sankey and Sons; ring shape specimen of cross sectional area 0.131 cm² and wean ring diameter 2.35 cm; density 7.775 g cm⁻¹; measured during heating. 102e 130 Morris, D.M. 1897 B 273-1323 Specimen A The above specimen; measured during cooling after heated to 1323 K; Curfe temperature 1068 K. 103e 130 Morris, D.M. 1897 B 289-1158 Specimen A The above specimen imeasured during cooling after heated to 1323 K; Unite, D.M. 1897 B 289-1158 Specimen A The above specimen after reheating to 1193 K; measured during cooling. 104a 130 Morris, D.M. 1897 B 273-1099 Specimen B 0.075 impurities, including C, P and Si, and traces of Mn; Swedish transformer from from Messr. Jos. Sankey and Sons; ring shape specimen vith cross sectional area 0.143 cm² and mean ring diam 2.23 cm; density 7.461 g cm⁻⁹; measured during cooling at 1113 K; Curfe | 2 | 5 | Kaufaan, L., Clougherty, E.V., and Meise, R.J. | 1963 | | 325-1425 | | Specimen same as used in Kaufmann, L., Leyenaar, A., and Harvey, J.S., Progress in Very High Pressure Research, p. 89, Wiley, New York, 1961; swaged; $\alpha \gamma \gamma$ transition 1183 K; resistivity calculated from reported magnetic resistivity: $\rho(\alpha_{S}) = \rho - 0.029T$ (1-0.002P); values from table. |
| 102* 150 Norris, D.M. 1897 B 273-1323 Specimen A The above specimen; measured during cooling after heated to 1323 K; Lurie temperature 1068 K. 103* 130 Norris, D.M. 1897 B 289-1158 Specimen A The above specimen after reheating to 1193 K; measured during cooling. 104* 130 Norris, D.M. 1897 B 273-1099 Specimen B 0.075 impurities, including C, P and S1, and traces of Mn; Swedish transformer from from Messr. Jos. Sankey and Sons; ring shape specimen vith cross sectional area 0.143 cm² and mean ring diam 2.23 cm; density 7.461 g cm⁻³; measured during cooling at 1113 K; Curie temperature 1055 K. | 101* | 150 | Morris, D.M. | 1897 | • | 273-1036 | Specimen A | Charcoal Iron; from Messr. Jos. Sankey and Sons; ring shape specimen of cross sectional area 0.131 cm^2 and mean ring diameter 2.35 cm ; density 7.775 g cm^{-3} ; measured during heating. |
| 1034 150 Morris, D.M. 1897 B 289-1158 Specimen A The above specimen after reheating to 1193 K; measured during cooling. 1044 150 Morris, D.M. 1897 B 273-1099 Specimen B 0.075 impurities, including C, P and S1, and traces of Mn; Swedish transformer from from Messr. Jos. Sankey and Sons; ring shape specimen with cross sectional area 0.143 cm ² and mean ring diam 2.23 cm; density 7.461 g cm ⁻² ; measured during cooling after annealing at 1113 K; Curie temperature 1055 K. | 102* | 150 | Norris, D.M. | 1897 | æ | 273-1323 | Spectmen A | The above specimen; measured during cooling after heated to 1323 K; Curie temperature 1068 K. |
| 10.075 impurities, including C, P and SI, and traces of Mn; Svedish transformer from from Messr. Jos. Sankey and Sons; ring shape specimen with cross sectional area 0.143 cm ² and mean ring diam 2.23 cm; density 7.461 g cm ⁻⁹ ; measured during cooling after annealing at 1113 K; Curie temperature 1055 K. | 101 | 81 | Morris, D.M. | 1897 | a | 289-1158 | Specimen A | The above specimen after reheating to 1193 K; measured during cooling. |
| | 104. | 130 | Morris, D.M. | 1897 | \$ | 273-1099 | Specimen B | 0.075 impurities, including C, P and SI, and traces of Mn; Swedish transformer iron from Messr. Jos. Sankey and Sons; ring shape specimen with cross sectional area 0.143 cm ² and mean ring diam 2.23 cm; density 7.461 g cm ⁻³ ; measured during cooling after annealing at 1113 K; Curie temperature 1055 K. |

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| | . Author (s) | Year | Nethod Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|----------|--|------|----------------|-------------------|-------------------------------------|--|
| 2 | 0 Motris, D.M. | 1897 | n î | 273-1423 | Specimen B | The above specimen measured during cooling after annealing at 1423 K Curie temperature 1051 K. |
| 61 | 0 Arajs, S., Schwerer, F.C., and Fisher, R.M. | 1969 | ~ | 4.2 | | 99.9 ^{\pm} pure; electrolytic; about 5 mm in diam and 50 mm long. |
| 11 | 2 Schwerer, F.C., Conroy, J.W., and Arajs, S. | 1969 | ۲ | 4.5-300 | | 0.002 C and 0.001 N, "high purity iron standard"; 0.508 cm in diam and 5 cm long; annealed at 1273 K for 1 week under vacuum; machined, reannealed at 1123 for 2 h; data at T \geq 50 K calculated from reported residual resistivity (0.08 x 10 ⁻⁶ R m) and smoothed ideal resistivity (from graph); measured with a current of 0.1 A. |
| 3 | l Shirakawa, Y. | 1939 | | 78-1123 | | 0.05 P and Si each, 0.04 C, 0.02 Co and Mn each, 0.01 Al and 0.003 S; electrolytic from Nippon-Deukai-Seitetausho; 0.0617 cm in diam and 5.25 cm long; annealed at 1273 K for 1 h under vacuum with specimen axis in the east-west direction; slow-coded; lead wires of nickel soldered by pure silver; reannealed at 1123 K for 1 h under vacuum and slow-cooled; measurement done with sample axis in east-west direc- tion. |
| 4 | l Hayer, A.R. | 1161 | > | 273-1273 | | Chemically pure; '0.015 Si02, 0.004 Cu and Ni each, <0.001 Mn and trace S1; from Kahlbaum; impurities analyzed by Physikalisch-Technischen Reichaanstalt; measured by AC voltage-current method; smoothed values from table; except for value at 293K which is measured separately by a DC voltage-current method. |
| 61 | l Meyer, A.R. | 1161 | ٨ | 273-1273 | | 99.94 pure charcoal iron from Armeco; other information same as above. |
| 19 | l Meyer, A.R. | 1161 | ٨ | 273-1173 | | <0.008 S, 0.007 P and traces C, Cu, Mn, and Si; from Langbein- Pfunhauser-Werke; other information same as above. |
| ~ | l Lavin, E.S., Ayushine, G.D., and Gel'd, P.V. | 1972 | æ | 1923 | | 99.988 pure, carbonyl iron class V-3; measurements carried out in aluminum or zirconium oxide crucibles covered with lapped lids in purified helium at a pressure of 760 mmHg; pure tungsten used as comparison standard. |
| 19 | 2 Cumenyuk, V.S. and Lebedev, V.V. | 1959 | | 309~1718 | | High purity iron obtained by vacuum distillation; total impurity 0.023 estimated from residual resistivity; specimen $3-6$ mm in diam and $50-100$ mm long; annealed at 1373 K for 4 h in high vacuum; measured in a vacuum of $10^{-5}-10^{-6}$ mmHg. |
| 51 | 6 Beum, B.A., Gel'd, P.V., and Tyagunov, G.V. | 1967 | t | 1551-2018 | | 99.99 pure carbonyl iron; remelted in a hydrogen atm and degassed in vacuum in the molten state; measured by "refluence method" of Baum et al., Izv. Akad. Nauk SSSR, Neorg. Materialy, <u>1</u> , 1289(1965) in pure helium at a pressure of 780 mamig; tungsten used as comparison standard |

| <pre>1# 195 Tanaka, K. and 1972 A 77,298 RE 0.0060 S, 0.0040 C, Mn Watanabe, T. Unite and Cast in vacuum; sur and cast in vacuum; sur in diam; wire specimen</pre> | Composition (weight percent), Specifications and Remarks 99.9 ⁺ pure: liquid state; contained in a 10 mm 1.D. recrystall slumina crucible at a pressure of 0.05-01 mmdg; data of Saito et al. (Bull. Kes. Inat. Min. Dress. Metall., Tohoku Univ. 22. 67, 109, 1969) used for calculating speciemn volume. 0.02 Mm, 0.01 Cr, and <0.01 Co; single crystal; 0.2 x 0.3 x 1.5 polished and acried in BG1 + 10X H20; Curte temperature 1040 inncorrected for thermal expansion; data in table form supplied first author. "High purity"; measured in purified helium. "High purity"; measured in purified helium. "Pure"; obtained by some measured by an exploiding wire techniqu heated by an almost rectanguiar shape pulse ('JO ⁵ s); current "Pure"; obtained by some mealting; residual resistivity ratio 23 temperature dependent part of resistivity reported. "Pure"; obtained by some melting; residual resistivity ratio 23 temperature dependent part of resistivity reported. Same as the above. Specimen contained in either alumina or zirconia crucible, meas in a mark of helium. 0.0166 M, 0.00048 C, 0.0003 60, 0.0003 51, 0.0002 Cu and Mm each, onool M, and P each; grain diam 50 4 20 um; 0.5 mm in diam and long; from Johnson and Matthey; heated at 1246 K for 48 h in we drogen; and 2 h in vacuum; carbon or nitrogen in solution (0.0002 0.0060 S, 0.00040 C, M and Si each; 0.0003 51, nould onooz Cu; re- electrolytic from supplied by benko Co; melted by induction he and case in vacuum; surface layer removed; hor-swaged into rod in diam; wire speciaen prepared in similar manner as above. | Name and Specimen JM RE | Temp. Range, K 1773-1898 1873 1873 1809 2.4-63 2.4-78 1573,1873 1573,1873 1573,298 77,298 | Tethod Ceed dd A A A A A A A A A A A A A A A A A A | Year 1972 1974 1976 1976 1976 1971 1972 1972 | Author(a) Author(a) Choo, T. and Yagi, T. Ono, Y. and Yagi, T. Saehra, M.S., Capan, V.L., and Silinsky, P. Dubini, E., and Vacolin, N.A. Labedev, S.V., and Vacolin, N.A. Labedev, S.V., and Vacolin, N.A. Labedev, S.V., and Vacolin, N.A. Fert, A. and Campbell, I.A. Fert, A. and Campbell, I.A. Baum, B.A., Tanaka, K. and Matanabe, T. Matanabe, T. | Raf. H | |
|--|---|-------------------------------------|--|--|--|--|------------------------------|---|
| | 0.0400 Ti; "C, N, O and B atoms in solid solution extremely low pared from re-electrolytic iron by alloying with Ti; specimen p tion same as the above except for no annealing in wet hydrogen. | E | 77,298 | < | 1972 | Tanaka, K. and Watanabe, T. | 195 | |
| a 195 Tanaka, K. and 1972 A 77,298 RE 0.0060 S, 0.0040 C, Mn | 0.0060 S, 0.0040 C, Mn and Si each; | RE | 77,298 | ۲ | 1972 | Tanaka, K. and | 195 | |
| | 0.0166 N, 0.0048 C, 0.0036 O, 0.0003 Si, 0. <0.0001 Al and P each; grain diam $50 \pm 20 \mu$ long; from Johnson and Matthey; heated at 1 drogen; and 2 h in dry hydrogen; cold rolle annealed at 823 K for 1 h in dry hydrogen; 923 K for 3 h in vacuum; carbon or nitrogen | £ | 77,298 | < | 1972 | Tanaka, K. and Watanabe, T. | 195 | • |
| 195 Tanaka, K. and 1972 A 77,298 JM 0.0166 N, 0.0068 C, 0.0 Watanabe, T. <0.0001 Al and P each; | Specimen contained in either alumina or zircon in an atm of helium. | | 1573,1873 | œ | 1971 | Baum, B.A., Tyagunov, G.V., Cel'd, P.V., and Khasin, G.A. | 159 | _ |
| 159 Baum, B.A., 1971 R 1573,1873 Specimen contained in e fragunov, G.V., Tyagunov, G.V., and Tyagunov, G.V., and Khasin, G.A. 195 Tanaka, K. and 1972 A 77,298 JM 0.0166 N, 0.0048 C, 0.0 (not set in the fraction of the fr | Same as the above. | | 2.4-78 | < | 1976 | Fert, A. and Campbell, I.A. | 127 | |
| 127 Fert, A. and 1976 A 2.4-78 Same as the above. Campbell, I.A. 1971 R 1573,1873 Specimen contained in e in an atm of helium. 159 Buum, B.A., 1971 R 1573,1873 Specimen contained in e in an atm of helium. 159 Buum, B.A., 1971 R 1573,1873 Specimen contained in e in atm of helium. 159 Buum, B.A., 1971 R 1573,1873 Specimen contained in e in atm of helium. 150 Buum, B.A., Image: G.V., Image: G.V., Image: G.V., Image: G.V., 195 Tanaka, K. and 1972 A 77,298 JM 0.0166 M, 0.0048 C, 0.0 Vatanabe, T. Image: True 1972 A 77,298 JM 0.0166 M, 0.0048 C, 0.0 Vatanabe, T. Image: Group of the in atm of the achine of the in atmost of the in atmosto | "Pure"; obtained by sone melting; residual resistiv temperature dependent part of resistivity reported. | | 2.4-63 | × | 1976 | Fert, A. and Campbell, I.A. | 121 | |
| 127 Fert, A. and 1976 A 2.4-63 "Fure"; obtained by son temperature dependent p campbell, I.A. 127 Fert, A. and 1976 A 2.4-78 Same as the above. Campbell, I.A. 139 Baum, B.A., 1971 R 1573,1873 Specimen contained in e fin an atm of helium. Cal'd, P.V., and Khasin, G.A. 195 Tanaka, K. and 1972 A 77,298 JM 0.0166 N, 0.0048 C, 0.0 % attanabe, T. 195 Tanaka, K. and 1972 A 77,298 JM 0.0166 N, 0.0048 C, 0.0 % attanabe, T. | <pre><0.2 C; in liquid state; measured by an exploding wir heated by an almost rectangular shape pulse ($^{100.5}$ s); 14 x 10¹⁶ A/m²; voltage and current measured by pulse</pre> | | 1809 | + | 1974 d | Lebedev, S.V., Savvatimekii, A.I., an Smirnov, Yu.B. | 194 | |
| 194 Lebedev, S.V., 1974 + 1809 Sarvatiamitii, A.I., and Sairnov, Yu.B. Sairnov, Yu.B. 127 Fert, A. and 1976 A 2.4-63 "Pure": obtained by son temperature dependent p tentus. 139 Baum, B.A., 1971 R 1573,1873 Specimen contained in e tentus. C.e.i (d, P.V., and the tentus. C.e.i (d, P.V., and the tentus. C.e.i (d, P.V., and tentus. C.e.i (d, P.V., and tentus. C.e.i (d, P.V., and tentus. T.e.i (d), P.V., and tentus. T.e.i (d), P.V., and tentus tentus | "High purity"; messured in purified helium. | | 1873 | | 1969 | Dubini, K., Esin, O.A., and Vecolin, N.A. | 19 3 | |
| 193 Dubini, E., 1969 1873 "High purity"; messured tests (a factor), and vacolin, N.A. 194 Labodev, S.V., and Sarraciamiti, A.I., and 1976 A 2.4-63 "Pure": obtained by son temperature dependent p Campbell, I.A. 127 Tert, A. and 1976 A 2.4-63 "Pure": obtained by son temperature dependent p Campbell, I.A. 128 Eart, A. and 1976 A 2.4-78 Same as the above. Campbell, I.A. 129 Baum, B.A., 1971 R 1573,1873 Speciaen contained in e thore. Cambbell, I.A. 139 Baum, B.A., 1971 R 1573,1873 Speciaen contained in e thore. Cambbell, I.A. 139 Tanka, K. and 1972 A 77,298 JH 0.0166 M, 0.0048 C, 0.0 Matanabe, T. 139 Tanka, T. and 1972 A 77,298 JH 0.0166 M, 0.0048 C, 0.0 Matanabe, T. | 0.02 Mn, 0.01 Cr, and <0.01 Co; single crystal; 0.2 x 0 polished and etched in BCl + 10% M2O2; Curie temperatur uncorrected for thermal expansion; data in table form s first author. | | 1000-1087 | < | 1974 | Seehra, M.S., Capan, V.L., and Silinsky, P. | 149 | |
| 14) Seekra, M.S., 1974 A 1000-1067 0.02 km, 0.01 Cr, and c Capana, V.L., and C Capana, C V. C Capana, V.A. 1969 1974 1974 1974 1974 1974 1974 1974 197 | 99.9 [†] pure; liquid state; contained in a 10 mm I.D. recr alumina crucible at a pressure of 0.05-0.1 mmHg; density Saito et al. (Bull. Res. Inst. Min. Dress. Metall., Toho 25, 67, 109, 1969) used for calculating specimen volume. | | 1773-1898 | Q4 Q4 | 1972 1977 | Ono, T. and Yagi, T. Ono, Y. | 8 | |
| 89 One, Y. and Yagi, T. 1372 R 1773–1896 99.9 ⁺ pure: liquid atat aunita cruchls at a Saito et al. (blu). Ness Saito b.N., and 1974 A 1000-1087 0.02 Ms, 0.01 Cr, and closen and etched in uncorrected for thermal. 193 Dubini, E., Saito, N.A. 1969 1873 0.02 Ms, 0.01 Cr, and | Composition (weight percent), Specifications and Re | Name and Specimen Designation | Temp. Range, K | Method Used | Year | Author (s) | . 1 2 2 2 | |

* Not shown on either figure.

| I.B. Manulater, H., and N. M. (2) A. (2) and the strategy and former constant to the strategy for the strategy and former constant to the strategy for the strategy and former constant to the strategy and strategy and | . | žź | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--|--------------|--------|---|------|----------------|-------------------|-------------------------------------|--|
| Wannelane, N., et el. Wannelane, N., et el. A 4.2 Banlar to the above except containing 0.003 interestitial C. Wannelane, N., et el. A 4.2 Stanlar to the above except containing 0.003 interestitial C. Wannelane, N., et el. A 4.2 Mannelane, N., et el. A 4.2 Stanlar to the above except containing 0.003 interestitial C. Mannelane, N., et el. A 4.2 Mannelane, N., et el. A 4.2 Mannelane, N., et el. I) A 4.2 Stanlar to the above except containing 0.03 N. Mannelane, N., et el. I) A 4.2 Mannelane, N. Mannelane, N., et el. I) A 4.2 Mannelane, N. Mann | 1254 | 136 | Wagenblast, K., Schwerer, F.C., and Horak, J.A. | 1971 | < | 4.2 | | 0.005 interstitial C; specimen prepared from vacuum melted iron with <0.1 at.% impurities; drawn and evaged to 0.6 mm in diam and 11.3 cm long wire; annealed at 1023 K for 15 min; annealed 1058 K for 5 h in wet hydrogen and furnace cooled in dry hydrogen to reduce carbon and nitrogen to 0.004 and 0.0004 at.%, respectively; carbonized by heating at 938 K for 16 h in a hydrogen-methane mixture; quenched in brine. |
| 1279 194 Wagmablast, R., et el. 1971 A 4.2 Staliar to the above except containing 0.005 interestitial C. 1289 196 Wagmablast, R., et el. 1971 A 4.2 Staliar to the above except containing 0.005 interestitial C. 1290 196 Wagmablast, R., et al. 1971 A 4.2 0.012 interestifial With architer 0.095 interestifial C. 130 196 Wagmablast, R., et al. 1971 A 4.2 Staliar to the above except containing 0.057 W. 1310 196 Wagmablast, R., et al. 1971 A 4.2 Staliar to the above except containing 0.104 W. 1310 196 Wagmablast, R., et al. 1971 A 4.2 Staliar to the above except containing 0.104 W. 1310 196 Wagmablast, R., et al. 1971 A 4.2 Staliar to the above except containing 0.104 W. 1311 196 Wagmablast, R., et al. 1971 A 4.2 Staliar to the above except containing 0.104 W. 1312 197 A 4.2 Staliar to the above except containing 0.104 W. 198 1313 197 A 4.2 3.13 at | 1264 | 196 | Wagenblast, H., et al. | 1971 | < | 4.2 | | Similar to the above except containing 0.022 interstitial C. |
| Warenblanc, N., et al. [37] Matter to the above except containing 0.108 N. Warenblanc, N., et al. [39] A. 4.2 Statiar to the above except containing 0.108 N. Warenblanc, N., et al. [39] A. 4.2 Statiar to the above except containing 0.138 N. Price, D.C. and [39] A. 4.2 Statiar to the above except containing 0.138 N. Wattiffaaa, G. Wattif | 127# | 196 | Wagenblast, N., et al. | 1971 | ¥ | 4.2 | | Similar to the above except containing 0.005 interstitial C. |
| 129 19 4.1 4.2 0.012 Interesticial N; specialmy preparation stailar to the above accept containing 0.007 N. 129 19 19 4.2 3141ar to the above accept containing 0.007 N. 131 19 Megenblast, N., et al. 1971 A. 4.2 3141ar to the above accept containing 0.104 N. 131 19 Megenblast, N., et al. 1971 A 4.2 3141ar to the above accept containing 0.104 N. 132 19 Megenblast, N., et al. 1971 A 4.2 3141ar to the above accept containing 0.104 N. 132 19 Megenblast, N., et al. 1971 A 4.2 3141ar to the above accept containing 0.104 N. 133 19 A 4.2 314ar to the above accept containing 0.104 N. 4.22 134 10 A 4.2 314ar to the above accept containing 0.104 N. 4.2 135 19 A 4.2 314ar to the above accept containing 0.104 N. 4.2 135 19 A 4.2 314ar to the above accept containing 0.104 N. 4.2 4.2 0.012 Interesticity 0.104 N. 4.2 0.012 N. 0.11100 N. 0.012 N | 1284 | 196 | Wagenblast, H., et al. | 1791 | 4 | 4.2 | | Similar to the above except containing 0.098 interstitial C. |
| How 196 Wagenblart, M., et al. 1971 A 4.2 Stallar to the above except containing 0.105 W. Wagenblart, M., et al. 1971 A 4.2 Stallar to the above except containing 0.138 W. Wagenblart, M., et al. 1971 A 4.2 Stallar to the above except containing 0.138 W. Price, D.C. and 1973 A 4.2-276 Price, D.C. and 1973 A 4.2-276 Price, D.C. and 1973 A 4.2-276 Price, D.C. and 1974 A 4.2-276 Price above except containing 0.138 W. Walliews, G. and 1973 A 4.2-276 Price, D.C. and 1973 A 4.2-276 Price above except containing 0.138 W. Walliews, G. and 1974 A 4.2-276 Price above except containing 0.138 M. Walliews, T. and 1974 A 4.2-276 Price above except containing 0.138 M. Walliews, T. and 1974 A 4.2-276 Stallar to the above except containing 0.138 M. Walliews, T. and 1974 A 4.2-276 Stallar to the above except containing 0.138 M. Walliews, T. and 1974 A 4.2-276 Stallar to the resultivity, pi, P = P₁ + p(4.2 M). Modryen, Ta Walliews, T Startin, A.W. 1962 R 1011-2000 Price 0.05 A 10 Figures detect containing 0.148 M. Startin, A.W. 1962 R 1011-2000 Price 0.05 A 10 Figures detect containing 0.148 M. Stallar to the resultivity plane figures detect containing 0.148 M. Stallar to the resultivity of the resultivity plane tablement to the respected containing 0.148 M. Stallar to the resultivity of the resultivity plane tablement to the respected containing 0.15 M. Stallar to the resultivity above 1 tablement to the respected containing 0.15 M. Stallar to the resultivity plane tablement to the respected containing 0.15 M. Stallar to the resultivity plane tablement to the respect of containing 1.4 Points 100 M. Stallar to the resultivity plane tablementer tablet (1.4, 0.0, 0.10, 1.0, 1.0, 1.0, 1.0, 1.0, 1. | 129* | 196 | Wagenblast, H., et al. | 1971 | ۲ | 4.2 | | 0.012 interstitial N; specimen preparation similar to the above except nitrogenized by heating at 748 K in a hydrogen-ammonia mixture. |
| 131 196 Wagenblast, H., et al. 1971 A 4.2 Staliar to the above except containing 0.104 H. 132 196 Wagenblast, H., et al. 1971 A 4.2 Staliar to the above except containing 0.138 H. 137 196 Wagenblast, H., et al. 1971 A 4.2 Staliar to the above except containing 0.138 H. 138 197 7 4.2 Staliar to the above except containing 0.138 H. 138 197 7 4.2 Staliar to the above except containing 0.138 H. 138 197 7 4.2 Staliar to the above except containing 0.148 H. 138 197 7 4.2 Staliar to the above except containing 0.158 H. 138 197 7 4.2 Staliar to the above except containing 0.158 H. 138 197 Vasiler in vascum at 1173 K for 2 D. Madreter extended of the above except contains of except to the above except to the abov | 130* | 196 | Wagenblast, H., et al. | 1791 | ۷ | 4.2 | | Similar to the above except containing 0.057 N. |
| Wagenblast, H., et al. 1971 A 4.2 Wagenblast, H., et al. 1971 A 4.2 Wagenblast, H., et al. 1971 A 4.2 Price, D.C. and 1973 A 4.2-216 Price, D.C. and 1973 A 4.2-216 Prise (1) 2 0.2 x 10 cm i applied by Johnson and Matt Villiams, G. Wall'evs, R.P. and 1973 A 4.2-216 Wastl'evs, R.P. and 1973 A 4.2-216 Wastl'evs, R.P. and 1973 A 4.2-216 Wastl'evs, R.P. and 1974 A 10-1149 Tot 2 x 10 cm i applied by Johnson and Matt Price, D.C. and 1974 A 10-2716 Wastl'evs, R.P. and 1974 A 132-775 Wastl'evs, R.P. and 1974 A 132-773 Wastl'evs, R.P. and 1974 A 132-773 Wastl'evs, R.P. and 1974 A 132-773 Schwerz, F.C. and 1970 Y 4.2-1200 Schwerz, F.C. and 1970 Y 4.2-1200 | *IEI | 196 | Magenblast, H., et al. | 1971 | V | 4.2 | | Similar to the above except containing 0.104 N. |
| 137 136 Wagenblast, N., et al. 1971 A 4.2 138 136 Wagenblast, N., et al. 1973 A 4.2-276 99965 preci 0.15 x 0.2 x 10 cm; unpiled by Johnson and Matt Williams, G. 135 197 Vasil'eva, R.P. and 1974 373-775 99965 preci 0.15 x 0.2 x 10 cm; unpiled y Johnson and Matt Bartyon, Ya. 136 148 Goherer, F.C. and 1974 373-773 No details reported (4.2 K) = 0.3300 x 10³ fm and respected of each seast set of the resistivity, pri p = p_T + p(4.2 K). 136 148 Goherer, F.C. and 1970 V 4.2-1200 Octails reported (4.2 K) = 0.3300 x 10³ fm and respected of the resistivity, pri p = p_T + p(4.2 K). 136 148 Goherer, F.C. and 1970 V 4.2-1200 Octails reported (4.2 K) = 0.034 x 10⁶ fm and respected of the resistivity, pri p = p_T + p(4.2 K). 137 8 Goherer, F.C. and 1970 V 4.2-1200 Octails reported (4.2 K) = 0.034 x 10⁶ fm and respectator deperture dependence. 137 9 Samurin, A.M. 1962 R 1811-2000 Meanured by the rotaxing field action maged; average of two ape (4.1 K). A.M. 1962 R 1811-2000 Meanured apalater the resistivity value fmoler atom respected Sections from graph. 138 135 Powell, R.W. 1953 - 279-1793 Meanured Matther frames from graph. 138 135 Powell, R.W. 1953 - 279-1793 Meanured Matther value from septemation respected Sections from septemation from the resistivity value calculated from respected for the resistivity above 1 meanured under vacuums resistivity above 1 arcs emported for the part from graph. 138 135 Powell, R.W. 1953 - 279-1793 Meanured Matther Values from graph. | 132* | 196 | Wagenblast, H., et al. | 1971 | V | 4.2 | | Similar to the above except containing 0.138 N. |
| 134 80 Price, D.C. and 1973 A 4.2-276 99.985 pure; 0.15 x 0.2 x 10 cm; supplied by Johnson and Matt Villiams, G. 135 197 Vasil'eva, R.P. and 1974 373-773 Rot of the resistivity, pr; p = p_T + p(4.2 K). 136 148 Schwerer, F.C. and 1970 V 4.2-1200 04.6 m in diam coorted from swaged; average of two are ouddy. L.J. 137 94 Samarin, A.M. 1962 R 1011-2000 Meanued by the rotating field activity of an alter apperature distribution. A.M. 1962 R 2000 05. (1.1.47-0.0.10) fin and temperature destribution. A.M. 1962 R 1011-2000 01. (1.1.47-0.0.10) fin and temperature destribution. A.M. 1962 R 1011-2000 01. (1.1.47-0.0.10) fin and temperature destribution. A.M. 1962 R 1011-2000 01. (1.1.47-0.0.0.4 x 10⁻⁶ fin activity value of anothen atm apperation. A.M. 1962 R 1011-2000 00. (1.1.47-0.0.0.4 x 10⁻⁶ fin activity value of anothen atm apperation. A.M. 1962 R 1011-2000 01. (1.1.47-0.0.0 x 10⁻⁶ fin activity value of anothen atm apperation. (1.1.47-0.00 x 10⁻⁷ fin activity value of anothen atm apperation. (1.1.47-0.00 x 10⁻⁷ fin activity above 1.1.41, not on a stativity above 1.1.41, not on attivity above | 133* | 196 | Wagenblast, H., et al. | 1971 | ۲ | 4.2 | | Similar to the above except containing 0.158 N. |
| 135 197 Vasil'eve, R.P. and 1974 373-773 No details reported. 136 148 Schwerer, F.C. and 1970 V 4.2-1200 0.64 x 10⁻⁶ fined iron; swaged; average of two spe 0.40, μ.J. 137* 94 Samarin, A.M. 1962 R 1811-2000 Measured by the rotating field method in a helium atm: apparent ibrated against the resistivity value of moleculated from reported 5et 139; resistivity value of moleculated from reported 5et 139; resistivity value of moleculated from reported 11.47-0.50 x 10⁻⁷ 7(C)] x 10⁶ dm⁻¹cm⁻¹; upper temperature limit 2000 K. 138 135 Powell, R.W. 1953 + 279-1793 "High purity" iron; measured under vacuum; resistivity above 1 are amoothed values from graph. | 134 | 80 | Price, D.C. and Williame, G. | 1973 | ۹. | 4.2-276 | | 99.9985 pure; 0.15 x 0.2 x 10 cm; supplied by Johnson and Matthey Co.; prepared by cold rolling rod stock between Melinex sheets; etched; annealed in vacuum at 1173 K for 2 h; guenched; resistivity calculated from reported $\rho(4,2 \text{ K}) = 0.3300 \times 10^{-6} \Omega \text{m}$ and temperature dependent part of the resistivity, ρ_T ; $\rho = \rho_T + \rho(4,2 \text{ K})$. |
| 136 143 Schwerer, F.C. and 1970 V 4.2-1200 V.B. m in diam; zone-refined iron; waged; average of two spectrum days. L.J. Cuddy, L.J. 137* 94 Samarin, A.M. 1962 R 1811-2000 Measured by the rotating field method in a helium atm; apparate the resistivity value of molten iron reported Set 139; resistivity value of aolten iron reported Set 139; resistivity value of aolten iron reported conductivit [1.47-0.50 x 10 ⁻³ 7(C)] x 10 ⁴ dm ⁻¹ cm ⁻¹ ; upper temperature limit 2000 K. 136 155 Powelli, R.W. 1953 + 279-1793 "High purity" iron; measured under vacuum; resistivity above 1 are smoothed values from graph. | 135 | 197 | Vasil'eva, R.P. and Kadyrov, Ya. | 1974 | | 373-773 | | No details reported. |
| <pre>137* 94 Samarin, A.M. 1962 R 1811-2000 Measured by the rotating field method in a helium atm; apparat 157* 139; reaistivity value of molten from reported 1647-0.50 x 10⁻³T(C)] x 10⁴ dm⁻¹cm⁻¹; upper temperature Mait 11.47-0.50 x 10⁻³T(C)] x 10⁴ dm⁻¹cm⁻¹; upper temperature Mait 2000 K. 138 155 Powell, R.W. 1953 + 279-1793 "High purity" from; measured under vacuum; resistivity above 1 are smoothed values from graph.</pre> | 136 | 148 | Schwerer, F.C. and Cuddy, L.J. | 1970 | Λ | 4.2-1200 | | $\sim 1.8~\text{mm}$ in diam; zone-refined iron; swaged; average of two specimens; $\rho(4.2~\text{K}) \sim 0.04~\text{x}~10^{-8}~\Omega~\text{m}$; smoothed values from graph. |
| <pre>136 155 Powell, R.W. 1953 + 279-1793 "High purity" from; measured under vacuum; resistivity above l are smoothed values from graph. * Not shown on either figure.</pre> | 137* | 46 | Semarin, A.M. | 1962 | 6 4 | 1811-2000 | | Measured by the rotating field method in a helium atm; apparatus cal- ibrated against the resistivity value of molten iron reported in Data Set 139; resistivity value calculated from reported conductivity: $[1.47-0.50 \times 10^{-3}T(C)] \times 10^{4} dm^{-1}cm^{-1}$; upper temperature limit assumed 2000 K. |
| * Not shown on either figure. | 138 | 155 | Powell, R.W. | 1953 | • | 279-1793 | | "High purity" iron; measured under vacuum; resistivity above 1623 K are smoothed values from graph. |
| | | Evolts | on either figure. | | | | | |

TABLE 8. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF IRON Fe (continued)

A DESCRIPTION OF THE OWNER OF THE

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فللمتكافية ومعمده كالمتكار مايدية فسمانات متعانيتها بتقريبات ويتعاد
| | <u>,</u> | Author (a) | Year | Me thod Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------|----------|-------------------------------|------|-----------------|-------------------|-------------------------------------|---|
| 139 | 51 | Powell, R.W. | 1953 | + | 1181 | | In molten liquid state; resistivity measured by immersing a specially constructed alumins tube in molten iron; current and potential contacts made by tungten rods through separate holes, in the middle of the wall of the tube, which are open to the axial hole through small up-turned channels; reported value mean of 24 measurements with two heating rates of the specimen and with two different durations of the measuring current. |
| 140# | 108 | Schimank, H. | 1914 | ¢ | 20-273 | Pe I | High grade pure electrolytic iron; from Kalbaum; 1-2 m long; drawn by Heraeous of Nanau. |
| 141* | 108 | Schimank, H. | 1914 | 2 2 | 20-273 | Fe 11 | Same as the above except annealed in nitrogen atm. |
| 142* | 198 | Holborn, L. | 1919 | | 80-784 | Fe I ₁ | Electrolytic iron, from vacuum melted iron supplied by Firma W.C. Herseous; wire specimen 0.2 mm in diam; heated for several min at 773 K. |
| 143# | 198 | Holborn, L. | 1919 | | 81-761 | Fe I ₂ | Same as the above except annealed at 573 K for 3 h. |
| 144* | 198 | Holborn, L. | 1919 | | 80-572 | Fe II | 0.004 Co, Cu and Nieach, 0.001Mn, traces of C, 0 and Si; "Nitrateisen" made from iron nitrate by Firma C.A.F. Kalbaum; drawn from 5 um to 0.2 mm in diam; annealed at 653 K for 3 h. |
| 145# | 104 | Meissner, M. and Voigt, B. | 1930 | + | 1.4-273 | fe l | Specimen same as for Data Set 142; 0.2 mm in diam and 55 mm long; distance between potential contacts 50 mm; tempered; measured by com- pensation method; resistivity calculated from reported resistance ratio, ice point resistance (0.149 ß) and sample dimensions. |
| 146* | 104 | Meissner, M. and Voigt, B. | 1930 | t | 1.4-273 | Fe 2 | Specimen same as for Data Set 144; 0.2 mm in diam and 59.7 mm long; distance between potential contacts 56.6 mm; tempered; measurement method and resistivity calculation same as above. |
| 147 | 104 | Meissner, M. and Voigt, B. | 0661 | + | 1.4-273 | Fe 2* | Same as the above specimen except 60 mm long and distance between potential contacts 56.3 mm. |
| 148 | 101 | Meissmer, M. and Voigt, B. | 1930 | t | 2.0-273 | Fe 3 | Specimen same as for Data Set 10; tempered; 1.0 mm in diam and 33.0 mm long; distance between potential contacts 30.0 mm; measurement method and resistivity calculation same as above. |
| 149 | 101 | Meissner, M. and Voigt, B. | 1930 | t | 2.0-273 | Fe 4 | Electrolytic iron from Firma Heraeus; 1.0 mm in diam and 58.2 mm long; stretched; course grained; distance between potential contacts 53.4 mm; measurement method and resistivity calculation same as above. |
| 1504 | 104 | Meissner, M. and Voigt, B. | 0661 | + | 1.4-273 | Fe 5 | Specimen obtained from Dr. Kreussier; 0.1 am in diam and 58.6 mm long; distance between potential contacts 54.2 mm; measurement method and resistivity calculation same as above. |
| * Not | shown | on either figure. | | | | | |

| 3 8 4 | 122 | Author (s) | Tear | Me thod Used | Temp. Renge, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--------|-------------------|--|--------------|-----------------|-------------------|-------------------------------------|---|
| 13 | ş | Mainemer, N. and Yoigt, B. | 0061 | + | 1.4-273 | Fe 6 | Same as the above specimen except 58.4 mm long and annealed at 573 K for 3 h; distance between potential contact 54.4 mm. |
| *** | 5 | Heismer, N. and Yoigt, J. | 0661 | t | 1.4-273 | Fe 7 | Electrolytic (5 times) iron from Firma Siemens and Matske; 0.3 mm in diam and 58.7 mm long; distance between potential contacts 54.0 mm; measurement method and resistivity calculation same as above. |
| 5 | Ŋ | Muleaner, N. and Yoigt, B. | 0661 | • | 1.3-273 | Fe 10 | The above specimen annealed at red-bot, 15 h and etched; 57.5 wm long distance between potential contacts 51.7 wm. |
| * | 101 | Meisemer, M. and Voigt, B. | 0661 | t | 1.4-273 | Fe 8 | Same as the above specimen except annealed at 573 K for 3 h; distance between potential contacts 54.4 mm. |
| ž | 101 | Meisener, N. and Voigt, B. | 1930 | • | 1.4-273 | Fe 9 | Same as the above specimen etched; 57.8 mm long; distance between po- tential contacts 55.1 mm. |
| e 9 | 125 | trusse ll, C.W., Christopher, J.E., and Coleman, R.V. | 1970 | 4 | 0.3-1.2 | | <100> iron whisker; measured in a magnetic field of 570 Oe. |
| *15 | ٠ | Matthiessen, A. and Voigt, C. | 1864 | | 273 | | Hard-drawn; resistivity value calculated from reported ratio of resistivities of silver and iron, with $p(silver)$ assumed to be 1.468 x 10^{-3} Ω m. |
| * | 199 | Potter, H.H. | 1937 | | 20-1130 | | 99.96 pure; chief impurities are 0 and Si; from Messr. Adem Hilger; U-shape specimen 2 mm in diam and 8 cm long. |
| 1 | 200 | Ribbeck, F. | 1926 | + | 273-1273 | | 0.07 Mm, 0.014 P, and traces of Si, Cu, S and Cr; electrolytic; 0.3-0.4 cm ² x 10 cm; measured by compensation method with current 2-3 A. |
| ş | 102 | Bhegat, S.M., Anderson, J.R., and Wu, M. | 1967 | | 84-297 | | <pre><111> from whiskers; about 0.2-0.4 mm wide and 8 mm long; grown by hydrogen reduction of FeCl; either at room temperature using hydrogen saturated with water vapor or at 1023 K with a hydrogen flow rate of 300 ml/min; electropolished; measured in a longitudinal magnetic fie of 2 kG.</pre> |
| •19 | 202 | Mussery-Tasey, G. | 1950 | | 194-1208 | | No details reported. |
| 2 | 203 126 | Sudovtaov, A.I. and Summeriko, E.E. Summeriko, E.E. and Sudovtaov, A.I. | 1957 1962 | ~ ~ | 1.2-4.2 | | 99.98 pure; polycrystalline specimen in the form of thin ribbons fro Hilger; $R(4.2K)/R(273K) = 3.9328 \times 10^{-2}$; resistance at 273K, 0.5091 R(T)/R(273K) = 3.92930 $\times 10^{-2}$ with T extrapolated to 0 K. |
| 2 | 126 | Sementeo, E.E. and Sudovteov, A.I. | 1962 | ۲ | 1.3-20.3 | | >99.99 pure; grain size ~ 0.1 mm; ~ 0.1 mm "transverse dimension" 36 m long; needle-shaped specimen grown by distillation in vacuum; $R(T)/R(273K) = 3.9606$ x 10 with T extrapolated to 0 K; measured under condition where the earth's magnetic field is compensated by Helmhol colls; specimen demagnetized with a 50 cps magnetic field of decreasi applitude after each reversal in measuring current. |

* Not shown on either figure.

| Det: Set No. | Ref. | TABLE Author (s) | 8. Year | EASUREMENT Method Used | INFORMATION Temp. Range, K | ON THE ELECTRICA Name and Specimen Designation | L RESISTIVITY OF IRON Fe (continued) Composition (weight percent), Specifications and Remarks |
|--------------------|-------|---|------------|------------------------------|----------------------------------|---|--|
| 180 | 124 | Beitchman, J.G., Trussel, C.W., and Coleman, R.V. | 1970 | ~ | 0.4-1.2 | T-7 | The above specimen measured in a longitudinal magnetic field of 1230 De. |
| 181 | 124 | Beitchman, J.G., et al. | 1970 | ¥ | 0.3-1.2 | T-7 | The above specimen measured in a longitudinal magnetic field of 1520 Oe. |
| 1824 | 124 | Beitchman, J.G., et al. | 1970 | ~ | 1.0-4.1 | T-7 | The above specimen measured in a longitudinal magnetic field of 1150 Oe. |
| 1834 | 124 | Beitchman, J.G., et al. | 1970 | v | 1.4-4.3 | B-1 | Single crystal; specimen axis in a <111> direction; measured in a longitudinal magnetic field of 1200 Oe. |
| 1844 | 124 | Beitchman, J.G., et al. | 1970 | ۷ | 4.7-21 | B-1 | The above specimen, measured at higher temperatures. |
| 185 | 205 | Swartz, J.C. and Cuddy, L.J. | 1970 | > | 4.2 | | Zone-refined iron; 0.13-0.40 mm in diam and 5-10 cm long; resistivity value calculated from reported $\rho(295k)/\rho(4.2K) = 180$, with $\rho(295k)$ taken to be 10.19 x 10^{-6} G m. |
| 1861 | 611 | Arajs, S., Oliver, B.F., and Michalak, J.T. | 1967 | ¥ | 4.2 | I | 99.9966 pure; 0.0019 C, 0.0011 O and 0.0004 others (at. x); interfacial grain area 7.0 mm ⁻¹ ; 1 mm in diam and about 80 mm long; produced by oxidation zone refining (oxygen activity v 1). |
| 1874 | 611 4 | Arajs, S., et al. | 1967 | V | 4.2 | 11 | 0.0019 C, 0.0018 O and 0.0042 others $(at.x)$; polycrystalline; interfacial grain area 14.3 mm ⁻¹ , 80 cm long. |
| 1884 | 119 | Arajs, S., et al. | 1967 | A | 4.2 | 11 | Same as the above except interfacial grain area 16.5 mm ⁻¹ . |
| 1894 | 112 | Fujii, T. and Morimoto, I. | 1968 | ۲ | 4.2 | Fe I | 0.0300 C (determined by vacuum combustion method), 0.0100 N and 0 each (determined by vacuum fusion method, and 0.0015 total metallic impurity; polycrystalline material obtained from Johnson and Matthey Co.; formed into a bar 5 mm in diam and 20 cm long; swaged into cylindrical rod 2.7 mm in diam and 50 cm long; annealed at 1163 K; chemically pollished in a 500-1-500 solution of $H_2O-HF-C_2H_5OH$, removing a surface layer of 0.1 mm; resistivity value calculated from reported $\rho(295K)/\rho(4.2K)$, with $\rho(295K)$ taken to be 9.91 x 10^{-9} Am. |
| 1904 | 112 | Fuji, T. and Morimoto, I. | 1968 | ۲ | 4.2 | Fe I | Same specimen material as the above, prepared by a method similar to the above but exact treatment not given; resistivity calculated by some method as above. |
| *191 | 112 | Fujii, T. and Morimoto, I. | 1968 | ~ | 4.2 | Fe II | 0.0300 C, 0.0100 0, and 0.0015 N (determined by the same methods as for Data Set 189), and 0.0015 total metallic impurity; from the same specimen material as the above; zone-refined (1 pass at 3 mm min ⁻¹ in dry H ₂); other preparations same as the above except annealed at 1123 K for 20 h in a vacuum of 2 x 10^{-6} mm before chemical polishing; resistivity calculated by same method as above. |
| 192* | 112 | Fujii, T. and Morimoto, I. | 1968 | ~ | 4.2 | Fe 111 | 0.0100 0, 0.0080 N, 0.0030 C (determined by same methods as for Data Set 189), and 0.0015 total metallic impurity; prepared from the same material and by a similar method as the above except decarbonized at 1023 K for 200 h in wet H_2 ; resistivity calculated by same method as above. |
| * Mot | shown | on either floure. | | | | | |

| Renarks | ar method as ulated by the | | | ethods as for -refined (1 pass sbove; resis- | ar method as ulated by the | | | | race N (deter- (1 pass at er preparations | ar method as ulated by same | | od O (determined (2 passes at m and 2 passes e above; resis- | g each, and sured by an d values from | |
|--|---|-------------------------------|-------------------------------|--|---|-------------------------------|-------------------------------|-------------------------------|---|--|-------------------------------|---|---|--|
| Composition (weight percent), Specifications and | Prepared from the same specimen material and by a simil the above, but exact method not given; resistivity calc same method as above. | Same as the above. | Same as the above. | 0.0030 C, <0.0005 N, 0.0004 C (determined by the same m Deta Set 189); and 0.0015 total metallic impurity; zone at 0.3 mm min ¹ in dry H_2); other preparations same as tivity calculated by same method as above. | Prepared from the same specimen material and by a simil the above; but exact method not given; resistivity calc same method as above. | Same as the above. | Same as the above. | Same as the above. | 0.0020 C, 0.0001 0, 0.015 total metallic impurity and t mined by same method as for Data Set 189); zone-refined 0.3 mm min ⁻¹ and 5 passes at 1 mm min ⁻¹ in dry H ₂); oth and restativity calculation same as the above. | Prepared from the same specimen material and by a simil the above, but exact method not given; resistivity calc method as above. | Same as the above. | <0.0010 C, 0.015 total metallic impurity and traces Naby the same methods as for Data Set 189); zone-refined 0.3 mm min ⁻¹ in vet E., 5 passes at 1 mm min ⁻¹ in vacuu at 1 mm min ⁻¹ in dry H ₂); other preparations same as the trutty calculated by same method as above. | 99.99 pure; 0.0003 Ca and Si each, 0.0002 Al, Cu, and M 0.0001 Ag. Cr, Mn, and Ni each (chemical analysis); mea exploding wire technique; measurement error 4%; smoothe curve; values corrected for thermal expansion. | |
| Name and Spectmen Designation | | | | Fe IV | | | | | | | | | | |
| Temp. Range, K | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 1007-2997 | |
| Method Used | ۲ | < | < | ۲ | ۲ | v | × | v | ۲ | < | < | ۲ | • | |
| Year | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1968 | 1977 | |
| Author (s) | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fuji1, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Fujii, T. and Morimoto, I. | Seydel, U. and Fucke, W. | |
| | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 112 | 81 | |
| F S E | 193* | 194* | 195* | 196* | 197* | 198 | 199* | 200* | 201 | 202* | 203 | 204 | 205 | |

* Not shown on either figure.

| 73 Güntler, N., 133 - 123-131 91.99 puts, 0.005 C and N activity ar current and petential connect with Nature N. S. Matter, N., and J. M. 1913 73 Bater, T.K. 1913 74 P. S. Matter, N., and S. M. 1914 75 Bater, T.K. 1917 76 Bater, T.K. 1917 77 Bater, C.F. Matter, 1000 0 and 0.0001 ki Material connection at Nature Natu | 3 | 2 2 2 | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--|----------|-----------|---|--------------|----------------|-------------------|-------------------------------------|--|
| 206 Bolder, T.K. 1971 A 90-400 207 Erford, C. and Y. and S. 2001 B. Watterfold of Comp. 2002 For an erectival from smoothed values are related from smoothed values are related from smoothed values are related from smoothed values control in the smoothed value are related from smoothed values are related values are value value values are related values are related | <u>ب</u> | 92 110 | Güntherodt, H.J. Hauser, E., Künzi, H.U., and Wüller, R. | 1975 1976 | + | 1726-1915 | | 99.999 pure from Johnson and Matthey Co.; measured with potential method in which the sample material was enclosed within an alumina tube with four protrusions serving as current and potential contacts. |
| B01 Erehov, G.S., 1914 1828–2065 99.97⁺ proce: meanured by a contact method fn a heilua area with appendixed in Arithmetica Matteria (1911 11) I 11 Outkenahteria, M.Y. and 1911 A 4.2-46 I 12 Outkenahteria, M.Y. and 1911 A 4.2-46 I 13 Outkenahteria, M.Y. and 1911 A 4.2-46 I 14 Outkenahteria (1912 M 1912 A 1.2-46) I 14 Outkenahteria (1912 M 1912 A 1.2-46) I 15 Outkenahteria (1912 M 1912 A 1.2-46) I 14 Outkenahteria (1912 M 1912 A 1.2-46) I 15 Outkenahteria (1912 M 1912 A 1.2-46) I 10 Outkenahteria (1912 M 1912 A 1.1-46) I 11 14 Outkenahteria (1912 M 1912 A 1.1-46) I 11 14 14 14 14 14 14 14 14 14 14 14 14 | ± | 206 | Holder, T.K. | 1977 | < | 90-400 | | 99.99 pure, 0.0025 C and N each, 0.0007 O and 0.0001 H; Material Research Corp. MARZ grade 3 pass zone refined iron; smoothed values from table; p(273.15K)/p(4K) = 189. |
| 113 Volkenshtedin, N.V. and 1971 A 4.2-46 Period Prove Manual Structure of Control Methy Society of Link Weight and Parties V. 2011 A 4.5-494 The above meanured in an applied longitudinal aggnetic field of 1.1 k Takina, V.P. 113 Volkenshtein, N.V. and 1971 A 4.5-494 The above meanured in an applied longitudinal aggnetic field of 1.1 k Takina, V.P. 113 Volkenshtein, N.V. and 1971 A 4.5-494 The above meanured in an applied longitudinal aggnetic field of 1.1 k Takina, V.P. 113 Volkenshtein, N.V. and 1971 A 4.5-494 The above meanured in an applied longitudinal aggnetic field of 1.1 k Takina, V.P. 113 Volkenshtein, N.V. and 1971 A 4.5-494 The above meanured in an applied transverse aggnetic field of 1.1 k Construction. 113 Volkenshtein, N.V. and 1973 - 1695-1895 Oc.066 K, 0.006 S, 0.005 Si, -0.005 G, and Cr ach, 0.001 ha and P organish. 114 No. 113 Volkenshtein, N.V. and 1973 - 1695-1895 Oc.066 K, 0.006 Si, -0.005 G, and Cr ach, 0.001 ha and P organish. 114 No. 115 Vika, Y., et al. 119 A - 1675-1895 Oc.066 K, 1960, 1990, 1895, 1813, 1913, 1931, 193 | - | 207 | Ershov, G.S., Kasatkin, A.A., and Gavrilin, I.V. | 1974 | | 1828-2065 | | 99.997 ⁺ pure; measured by a contact method in a helium atm with speci- men inside a vertical alundum crucible; liquid metal column 40-50 mm long. |
| 113 Volkensktedn, W.V. and 1971 A 4.5-494 The above measured in an applied longitudinal magnetic field of 1.1 k Yakina, V.P. 113 Volkenskein, W.V. and 1971 A 4.4-46.1 The above measured in an applied transverse magnetic field of 1.1 k Volkenski, v.P. 113 Volkenski, V.P. and 1971 A 4.4-46.1 The above measured in an applied transverse magnetic field of 1.1 k Volkenski, v.P. 124 Kita, V.P. and 1971 A 4.4-46.1 The above measured in an applied transverse magnetic field of 1.1 k Volkenski, v.P. 137 Kita, Y., et al. 1978 - 1695-1895 0.006 K, 0.006 S, 0.003 St, 0.003 Gu and Cr each, 0.003 hm ad P volkenski, in a vacua Nortica, 2. 93 Kita, Y., et al. 1978 - 167-1919 1.135, 1131, 1695 K; values from tables augmited by authors: values from tables augmited by authors; values from tables from tables, isol, 1930, 1931, 1930, 1931, 1931, 1931, 1931, 1931, 1931, 1931, 1931, 1 | _ | 113 | Volkenshtein, N.V. and Yakina, V.P. | 161 | ~ | 4.2-46 | Fe-4 | Polycrystalline specimen from Johnson and Matthey Co.; O.1 mm thick, 3.0 mm wide and 15 mm long; vacuum $(10^{-6}$ mmMg) annealed at 1273 K for 1 h, demagnetized; measuring current density 3.3 A mm ⁻² . |
| 113 Volkemähtein, N.V. and 1971 A 4.4-46.1 The above measured in an applied transverse magnetic field of 1.1 is braina, V.F. 1334, 1393, 1364, 1300, 1303, 1304, 1309, 1305 | * | 113 | Volkenshtein, N.V. and Yakina, V.P. | 161 | v | 4.5-494 | | The above measured in an applied longitudinal magnetic field of 1.1 kOc. |
| 93 Kita, T., 1978 - 1695-1895 0.008 Ki, 0.003 Si, <0.003 Si, <0.003 Gi and Cr each, 0.000 Mn and P each action an wich the anticur processention in which the action 2. | | 113 | Volkenshtein, N.V. and Yakina, V.P. | 1971 | ~ | 4.4-46.1 | | The above measured in an applied transverse magnetic field of 1.1 kDe. |
| 93 Kita, Y., et al. 1978 - 1676-1919 Same as the above; a second welt; temperature sequence: 1823, 1842 1874, 1893, 1905, 1919, 1900, 1875, 1854, 1803, 1776, 1766, 1741, 1720, 1699 and 1676 K. 93 Kita, Y., et al. 1978 + 1673-1973 Same as the above; a third melt; temperature sequence: 1823, 1843, 1866, 1876, 1869, 1805, 1915, 1996, 1869, 1870, 1841, 18 1825, 1845, 1865, 1875, 1915, 1915, 1966, 1870, 1841, 18 1825, 1845, 1865, 1876, 1809, 1905, 1915, 1996, 1800, 1803, 1913, 18 1825, 1845, 1845, 1845, 1865, 1875, 1915, 1996, 1869, 1870, 1841, 18 1822, 1977, 1764, 1748, 1728, 1906, 1896, 1890, 1841, 18 1822, 1977, 1915, 1996, 1809, 1800, 1841, 18 1822, 1977, 1764, 1748, 1728, 1906, 1804, 1850, 1841, 18 1822, 1777, 1764, 1748, 1728, 1708, 1897, 1864, 1850, 1841, 18 1802, 1777, 1764, 1748, 1728, 1708, 1897, 1864, 1850, 1841, 18 1802, 1777, 1764, 1748, 1728, 1708, 1897, 1894, 1850, 1841, 18 1802, 1114pov, 5.1., and Litaitskii, B.S. 157 Araentiav, P.P., 1970 + 1693-1874 Sectimen produced from electrolytic powder of composition: 0.23 C, Fillipov, S.I., and Litaitskii, B.S. 157 Araentiav, P.P., 1970 + 1693-1874 Sectimen produced from electrolytic powder of composition: 0.23 C, Fillipov, S.I., and Litaitskii, B.S. 157 Araentiav, P.P., 1970 + 1693-1874 Sectimen produced from electrolytic powder of composition: 0.23 C, Fillipov, S.I., and Litaitskii, B.S. | | 93 | Kita, T., Ohguchi, S., and Morita, Z. | 1978 | + | 1695-1895 | | 0.008 Ni, 0.006 S, 0.005 Si, <0.005 Cu and Cr each, 0.003 Mn and P each, and 0.002 C; measured with a four probe method in which the electrodes are made of the same material as the specimer, in a vacuum of 10 ⁻⁴ Torr; data points are taken at temperatures in the sequence: 1833, 1854, 1864, 1890, 1895, 1872, 1835, 1835, 1316, 1799, 1786, 1759, 1735, 1713, 1695 K; values from table supplied by authore; values corrected for thermal expansion. |
| 93 Kita, Y., et al. 1978 + 1673-1973 Same as the above; a third melt; temperature sequence: 1823, 1843, 1856, 1876, 1898, 1905, 1917, 1910, 1894, 1879, 1850, 1851, 18 1829, 1845, 1853, 1876, 1878, 1893, 1910, 1894, 1850, 1850, 1841, 18 1829, 1845, 1876, 1876, 1876, 1876, 1876, 1876, 1896, 1870, 1894, 1850, 1850, 1851, 18 1829, 1845, 1865, 1876, 1876, 1876, 1893, 1910, 1894, 1850, 1850, 1851, 18 1829, 1845, 1865, 1876, 1876, 1878, 1910, 1894, 1850, 1850, 1851, 18 1829, 1845, 1865, 1876, 1876, 1878, 1910, 1894, 1850, 1864, 1850, 1841, 18 1829, 1845, 1764, 1764, 1764, 1706, and 1673 K. 157 Arsentiev, P.P., 1970 + 1693-1874 Specimen produced from electrolytic powder of composition: 0.23 C, Fillipov, S.I., and 157 Arsentiev, P.P., 1970 + 1693-1874 0.015 0, 0.012 0, 0.012 6, 0.005 F and 51 each, and trace Mn; melted in hyd gen atm; electrical restrivity reported is the same as that report for a 0.005 C specimen; measured with a potential method with tungs electrodes; experimental chamber evacuated before heating and then filled with pure Pe; measured while heating. | | 93 | Kita, Y., et al. | 1978 | t | 1676-1919 | | Same as the above; a second melt; temperature "equence: 1823, 1842, 1857, 1874, 1893, 1905, 1919, 1900, 1875, 1858, 1816, 1817, 1803, 1798, 1776, 1760, 1741, 1720, 1699 and 1676 K. |
| * 157 Arsentiev, P.P., 1970 + 1693-1874 Specimen produced from electrolytic powder of composition: 0.23 C, Fillipov, S.I., and trace Mn; melted in a hyd gen atm; electrical resistivity reported is the same as that report for a 0.005 C specimen; measured with a potential method with tungs electrodes; experimental chamber evacuated before heating and then filled with pure Pe; measured while heating. | | 33 | Kita, Y., et al. | 1978 | t | 1673-1973 | | Same as the above; a third melt; temperature sequence: 1823, 1843, 1866, 1876, 1889, 1905, 1915, 1937, 1915, 1896, 1869, 1830, 1831, 1814, 1829, 1845, 1863, 1878, 1893, 1910, 1894, 1879, 1864, 1850, 1841, 1817, 1802, 1777, 1764, 1748, 1728, 1708, and 1673 K. |
| | * | 157 | Arsentiev, P.P., Fillipov, S.I., and Liteitskii, B.S. | 1970 | t | 1693-1874 | | Specimen produced from electrolytic powder of composition: 0.23 C, 0.015 O, 0.012 S, 0.005 P and Si each, and trace Mn; melted in a hydro- gen atm; electrical resistivity reported is the same as that reported for a 0.005 C specimen; measured with a potential method with tungsten electrodes; experimental chamber evacuated before heating and then filled with pure Fe; measured while heating. |

| | żż | Author (s) | Year | Me thod Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------|-------|---|------|-----------------|-------------------|-------------------------------------|---|
| 216* | 151 | Arsentiev, P.P., Fillipov, S.I., and Litaitakii, B.S. | 1970 | + | 1683-1874 | | The above; measured while cooling. |
| 217 | 147 | Lauchbury, M.D. and Saundere, N.H. | 1976 | ~ | 373-1128 | | <0.03 Mm and <0.01 Cu, Si, Ca, and Mg each; cylindrical specimens 1.5 mm or 2 mm in diam and ~20 mm long, machined from 5 mm diam poly- crystalline rods from Johnson and Matthey Co.; annealed at 1250 K for several hours in an argon atm; random measurement error 11. |
| 218 | 128 | Janos, S., Kovac, L., and Niynek, R. | 1972 | | 9.9-28 | | Only temperature dependent part of resistivity reported; values from graph. |
| 219 | 115 | Isshiki, M. and Igaki, K. | 1978 | 4 | 1.7~271 | | High purity, prepared by floating zone refining and heated treated at 1073 K for 24 h in wet hydrogen described by authors in Trans. Jpn. Inst. Metals, <u>18</u> , 413, 1977; specimen then electropolished in 95% acetic acid and 5% perchloric acid from a diam of 500 µm to 150 µm; about 10 cm in length; measured in a longitudinal applied magnetic field of 60 KAm ⁻¹ ; values from graph. |
| 220 | 113 | lsshiki, M. and Igaki, K. | 1978 | 4 | 1.7~301 | | Similar to the above except specimen diam reduction from 500 µm to 180 µm. |
| 221 | 113 | leshiki, M. and Igaki, K. | 1978 | < | 1.7-268 | | Signilar to the above except specimen diam reduction from 500 µm to 190 µm. |
| 222 | 115 | Isshika, M. and Igaki, K. | 1978 | 4 | 1.6-164 | | Similar to the above. |
| 223 | 511 | leshiki, M. and Igaki, K. | 1978 | 4 | 1.6-292 | | Similar to the above excent specimen diam reduction from 500 µm to 350 µm. |
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| * Not | shown | on either figure. | | | | | |

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[Temperature, T, K; Electrical Resistivity, p, 10⁻⁴ Am]

| G | SET 17 (con | 14. | 16. 16. | DATA SET 1 | | 1.63 0. | 3.14 0. | 4.33 0. | 6.30 0. | 9.02 0. | 10.7 0. | | DATA SET 19 | | 13 10. | '3 14. | · 3 22. | ·3 31. | 13 42. | 13 54. | '3 69. | 3 86. | 3 106. | '3 III. | 115. | '3 118. | | ATA SET 20 | 1 | 16.5 5. | 3.2 6. | 5.3 7. | 01.1 10. | 19.7 I3. |)6.6 16. | | DATA SET 21 | | 18.2 10. | 11. 2.6 | 3.2 14. | 13.2 18. | 3.2 21. | |
|---|-------------|-------|---------------|------------|--------|---------|---------|---------|---------|---------|---------|--------|-------------|--------|--------|--------|----------------|--------|--------|---------|--------------|--------|---------------|---------|-------|----------------|--------|------------|--------|----------------|---------|---------|----------|----------|-----------------|--------|-------------|--------|-------------|---------|---------|----------|---------|-------------|
| + | DATA | 96 | 07 | | | | | | | | 80 | | | | 29 | 37 | 47 | 57 | 67 | 11 | 87 | 16 | 107 | 111 | 127 | 137 | | | | 19 | 22 | 24 | 30 | 34 | 64 | | | | 29 | 32 | 37 | 42 | 47 | |
| ٩ | T 16(cont.) | 5.31 | 9.04 | 14.70 | 18.06 | 21.84* | 26.10 | 30.72 | 35.90 | 41.51 | 47.53 | 54.12 | 61.22 | 68.89 | 77.10 | 86.22 | 96.46 | 105.53 | 109.58 | 112.56* | 113.09 | 112.54 | 113.66 | 115.49 | | A SET 17 | | 0.0428 | 0.97 | 1.27* | 1.95 | 2.67 | 3.47 | 4.31 | 5.20 | 6.11 | 7.04 | 8.00 | 8.61 | 8.99 | 10.01* | 11.09 | 12.25 | 4 - - |
| | DATA SE | 194.1 | 273 | 373 | 423 | 473 | 523 | 573 | 623 | 673 | 723 | 173 | 823 | 873 | 923 | 973 | 1023 | 1073 | 1123 | 1173 | 1183 | 1193 | 1223 | 1273 | | TAD | | 4.2 | 96 | 100 | 120 | 140 | 160 | 180 | 200 | 220 | 240 | 260 | 273 | 280 | 300 | 320 | 340 | |
| ٩ | 14(cont.)* | 71.0 | 8/.5 107.2 | | SET 15 | | 1.037* | 5.17 | 9.04 | 10.29* | 10.35* | 11.06 | 14.74* | 18.05* | 21.92* | 26.14* | 30.67* | 35.94* | 41.07 | 47.38 | 53.98* | 61.18* | 68.33 | 77.02 | 85.85 | 90.25 | 96.16 | 96.18* | 102.06 | 105.48* | 109.45* | 112.35* | 112.55* | 112.93 | 112.21* | 112.20 | 112.47 | 113.92 | 115.30 | | SET 16 | | 0.40 | |
| 4 | DATA SET | 873 | 5/6 5/01 | | DATA | | 73 | 189 | 273 | 296 | 297 | 310 | 373 | 422 | 473 | 524 | 573 | 625 | 671 | 723 | 774 | 824 | 871 | 924 | 973 | 995 | 1023 | 1023 | 1047 | 1074 | 1123 | 1173 | 1177 | 1186 | 1190 | 1611 | 1198 | 1237 | 1273 | | DATA | | 4 | |
| ٩ | SET 11 | 0.092 | 0.100 | 0.106 | 0.120 | 0.269 | 0.368 | 0.631 | 0.744 | 1.06 | 10.3 | | ET 12* | | 11.7 | 14.7 | 17.9 | 21.6 | 25.6 | | <u>ET 13</u> | | 11.9 | 14.9 | 18.2 | 21.8 | 25.8 | 30.3 | 41.0 | 53.3 | 67.9 | 85.2 | 104.2 | | ET 14* | | 15.8 | 18.7 | 22.0 | 25.9 | 30.0 | 34.6 | 45.0 | |
| ÷ | DATA | 4.2 | 20.8 | 26.1 | 32.5 | 54.4 | 61.2 | 74.2 | 79.1 | 90.2 | 293.0 | | DATA S | | 323 | 373 | 423 | 473 | 523 | | DATA S | | 323 | 373 | 423 | 473 | 523 | 573 | 673 | 517 | 873 | 973 | 1073 | | DATA S | | 323 | 373 | ^.23 | 473 | 523 | 573 | 673 | |
| ٩ | SET 3 | 0.925 | 974 8.974 | 10.33* | | *4 T2 | | 11.5 | 14.5 | 17.8 | | SET 5* | | 0.826 | 9.61 | | ET 6* | | 0.826 | 10.3 | | ET 7* | | 1.63 | 10.7 | | SET 8* | | 0.1437 | 0.929 | 9.11 | | SET 9* | | 1.060 | 1.917 | 9.95 | | SET 10 | | 0.0681 | 0.778 | 8.71 | |
| H | DATA | 17.78 | 273.3 | 298.8 | | DATA SI | | 323 | 373 | 423 | | DATA | | 8 | 273 | | DATA | I | 80 | 273 | | DATA S | | 80 | 273 | | DATA | | 21.2 | 83.2 | 273.2 | | DATA | | 21.2 | 83.2 | 273.2 | | DATA | | 21.2 | 83.2 | 273.2 | |
| | 11 | 1.46* | 1.46* | 1.46* | 1.46* | 1.46* | 1.46* | 1.46* | 1.46* | 1.46* | 1.46 | 1.46 | 1.47 | 1.47 | 1.44 | 1.44 | 1.44 | 1.47 | 1.48 | 1.51 | 1.51 | 1.51 | 1.50 | 1.51 | 1.51 | 1.59 | 1.61 | 1.68 | 1.80 | 1.84 | 1.89 | 1.92 | 2.02 | 2.08 | 2.14 | | ET 2 | | 1.09 | 5.78 | 9.06# | 14.73 | | |
| ٩ | S | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | וניט | | | | | | | |

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| TABLE |

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|----------|----------------|-------------|-----------|----------|-----------|---------|-----------------|--------|----------------|------------|--------------|
| DATA SET | 21(cont.) | DATA SET | 22(cont.) | DATA SET | 24(cont.) | DATA SI | 1 29* | DATA | SET 33 | DATA SET 3 | 5(cont.)* |
| 573.2 | 30.97 | 1273 | 115.8 | 973.2 | 87.44* | 293.2 | 9.72 | 293.2 | 10.00* | 983.4 | 86.5 200 |
| 623.2 | 36.18 | 1323 | 5./11 | 983.2 | 89. / 6× | | | 7.676 | -70'TT | 1.001 | 00.00 |
| 6/3.2 | 41.82 | 13/3 | 0.911 | 1001 | 92.0U | IC VIVO | -06 13 | 2.575 | 18 164 | 1.1001 | 0 10 |
| 7.621 | | (74T) | 4.U21 | 1.001 | | (EOC | 17 0 | 1.1.1 | 21 07 | 1.001 | 0.00 |
| 2.611 | 24.37 | 14/3 | 0.121 | 2 CTOT | 01 174 | 7.067 | | 2222 | 26.20 | 1014.1 | 97.9 |
| 7.C70 | 66 97# | C7CT | 1.021 | 2 LEUI | 98.50# | DATA | SET 31 | 573.2 | 30.89 | 1016.0 | 63.3 |
| 4.5.0 | 76.06 | DATA C | 26T 33# | 1063 2 | 00 67 | | | 623.2 | 35.97# | 1018.7 | 93.8 |
| 1.026 | 10.70 Df Df | VIVA | -7 130 | 1062 1 | 100 704 | 6 7 | 876 0 | 673 7 | A1 55 | 1010 8 | 0.40 |
| 1.5.1% | C0.C0 | Ę | 90 1 | 10001 | 100.001 | 1.4.4 | 0.258 | 2.0.0 | 07 64 | 1020 8 | 1.16 |
| 1003.2 | 11.12 | 5 | 00.1 | 7.001 | 101 264 | | 0.250 | 2.C2/ | 57 07 | 0.0201 | 1 |
| 1023.2 | 50.03 | 195 | 1.0 | 7.6/01 | -06.201 | 7.01 | 107.0 | 2.611 | | 0.1201 | |
| 1033.2 | 96.J/ | 0.67 | 56.6 | 1003.2 | tu.cut | 0.77 | C07.U | 7.040 | 20.72 28 61 | 1 3001 | 0.04 |
| 1036.2 | 14.66 | į | | 1093.2 | 101.00 | 0.42 | 007.0 | 7.6/0 | 10.00 | 1.0201 | 4.04 2 20 |
| 1043.2 | 100.84 | DATA | SET 24 | 1103.2 | 104.23 | 2.52 | 0/7.0 | 2.626 | 01.07 | 5-07NT | 0.04 |
| 1053.2 | 102.23 | | | 1113.2 | 104.03 | | 0.290 | 213.2 | -14.00 | 0.1201 | 4.04 |
| 1073.2 | 104.33* | 293.2 | 9.760* | 1123.2 | 105.40* | 36.6 | 0.300 | 998.2 | 90.95 | 1028.9 | |
| 1123.2 | 108.10* | 323.2 | 10.80 | 1133.2 | 105.92 | 53.1 | 0.439 | 1023.2 | 96.31* | 1031.6 | 96.9 |
| 1173.2 | 110.78 | 373.2 | 13.4 | 1143.2 | 106.41* | 64.4 | 0.593 | 1048.2 | 102.2 | 1032.8 | 97.2 |
| 1223.2 | 112.79 | 393.2 | 14.85 | 1153.2 | 106.85 | 73.6 | 0.689 | 1073.2 | 105.5* | 1034.2 | 97.6 |
| [273.2 | 114.49 | 413.2 | 16.39 | 1163.2 | 107.23* | 88.9 | 1.16 | 1098.2 | 197.8 | 1036.7 | 98.1 |
| 323.2 | 116.04 | 423.2 | 17.20 | 1173.2 | 107.55 | 105 | 1.81 | 1123.2 | 109.6* | 1038.1 | 98.6 |
| | | 433.2 | 18.01* | 1183.2 | 107.83* | 122 | 2.24 | 1173.2 | 112.3* | 1042.9 | 66.7 |
| DATA | SET 22 | 443.2 | 18.83* | 1193.2 | 108.07 | 122 | 2.45 | 1223.2 | 113.4 | 1045.9 | 100.5 |
| | | 453.2 | 19.66 | 1203.2 | 108.26 | 151 | 3.64 | 1273.2 | 115.0 | 1047.7 | 100.8 |
| 273 | 8.86# | 463.2 | 20.49* | 1213.2 | 108.43* | 186 | 5.10 | 1323.2 | 116.6 | 1050.8 | 101.2 |
| 293 | 9.81* | 473.2 | 21.31* | 1223.2 | 108.57 | 221 | 6.87 | 1373.2 | 118.2 | 1054.7 | 101.8 |
| 323 | 11.54* | 483.2 | 22.14 | 1233.2 | 108.70* | 282 | 10.1 | 1423.2 | 119.9 | 1061.7 | 102.7 |
| 373 | 14.53* | 493.2 | 22.98* | 1243.2 | 108.83 | 293.2 | 10.0* | 1473.2 | 122.1 | 1079.8 | 104.6 |
| 423 | 17.85# | 513.2 | 24.69* | | | | | 1523.2 | 124.1 | | |
| 473 | 21.55* | 523.2 | 25.58* | DATAS | ET 25* | DATI | V SET 32 | | | DATA | SET 30" |
| 523 | 25.65* | 573.2 | 30, 30# | | | | | VIVO | SET 34 | | |
| 573 | 30.2* | 623.2 | 35.50 | 293.2 | 9.69 | 0.452 | 0.339 | | | 974.6 | 85.4 |
| 623 | 35.3 | 673.2 | 41.19 | | | 0.643 | 0.346 | 90 | 1.30 | 984.2 | 88.0 |
| 673 | 40.95# | 723.2 | 47.39* | DATA S | ET 26# | 0.752 | 0.339* | 133 | 2.48 | 994.3 | 89.9 |
| 723 | 47.0 | 773.2 | 54.04 | • • | | 0.752 | 0.345 | 152 | 3.19 | 1002.4 | 91.5 |
| 573 | 53.7 | 823.2 | 61.25* | 293.2 | 9.72 | 0.788 | 0.350 | 172 | 4.06 | 1001.3 | 92.6 |
| 823 | ¥6°09 | 873.2 | 69.05 | | | 0.849 | 0.350 | 192 | 5.15 | 1012.3 | 93.6 |
| 873 | 68.7* | 883.2 | 70.68 | DATA S | ET 27* | 0.860 | 0.339 | 211 | 6.01 | 1018.9 | 95.0 |
| 923 | 76.85* | 893.2 | 72.34 | | | 0.860 | 0.349 | 231 | 6.95 | 1022.2 | 95.7 |
| 973 | 85.9* | 903.2 | 74.03* | 293.2 | 9.71 | 0.892 | 0.338 | 251 | 7.95 | 1025.6 | 96.6 |
| 1023 | 96.0# | 913.2 | 75.74 | | | 0.936 | 0.350 | 271 | 8.92 | 1028.0 | 97.3 |
| 1033 | 98.5* | 923.2 | 77.50* | DATA S | ET 28* | 0.944 | 0.353 | 291 | 10.00 | 1.1001 | 98.2 |
| 1073 | 104.9 | 933.2 | 79.32 | | | 0.952 | 0.338 | | | 1035.1 | 1.96 |
| 1123 | 108.7* | 943.2 | 81.21 | 293.2 | 9.70 | 1.001 | 0.333 | DATA S | ET 35* | 1039.2 | 100.1 |
| 1173 | 111.6 | 953.2 | 83.16* | | | 1.031 | 0.328 | | | 1044.9 | 101.4 |
| 1223 | *6.[1] | 963.2 | 85.26 | | | 1.102 | 0.326 | 917.6 | 83.5 | 1059.8 | 103.4 |
| | | ; ; ; | | | | | | | | 1078.8 | 105.3 |

* Not shown on either figure.

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|--|---------|------------------|--------------------|------|----------------------------|--------------|------------|----------|------------|--------------|-----------------|
| DATA S | ET 37* | DATA SET | 38(cont.) * | DATA | SET 40 | DATA SET | 43(cont.) | DATA SET | 47(cont.)* | DATA S | ET 49* |
| 1165.5 | 110.311 | 1183.6 1184.4 | 110.589 | 1103 | 105.8 | 253 273 | 7.9 8.8 | 16 18 | 0.390 | 53.8 76.1 | 1.820 2.341 |
| 1169.1 | 110.387 | 1186.2 | 110.624 | 1143 | 108.7 | 293 | 9.87 | 20 | 0.392 | | |
| 1171.9 | 110.437 | 1187.0 | 110.638 | 1163 | 109.8 | 323 | 11.6 | 25 | 0.399 | DATA S | ET 50 |
| 1172.9 | 110.463 | 1187.9 | 110.652 | 1183 | 110.7 | 373 | 14.7 | 0 2 | 0.410 | 1 75 | 1 220 |
| 1174.6 | 110.494 | 1190.6 | 109 011 | 1221 | 112.0 | 674 | 21.4 | 04 | 0.450 | 1.01 | 5.318 |
| 1176.2 | 110.520 | 4.1011 | 110.701 | 1243 | 112.7 | 523 | 26.0 | 53 | 0.484 | 234.0 | 7.168 |
| 1177.3 | 110.544 | 1192.5 | 110.715 | 1263 | 113.3 | 573 | 30.1 | 50 | 0.528 | 273 | 9,065* |
| 1178.2 | 110.567 | 1194.9 | 110.741 | 1283 | 114.0 | 623 | 35.0 | 55 | 0.585 | 273.85 | 9.115 |
| 1179.0 | 110.589 | | | | | 673 | 40.3 | 60 | 0.654 | 291.40 | 10.014 |
| 1179.8 | 110.604 | DATA S | ET 39 | DATA | SET 41 | 723 | 46.8 | 59 i | 0.737 | 333.40 | 12.359 |
| 1180.8 | 110.624 | | - | | | 773 | 53.3 | 20 | 0.832 | 371.25 | 14.631 |
| 5 L811 | 040-011 | 2.67 | C | (()) | 121.111 121 59 4 | 04.2 87.2 | 1.00 | | 0.7.0 | 0.014 | 00 V 10 |
| 1183.5 | 110.680 | 173.2 | 6.3 | 1593 | 121.92 | 923 | 76.0 | 22 22 | 1.188 | | |
| 1185.3 | 110.697 | 223.2 | 6.6 | 1613 | 122.34 | 973 | 84.8 | 6 | 1.327 | DATA SI | ET 51* |
| 1186.1 | 110.696 | 273.2 | 0.6 | 1633 | 122.76 | 1023 | 94.2 | 95 | 1.476 | | |
| 1187.0 | 110.696 | 323.2 | 11.8 | 1653 | 123.17 | 1073 | 102.1 | 100 | 1.632 | 51.0 | 0.660 |
| 1188.0 | 110.689 | 373.2 | 14.4 | 1659 | 123.31 | 1123 | 106.3 | 110 | 1.969 | 54.0 | 0.725 |
| 1188.9 | 110.689 | 423.2 | 17.9 | 1663 | 123.49 | 1173 | 109.0 | 120 | 2.330 | 76.1 | 1.220 |
| 1192.3 | 110.687 | 473.2 | 21.5 | 1673 | 123.74 | 1223 | 111.1 | 130 | 2.707 | 273.2 | 9.065 |
| 1193.2 | 110.698 | 523.2 | 25.5 | 1693 | 124.22 | 1273 | 113.1 | 140 | 3.10 | | |
| 1194.0 | 110.709 | 573.2 | 30.6 | 1713 | 124.73 | | | 150 | 3.50 | DATAS | ET 52* |
| 1195.0 | 110.719 | 623.2 | 35.8 | | | DATA | SET 44* | 160 | 3.91 | | |
| 1197.6 | 110.745 | 673.2 | 40.9 | DATA | SET 42* | | | 170 | 4.32 | 50.5 | 0.644 |
| | | 723.2 | 46.4 | | | 291 | 11.96 | 180 | 4.75 | 50.8 | 0.649 |
| DATA S | ET 38* | 773.2 | 52.8 | 83 | 1.22 | 373 | 16.81 | 190 | 5.18 | 76.1 | 1.220 |
| | | 823.2 | 60.2 | 203 | 5.60 | | | 200 | 5.61 | | |
| 1163.9 | 110.485 | 873.2 | 67.2 | 223 | 6.50 | DATA | SET 45* | 220 | 6.52 | DATA | SET 53 |
| 1165.5 | 110.519 | 923.2 | 75.6 | 248 | 7.65 | | | 240 | 7.44 | | |
| 1167.4 | 110.553 | 973.2 | 84.2 | 273 | 8.96 | 273 | 9.64 | 260 | 8.42 | 76 | 0.608 |
| 1168.3 | 110.578 | 1023.2 | 93.8 | 293 | 10.0 | 373 | 15.09 | 280 | 9.43 | 16 | 1.067* |
| 1169.2 | 110.595 | 1073.2 | 103.3 | 313 | 11.3 | | | | | 173 | 4.010* |
| 11/1.8 | 110.603 | 1123.2 | 108.1 | 333 | 12.5 | DATA | SET 46* | DATA S | ET 48* | 274 | 8.659* 0.555 |
| 2.1112 | 047.011 | 7.0.11 | 4.011 | | 13.0 | | : | | | 00.142 | |
| 11/2./ | 110.562 | 1223.2 | 112.5 | | | 312.07 | 11.99 | 76.1 | 2.341 | 369.6 | 11.11 |
| | 700.011 | 7.0121 | 0.411 | NAIA | 261 43 | | | 191.3 | 100.0 | | |
| 11/4.0 | 110.522 | 1323.2 | 115.3 | č | • | DATA | SET 47* | 229.3 | 8.364 | DATA SE | |
| 11/2.4 | 104-011 | 1.1.1.1 | 0.011 | 5 | 7.7 | | | 2/3.0 | 210.01 | | • |
| 6-0/11 | 0/6-011 | 1423.2 | 11/.9 | | 1.7 | 0 | 0.38/ | 274.55 | 10.592 | 505 | 17.5 |
| 11// · · · · · · · · · · · · · · · · · · | 110.491 | 1473.2 | 119.2 | 133 | 2.4 | ~ | 0.387 | 291.65 | 11.498 | 367 | 20.0 |
| 1178.Z | 110.514 | 1523.2 | 120.6 | 153 | 3.1 | 80 | 0.385 | 325.25 | 13.399 | 413 | 23.1 |
| 1180.1 | 110.531 | 1573.2 | 121.6 | 173 | 4.0 | 6 | 0.385 | 363.7 | 15.729 | 460 | 26.3 |
| 1180.9 | 110.546 | 1623.2 | 122.8 | 193 | 5.0 | 10 | 0.385 | 412.0 | 18.902 | 527 | 32.0 |
| 1151.8 | 110.566 | 1673.2 | 124.0 | 213 | 5.9 | 12 | 0.387 | 470.5 | 23.251 | 575 | 36.4 |
| | | 1715.2 | 125.2 | 233 | 6.9 | 14 | 0.389 | | | 648 | 43.6 |

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* Not shown on either figure.

| F | ٩ | F | ٩ | 4 | ٩ | F | ٩ | F | ٩ | H | a |
|----------|-----------|-------------------|----------------|----------|------------|----------|------------|----------|-----------|-------------|-----------|
| DATA SET | 54(cont.) | DATA SET | 55(cont.)* | DATA SET | 56(cont.)* | DATA SET | 58(cont.)# | DATA SET | 63(cont.) | DATA SET | 66(cont.) |
| 663 | 45.3* | 784 | 58.1 | 1042.2 | 103.89 | 1182.9 | 113.16 | 1580 | 121.92 | 573 | 32.781 |
| 735 | 53.1 | 567 | 59.8 | 1043.2 | 104.06 | 1185.7 | 112.69 | 1600 | 122.35 | 598 | 35.235 |
| 908 | 61.6 | 831 | 65.1 | 1044.3 | 104.23 | 1186.7 | 112.74 | 1620 | 122.76 | 623 | 37.877 |
| 006 | 76.4 | 836 | 66.3 | 1044.8 | 104.32 | | | 1640 | 123.17 | 648 | 40.583 |
| 933 | 80.7 | 885 | 74.0 | 1046.8 | 104.60 | DATA | SET 59* | 1660 | 123.56 | 673 | 43.345 |
| 973 | 90.2 | 894 | 75.2 | 1047.9 | 104.78 | 1 | | | | | |
| 982 | 92.1 | 901 | 76.7 | 1049.1 | 104.97 | 4.2 | 2.58 | DATA | SET 64 | DATA S | ET 67* |
| 1015 | 98.7 | 918 | 79.8 | 1052.6 | 105.45 | | | | | | |
| 6101 | 100.04 | 156 | 9.28 | 1054.9 | 105.78 | DATA | SET 60 | 1700 | 125.80 | 293 | 9.7 |
| 1024 | 100.74 | 975 | 0 | 1057 6 | | | | 1720 | 126.13 | | |
| 1033 | | 010 | | 1 VEN 1 | 106 33 | 202 | 13 44 | 1740 | 136 6. | 1111 | |
| 5501 | 102.2 | 616 | C.1% | 1.401 | 100.33 | 667 | | 04/1 | (4.02T | VIV | 261 061 |
| 1045 | 105.8* | 982 | 91.8 | 1059.9 | 106.32 | 10/3 | 80 | 1/60 | 170.11 | | |
| 1062 | 106.6 | 987 | 92.8 | 1062.2 | 106.69 | 1123 | 112 | 1780 | 127.07 | 66 | 2.635 |
| 1083 | 110.3* | 1000 | 94.6 | 1064.7 | 107.01 | 1173 | 114 | 1800 | 127.38 | | |
| 1090 | 111.3* | 1050 | 106.8 | 1065.9 | 107.09 | 1223 | 114 | | | DATA | SET 694 |
| 1124 | 112.9 | 1054 | 107.5 | 1068.4 | 107.39 | 1279 | 121 | DATA | SET 65 | | |
| 1124 | 113.8* | 1061 | 108.1 | | | 1378 | 125 | | | 66 | 1.647 |
| 1135 | 114.5* | 1067 | 108.9 | DATA S | ET 57* | 1480 | 124 | 1700 | 124.87 | | |
| 1161 | 115.1 | 1076 | 110.0 | | | 1578 | 135 | 1720 | 125.22 | DATA | SET 70# |
| 1163 | 115.8* | 1085 | 110.6 | 1151.9 | 113.48 | 1698 | 135 | 1740 | 125.54 | | |
| 1174 | 117.0 | 1100 | 111.3 | 1156.2 | 113.71 | | | 1760 | 125.83 | 93 | 2.25 |
| | | 1123 | 113.3 | 1162.8 | 114.07 | DATA | SET 61* | 1780 | 126.08 | | |
| DATA S | ET 55* | 1141 | 114.6 | 1165.8 | 114.23 | | | 1800 | 126.30 | DATA | SET 71* |
| | | 1150 | 115.0 | 1173.7 | 114.63 | 313 | 11.65 | | | | |
| 8 | 10.8 | 1213 | 115.0 | 1175.5 | 114.70 | 323 | 12.21 | DATA | SET 66 | 11 | 0.7786 |
| 311 | 11.5 | 1229 | 115.7 | 1177.5 | 114.79 | 333 | 12.77 | | 1 | | |
| 347 | 13.4 | 1247 | 116.2 | 1180.8 | 114.13 | 343 | 13.33 | 84 | 2.653 | DATA | SET 72* |
| 358 | 14.1 | 1291 | 117.9 | 1182.9 | 113.52 | • | | 86 | 3.091 | | |
| 373 | 15.1 | | | 1185.2 | 112.97 | DATA | SET 62 | 123 | 3.988 | 11 | 0.7686 |
| 986 | 16.3 | DATA S | SET 56* | 1187.7 | 112.77 | | | 148 | 4.962 | | |
| 414 | 19.6 | | | 1189.5 | 112.84 | 1500 | 121.12 | 173 | 5.979 | DATA | SFT 738 |
| 451 | 20.8 | 1017.6 | 97.78 | 1190.6 | 112.90 | 1520 | 121.59 | 198 | 6.937 | | |
| 478 | 27 0 | 1018 0 | OR UN | 1194 6 | 112 05 | 1540 | 122 05 | 222 | 6 1 V 7 | 7.6 | 0176 0 |
| 5 | 0.55 | 1010 0 | 0.8 24 | 1197 3 | 112 16 | 1560 | 122 51 | 248 | 348 | | |
| | 8.56 | 1077 8 | 08 83 | | 01.011 | 1580 | 122 05 | 575 | 10,601 | DATA | CET 744 |
| | | 1011 4 | 20.00 | 14TA 0 | 277 CQ4 | 1400 | 122 20 | 900 | 100.01 | | 10 10 |
| 3 | | 4.0201 4.021 6 | 40. V4 | NUN | -OC 130 | 0001 | 10.01 | 666 | (0).31 | • | |
| | - TC | 1010 E | 00.00 00 66 | 0 1311 | | 0701 | 70.021 | C7C | 12.204 | 0.1 1 | |
| | | C.C201 | 00.64 | 0.1011 | 113./3 | 1040 | 124.2J | | 770°CT | 0. 7 | 0.13/ |
| | 0.55 | 1028.6 | 100.42 | 1101./ | 114.30 | 1660 | 124.60 | 575 | 16.630 | 4.1 | 0.137 |
| 628 | | 1029.5 | 100.56 | 1167.9 | 114.62 | | | 398 | 18.235 | 5.3 | 0.138 |
| 636 | 38.8 | 1031.1 | 100.99 | 1171.5 | 114.82 | DATA | SET 63 | 423 | 20.012 | 6.2 | 0.138 |
| 644 | 0.04 | 1034.0 | 101.76 | 1174.1 | 114.92 | | | 448 | 21.504 | 7.3 | 0.138 |
| 675 | 43.6 | 1036.0 | 102.27 | 1175.7 | 114.74 | 1500 | 120.13 | 473 | 23.928 | 8.5 | 0.146 |
| 687 | 45.2 | 1038.7 | 103.13 | 1177.8 | 114.42 | 1520 | 120.59 | 498 | 26.000 | 10.1 | 0.148 |
| 725 | 50.1 | 1039.5 | 103.26 | 1180.4 | 113.78 | 1540 | 121.04 | 523 | 28.196 | 11.8 | 0.148 |
| 752 | 54.0 | 1041.0 | 103.58 | 1181.7 | 113.47 | 1560 | 121.49 | 548 | 30.357 | 14.0 | 0.148 |

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* Not shown on either figure.

82.3 85.8# 85.8# 92.4# 98.4# 98.4# 98.4# 100.8 100.8 100.8 110.8 1112.2 1113.6 115.7 91(cont.) 122.8 128.8 126.1 116.5 117.2 122.6 129.9* 14.4 16.1 20.3 20.3 26.8 33.6 45.0 65.1 85.0 85.0 140.00 80.7 81.6 82.4 ¢ DATA SET 93 SET 94 **SET 92** SET 95 DATA SET DATA DATA DATA 927 949 964 980 980 1002 1003 1013 1037 1037 1037 1036 1107 11060 11076 11107 11125 1808 1448 1677 1755 1755 1814 1814 2046 2046 928 344 405 457 457 598 598 694 842 944 944 F 86 (cont.) 10.8* 15.5 221.6 221.6 221.6 22.1 6 55.9 8 33.2 8 55.9 8 55.9 4 8 55.1 4 75.0 77.0 10.75 8.93 a 10.87 12.5 DATA SET 87* DATA SET 88* DATA SET 89* DATA SET 90* DATA SET 91 DATA SET 98.0 105.5 111.1 115.2 115.2 124.1 134.3 178.4 199.3 178.4 199.3 251.6 251.6 2531.6 253 22.5 293 H 293 293 293 0.0953 0.0957 0.0957 0.0957 0.0959 0.0959 0.0969 0.09979 0.09979 0.09979 0.09979 0.1015 060.0 0.084 0.057 0.24 9.60 0.57 **SET 86** 4.1 6.9 10.7 DATA SET 84 DATA SET 85* DATA SET 83* 0.8 SET 81* SET 82* đ **SET 80** DATA DATA DATA DATA 4.2 293 4.2 293 4.2 293 4.2 293 5.5 8.8 8.8 8.8 8.8 8.8 111.9 6.6 111.9 6.111.9 113.0 113.0 113.0 4.2 200 EFT % 273 H 79(cont.) 0.88 88.99 98.99 98.99 98.99 9. .65 9.77 10.02 10.12 10.41 9.31 ٩ DATA SET H 111.69 111.97 111.97 111.92 111.92 111.92 111.32 111.43 111.43 111.61 111.61 111.61 111.85 111.85 0.25 0.26 0.82 9.1* 0.63 0.78 0.84 21.4 41.0 68.2 106.4 SET 78* SET 77 194 SET 764 đ SET 4.00 20.2 77.2 273 473 673 673 873 873 VIV DATA DATA 1167.4 1169.5 1173.0 1174.6 1175.9 1178.4 1178.4 1180.6 1184.8 1184.8 1184.8 1184.3 1187.9 1187.9 1189.7 76.7 85.5 91.6 91.6 102.6 112.7 112.7 113.0 1139.0 1139.0 1139.0 1122.2 1139.0 1139.0 1122.2 1122.2 1139.0 1122.2 1123.2 1122.2 1123.2 DATA 77 82.0 84.6 1160 H Not shown on either figure. DATA SET 74(cont.)* 0.155 0.155 0.155 0.156 0.188 0.188 0.188 0.228 0.327 0.503 0.734 111.75* 111.75* 111.86* 111.86* 112.03* 112.29* 112.29* 112.98* 112.98* 112.98* 112.98* 112.98* 112.98* 111.84* 112.02* 111.84* 112.12 107.16 108.03 109.41 11.64 110.62 ٩ DATA SET 75 16.8 20.0 227.5 286.3 56.9 55.9 56.6 0 1088 1123.3 1124.1 1154.5 1156.5 1156.5 1166.6 1156.5 1166.6 1175.3 1176.5 1175.5 1175.5 1175.5 1175.6 1175.5 1175.6 1175.6 1175.6 1175.6 1175.6 1175.6 1175.6 1175.6 1175.6 1175.7 1186.1 1186.1 1196.1 1196.1 1196.1 ۲

| (continued) |
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| e. |
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| RESISTIVITY |
| ELECTRICAL |
| THE |
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| DATA |
| EXPERIMENTAL |
| TABLE 9. |

| - | ٩ | F | Q | H | ٩ | ų | ٩ | н | ٩ | Ŧ | ٩ |
|--------------|---------------|----------|------------|--------|--------------------|-----------|------------|----------|-------------|------------|-------------|
| DATA SET | 95(cont.) | DATA SET | 96(cont.)* | DATA | SET 98* | DA. A SET | 99(cont.)* | DATA SET | .01(cont.)* | DATA SET 1 | .03(cont.)* |
| 942 | 83.2 | 1040 | 103.8 | 1174.7 | 117.711 | 1175.6 | 117.682 | 483.5 | 27.68 | 959.5 | 81.30 |
| 647 | 84.1 | 1046 | 104.8 | 1175.6 | 117.735 | 1176.5 | 117.663 | 486 | 27.88 | 1009 | 00.68 |
| 952 | 85.0 ex e | 1155 | 116 8 | 2.0/11 | 11/.//I | 1178 3 | 117 632 | C.12C | 41.30 | 1169 | 110 60 |
| | 86. N | 158 | 115.0 | 1178.3 | 117.843 | 1179.2 | 117.651 | 803.5 | 61.55 | C-06TT | 00.011 |
| 3 <u>6</u> 2 | 87.6 | 1164 | 115.2 | 1179.2 | 117.869 | 1180.0 | 117.655 | 808.5 | 61.55 | DATA SI | ET 104* |
| 970 | 88.6 | 1168 | 114.8 | 1180.0 | 117.920 | 1181.0 | 117.655 | 916 | 77.40 | | |
| 975 | 89.5 | 1172 | 114.9 | 1181.0 | 117.963 | 1181.9 | 117.665 | 647 | 83.40 | 273 | 10.50 |
| 086 | 90.3 | 1176 | 115.0 | 1181.9 | 118.002 | 1182.8 | 117.690 | 1025 | 96.70 | 284.1 | 11.10 |
| 984 | 91.4 | 1181 | 115.1 | 1182.8 | 118.036 | 1183.6 | 117.713 | 1036 | 99.70 | 325 | 13.21 |
| 686 | 92.3 | 1186 | 115.1 | 1183.6 | 118.061 | 1184.5 | 117.741 | | | 374 | 11.41 |
| 666 | 93.2 | 1190 | 115.2 | 1184.5 | 118.077 | 1185.5 | 117.773 | DATA S | ET 102* | 401.5 | 18.44 |
| 866 | 94.3 | 1194 | 115.3 | 1185.5 | 118.098 | 1186.4 | 117.800 | | | 463.5 | 23.28 |
| 1008 | 96.2 | 1198 | 115.5 | 1186.4 | 118.112 | | | 273 | 12.500 | 525.5 | 28.66 |
| 1012 | 97.2 | 1203 | 115.6 | 1187.2 | 118.105 | DATA S | ET 100* | 289 | 13.58 | 587.5 | 34.92 |
| 1016 | 98.3 | 1207 | 115.8 | 1188.2 | 118.082 | | | 291 | 13.82 | 631.5 | 39.80 |
| 1026 | 100.5 | 1211 | 115.9 | 1189.0 | 118.070 | 325 | 12.43 | 444.5 | 23.48 | 686.5 | 45.90 |
| 1031 | 101.6 | 1217 | 116.1 | 1189.6 | 118.056 | 375 | 14.88 | 474.5 | 25.13 | 739.5 | 52.70 |
| 1036 | 102.7 | 1221 | 116.2 | 1190.7 | 118.045 | 425 | 18.33 | 594 | 36.28 | 790 | 59.25 |
| 1050 | 105.8 | | | 1191.5 | 118.047 | 475 | 22.78 | 600 | 36.76 | 828 | 64.40 |
| 1054 | 106.4 | DATA | SET 97* | 1192.4 | 118.052 | 525 | 26.23 | 603.5 | 37.00 | 834 | 65.40 |
| 1059 | 106.9 | | | 1193.2 | 118.092 | 575 | 30.68 | 777.5 | 55.50 | 878.5 | 71.95 |
| 1063 | 107.6 | 1003 | 95.4 | 1194.0 | 118.108 | 625 | 36.13 | 179 | 55.70 | 922 | 78.90 |
| 1068 | 108.1 | 1021 | 9.6 | 1194.8 | 118.125 | 675 | 41.58 | 893 | 71.35 | 952 | 83.75 |
| 1073 | 108.6 | 1040 | 104.4 | 1195.5 | 118.142 | 725 | 48.03 | 926 | 75.60 | 987.5 | 89.30 |
| 1077 | 109.0 | 1045 | 105.4 | 1196.4 | 118.158 | 115 | 54.48 | 979 | 84.40 | 1012.5 | 94.20 |
| 1082 | 109.5 | 1001 | 110.5 | 1197.0 | 118.198 | 825 | 61.93 | 997.5 | 86.60 | 1024.0 | 96.20 |
| 1085 | 110.0 | 1155 | 114.2 | 1197.7 | 118.230 | 875 | 69.38 | 1034 | 92.60 | 1037.0 | 98.60 |
| 1095 | 110.6 | 1159 | 114.4 | 1198.5 | 118.258 | 925 | 77.83 | 1059 | 97.20 | 1095 | 100.00 |
| 1100 | 111.0 | 1164 | 114.7 | | | 975 | 86.28 | 1078 | 101.10 | 1059.5 | 103.00 |
| 1011 | 111.3 | 1167 | 115.4 | DATA | SET 99* | 1025 | 94.73 | 1081.5 | 101.10 | 1073 | 106.10 |
| 1109 | 111.6 | 7/17 | 115.4 | | | 1075 | 102.18 | 1154 | 110.00 | 1099 | 108.30 |
| 1114 | 111.8 | //11 | 115.6 | 1163 | 117.263 | 1125 | 107.63 | 1143 | 109.40 | | |
| 0111 | 112 5 | 1011 | 1.011 | 6 7711 | 117 201 | 2/11 | 90.111 | 1273 5 | 07.611 | DAIA S | CO1 13 |
| (711 | C . 711 | 1100 | 0.011 | 0.4011 | 100/111 | 2771 | CC.CI1 | C.C221 | 114.20 | | 10 60 |
| 1111 | 1.511 | 1195 | 0.011 | 1.0011 | 674.111 874.111 | 5/21 | 116 67 | 5 0001 | 00.011 | 106 | 0C-0T |
| 1127 | | 1108 | 0 911 | 1167 5 | 117 540 | 1175 | 117 88 | 1222 | 115 80 | 135 | 15.20 |
| 1711 | 111.5 | 1203 | 116.2 | 1168.5 | 009 211 | 1675 | 120.33 | 1111 | 00.011 | 114 | 10 01 |
| 1146 | 113.9 | 1207 | 116.4 | 1169.4 | 117.661 | | | DATA S | ET 103* | 469.5 | 24.02 |
| 1150 | 114.2 | 1211 | 116.4 | 1170.1 | 117.704 | DATA S | ET 101* | | | 525.5 | 29.00 |
| | | 1216 | 116.7 | 1171.1 | 117.721 | | | 289.8 | 13.510 | 568.5 | 34.02 |
| DATA S | 5ET 96* | 1220 | 116.8 | 1172.0 | 117.718 | 273 | 13.600 | 293 | 13.94 | 634 | 40.58 |
| | Ì, | | | 1173.0 | 117.712 | 291 | 14.61 | 903 | 72.90 | 629 | 43.40 |
| 1004 | 94.9 | | | 1173.9 | 117.689 | 400 | 22.15 | 905.5 | 72.40 | 619 | 45.72 |
| 1022 | 99.1 | | | 1174.7 | 117.690 | 462 | 26.30 | 954 | 79.75 | 727.5 | 51.77 |
| | | | | | | | | | | | |
| * Not sh | own on either | figure. | | | | | | | | | |

DATA SET 113(cont.) 114.8* 115.8 115.8 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 117.2* 112.2* 122.2* 122.2* 122.2* 122.3* 122.3* 122.3* 122.3* 123.5* 123. ٩ 114 SET DATA 1417 1445 14497 14497 14497 1544 15544 15544 1556 16568 16568 16686 16686 1697 1718 1397 ۲ 112.6 113.5***** 114.3***** 113(cont. DATA SET м 9.35 10.95 11.92* 15.49 15.49 31.93 37.07 56.79 56.30 56.30 79.40 79.40 71.05 79.40 79.40 71.05 111.0 105.1 DATA SET 110(cont.) 79.55 89.70 103.3 113.2 118.6 118.6 120.4 121.2 122.0 10.0 11.5 13.1 14.1 15.7 17.2***** 19.0 ٩ SET 111 SET 113 138 112 SET DATA DATA DATA 1923 304 327 327 327 327 53 55 51 51 ٠ 9.57 112.06 115.39 19.09 23.67 23.67 28.72 34.15 44.09 54.88 62.35 70.30 11.64 15.53 22.00 22.00 25.00 25.00 55.50 55.50 67.55 55.50 67.55 55.50 67.55 59.55 67.55 100.8 85.20 85.20 810.8 8.53 19.91 108 (cont. 91.6 97.5 97.5 100.2 101.5 103.6 106.0 111.1 112.8 113.6 SET 109* SET 110 a DATA DATA SET DATA 1044 1053 1053 1073 1073 1123 273 2293 373 373 373 473 473 573 673 673 673 773 773 8823 873 873 273 323 373 473 473 673 673 673 7723 823 823 823 973 1023 1073 1073 1173 1173 1223 1223 23 H 107 (cont.) 2.07 5.81 15.5 15.5 15.5 30.6 41.6 53.9 53.9 53.9 53.9 53.9 53.9 53.9 ٩ 108 SET SET DATA DATA F 78 178 273 273 370 570 681 783 864 864 982 033 0.080 57.85 64.85 76.05 77.00 77.00 89.20 89.20 89.20 99.65 99.65 99.65 100.90 100.90 100.90 100.90 100.90 100.90 100.90 100.50 111.40 11.40 11.40 11.40 11.40 11.40 11.40 11.40 11.40 11.40 11.40 11.40 11. DATA SET 105(cont 0.23 SET 106 DATA SET 107 a DATA 776.5 826.5 826.5 931.5 931.5 931.5 931.5 931.5 930.5 931.5 932.5 1034.5 1114.5 4.2 ~ • •

* Not shown on either figure.

| H | ٩ | F | م | Т | ٩ | ÷ | p - p | H | d | T | ٩ |
|------------------|--------------------|----------|--------------------|----------|-------------------|----------------|------------|------------|----------|--------------|------------------|
| DATA SE | <u>1115</u> | DATA SET | 116(cont.) | DATA SET | <u>116(cont.)</u> | DATA | SET 119* | DATA S | ET 124* | DATA SET | 34 (cont.) |
| 6/11 | 129.9 | 1023.4 | 98.589* | 1054.4 | 106.326* | 2.438 | 0.00009942 | 11 | 0.700 | 25.4 | 0.3583 |
| 1797 | 131.0 | 1024.7 | 98.981* Go Ange | 1056 3 | 106.433* | 3.062 | 0.0001421 | 867 | 9.60 | 20.2 | 0.3553# |
| 1832 | 140.0 | 1027.1 | 100.015* | 1057.4 | 106.611* | 5.000 | 0.0003850 | DATA | SET 125* | 30.9 | 0.37608 |
| 1842 | 138.4 | 1027.2 | 99.694* | 1059.0 | 106.825* | 7.674 | 0.0007771 | | | 33.6 | 0.3802 |
| 1847 | 139.2 | 1028.5 | 100.122* | 1059.6 | 106.896* | 10.00 | 0.001326 | 4.2 | 0.236 | 37.2 | 0.4146 |
| 1852 | 141.3 | 1029.6 | 100.443* | 1060.5 | 106.896 | 11.32 | 0.001720 | | | 40.7 | 0.4484 |
| 1862 | 139.3 | 1030.4 | 100.764* | 1061.2 | 106.932* | 15.92 | 0.004041 | NTA | SET 126* | 40.8 51 5 | 0.497/ |
| 18/2 | 140.8 | 1031.0 | 100.9/8# | 1.2001 | 107 003# | 18.84 20 31 | 0.020088 | 4 2 | 151.0 | 0.05 | 1200.0 |
| 1892 | 142.1 | 1032.6 | 100.512* | 1064.0 | 107.039* | 38,90 | 0.04770 | | | 64.6 | 0.7590 |
| 1898 | 141.1 | 1033.4 | 101.833* | 1065.2 | 107.075* | 49.77 | 0.1184 | DATA | SET 127* | 70.6 | 0.8995 |
| i | | 1034.0 | 102.012# | 1066.0 | 107.146* | 62.66 | 0.2776 | | | 71.9 | U.93/4= |
| DATA | SET 110 | 1035.0 | 102.368* | 1068.0 | 107.324* | DATA | SET 120* | | ccc.n | 7.61 | 1.120 |
| 8.666 | 91.101 | 1035.7 | 102.618* | 1069.1 | 107.396* | | | DATA | SET 128* | 82.2 | 1.218 |
| 995.4 | 91.422* | 1036.0 | 102.760* | 1069.9 | 107.431* | 2.366 | 0.0001022 | | | 86.3 | 1.359* |
| 996.4 | 91.636* | 1036.7 | 102.974* | 1070.3 | 107.503* | 2.951 | 0.0001554 | 4.2 | 0.726 | 90.6 | 1.509* |
| 996.7 | 91.707# | 1037.4 | 103.295* | 1071.4 | 107.574* | 4.130 | 0.0002732 | | | 95.1 | 1.690 |
| 997.7 | 91.885* | 1038.2 | 103.519* | 1072.3 | 107.610* | 4.989 | 0.0004004 | DATA | SET 129* | 102.1 | 1.920* |
| 998.2 | 91.921# | 1038.8 | 103.68/* | 1073.0 | 107.645* | 7.379 | 0.0008138 | | | 6.801 | 2.173* |
| 998.8 | 92.171# 07 817 | 1039.2 | 103.830# | 10/3.6 | 107.7524 | 11.02 | 0.001/00 | 4.2 | 0.36/ | C./11 | 7 0154 2 0154 |
| 1001 | 92.014 97 167# | 1040.0 | 187 | 1076.0 | 107.824# | 10.61 | 0.01001 | DATA | SET 130* | 137.4 | 7.76 |
| 1003.5 | 93.419* | 1040.3 | 104.294* | 1077.0 | 107.895* | 39.45 | 0.04041 | | AC* 130 | 150.0 | 3.85 |
| 1004.4 | 93.561* | 1040.8 | 104.508* | 1077.9 | 107.930* | 47.64 | 0.07789 | 4.2 | 0.641 | 166.3 | 4.66* |
| 1005.5 | 92.527* | 1041.3 | 104.650* | 1078.7 | 108.037* | 77.62 | 0.5514 | | | 175.4 | 5.067 |
| 1005.7 | 93.704 | 1041.9 | 114.828* | 1079.7 | 108.144* | | | DATA | SET 131* | 181.6 | 5.548* |
| 1006.2 | 93.918* | 1042.4 | 104.864* | 1080.4 | 108.251 | | | • | | 195.9 | 6.321 |
| 1007.1 | 94.239* 96.417* | 1042.8 | 105.007* | 1081.4 | 108.323* | н | ٩ | 4.2 | 0.924 | 218.3 | 7.336 |
| 1008.8 | 94.666* | 1043.7 | 105.114* | 1083.2 | 108.430* | | | DATA | SET 132* | 252.3 | 9.253 |
| 1010.4 | 94.916* | 1044.3 | 105.185* | 1084.3 | 108.501* | DATA SET | 121* | | | 259.4 | 9.482 |
| 1011.4 | 95,130* | 1045.2 | 105.399* | 1085.5 | 108.572* | 1573 | 111 8 | 4.2 | 1.086 | 276.1 | 10.136 |
| 1012.2 | 95.415* | 1045.7 | 105.542* | 1086.5 | 108.608* | 1873 | 136.4 | | | 300.0 | 10.33 |
| 1015.0 | 90.000 M | 1046.0 | 105.615F | T022.1 | 106.71 | | | VIVO | SET 133* | DATA CE | . 136 |
| 1015.7 | 96.271* | 1047.3 | 105.791* | DATA SET | 117 | DATA SE | T 122* | 4.2 | 1.298 | TO VIVO | CT |
| 1016.5 | 96.521* | 1048.2 | 105.862* | | | ; | 600 | | | 373 | 16.1 |
| 1017.1 | 96.628* | 1049.2 | 105.969* | 1873 | 110 | 64C | 0.00 | DATA | SET 134 | 473 | 22.8 |
| 1017.8 | 96.877* | 1049.8 | 106.005* | | | 710 | 00.0 | | | 573 | 30.8 |
| 1019.3 | 97.412* | 1050.4 | 106.041 | DATA SET | r 118 | DATA SE | T 123* | 4.2 | 0.3300 | 673 | 42.6 |
| 20201 201 | 97.697 | 0.1201 | 106.112# | | | | | 16.3 | 0.3417 | | 4.00 |
| 1.1201 1.1701 | 9/.911× GR 768# | 1057 0 | 106 1834 | 609T | 134 | 11 | 0.620 | 1.01 | 2455 U | | |
| 1022.4 | 98. 339* | 1053.7 | 106.290* | | | 298 | 9.80 | 22.3 | 0.3522 | | |
| | | | | | | | | | | | |

* Not shown on either figure.

EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF IRON Fe (continued)

TABLE 9.

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TABLE

DATA SET 158(cont.)* 97.684 97.843 98.003 98.003 98.625 99.531 99.531 99.531 99.531 99.531 100.77 101.56 100.77 101.58 100.77 101.58 105.39 105.32 105.32 105.32 105.32 105.32 105.32 105.32 8.57 9.61 14.296 21.5 30.3 53.4 53.4 45,434 60.230 61.241 880.392 880.392 92.762 94.828 94.828 94.828 95.539 95.539 95.539 95.233 95.233 97.086 97.086 97.3457 97.3457 97.3457 97.3457 97. 159 ¢ SET 719.5 8370.6 8370.6 837.8 955.9 955.9 955.9 955.9 1012.25 1012.25 1023.4 1023.4 1033.4 1033.4 1033.5 1033.5 1033.5 1045.5 1045.5 1045.5 1045.5 1045.5 1045.5 1045.5 1045.5 1055.6 1005.6 10055.6 1005.6 1005.6 1005.6 1005. DATA ٣ 0.006210 0.006211 0.006212 0.006215 0.006217 0.006221 0.006225 0.006225 0.6696 0.6696 0.6712 0.6967 1.982 2.391 2.391 15.98 0.8806 0.8806 0.8806 0.9348 2.755 22.58 DATA SET 153(cont.) 1.288 1.520 11.04 SET 156* SET 155* 0.180 1.046 8.572 8.572 14.442 29.129 30.269 SET 154# 8.73 156A 1574 ٩ SET SET DATA DATA DATA 1.38 3.71 4.21 20.40 81.73 90.46 273.16 0.302 0.400 0.500 0.500 0.600 0.700 0.805 0.908 1.004 77.79 85.19 273.16 1.38 3.71 4.21 20.40 81.73 273.16 DATA DATA н 273 0.1631 0.1641 0.1674 0.1772 0.8935 10.87 0.0556 0.0565 0.0692 0.6751 9.11 0.0723 0.0723 0.0795 0.6751 8.93 0.1604 0.1614 0.1781 0.8610 9.84 0.6166 0.6166 0.6176 0.6425 1.421 1.66 9.59 0.5123 0.5167 0.5235 SET 150* SET 151* SET 152* SET 153* SET 148 SET 149 ۹ DATA DATA DATA DATA DATA DATA 1.98 4.21 20.40 78.20 273.16 1.98 4.21 20.40 78.24 273.16 1.38 4.21 20.40 77.74 273.16 1.38 3.71 4.21 20.40 77.74 273.16 1.38 3.71 4.21 20.40 81.73 90.46 90.46 1.29 4.21 20.40 H 0.962 4.9928 8.57 14.296 14.296 30.215 8.57 9.6100 14.296 14.296 14.296 14.296 21.432 31.015 36.259 51.759 0.0896 0.0887 0.0974 0.828 0.828 8.70 0.2020 0.2022 0.2136 0.8602 1.094 9.36 0.1252 0.1252 0.1252 0.1341 0.8898 8.88 DATA SET 143(cont.) SET 145* 146* 147 SET 144* σ SET SET DATA **VII** DATA 1.38 4.21 20.40 83.90 273.16 DATA 1.38 4.21 20.40 78.85 87.42 87.42 1.38 3.71 4.21 20.40 83.90 83.90 80.3 194.9 273.0 373 373 373 273.0 293.0 373.0 373.0 373.0 373.0 472.6 580.8 580.8 H --0.64286 0.97180 5.1337 8.57 -0.64286 0.97180 5.1537 8.57 0.963 0.969 4.980 8.57 9.6100 14.296 14.296 14.296 14.296 14.296 54.954 54.958 0.9836 4.9928 4.9969 SET 140⁴ DATA SET 141* 1434 1424 DATA SET 138(cont. 120.5 121.1 121.1 122.5 122.5 122.5 125.0 125.0 125.0 125.1 125.1 125.1 125.1 a SET SET DATA DATA DATA 20.4 80.6 198.3 273.1 20.4 80.6 198.3 273.1 81.0 194.9 195.0 1511 1532 1532 1572 1572 1673 1673 1773 1773 H 142.7 152.3 164.9 **DATA SET 136** ٩ 137# 138 Ę SET VIN VIN 1811 279 635 565 7668 7668 985 9856 9800 1107 11173 11173 11173 11174 1 ţ.

Not shown on either figure.

| F | ٩ | F | ٩ | Ļ | d | т | d | T | ٩ | ÷ | a |
|--------------|----------------|----------------|--------------|--------------|--------------------|------------|----------------|------------|----------------|----------------|----------------------|
| DATA SET 1 | [59(cont.)# | DATA SI | ET 161* | DATA SET | 162(cont.)* | DAT | A SET 166 | DATA SE | rt 178* | DATA | SET 181* |
| 973 1073 | 85.2 105 | 193.8 292.8 | 5.06 9.6 | 4.17 4.19 | 0.03370 0.03370 | 4.2 | 0.0599 | 879 879 | 70.79 73.82 | 0.310 0.338 | 0.005887 0.005890 |
| 6/11 | 127 | 398.0 | 15.9 | 4.19 | 0.03371 | DAT | 1 SET 167 | 903 | 74.84 | 0.423 | 0.005894 |
| 12/3 | 261 | 491.8 586.6 | 23.U 31.6 | DATA | SET 163 | 4.2 | 0.0381 | 928 928 | 72.97 | 0.601 | 0.005900 |
| DATA | SET 160* | 684.6 | 42.2 | | | | | 951 | 81.51 | 0.699 | 0.005905 |
| | | 784.6 | 55.0 | 1.26 | *660.0 | DATA | SET 168* | 951 | 83.13 | 0.807 | 0.005911 |
| 84.9 | 0.735 | 887.8 | 70.5 | 1.46 | 0.03400 | | | 976 | 87.58 | 0.909 | 0.005915 |
| 88.7 | 0.766 | 988.9 | 88.1 | 1.64 | 0.03401 | 4.2 | 0.0368 | 979 | 86.57 | 10.1 | 0.005922 |
| 87.4 | 0.784 | 1085.8 | 107.5 | 1.84 | 0.03403 | | 4031 22 | 1000 | 91.02 | 1.10 | 0.005928 |
| 0.44 0.46 | 0.010 | 1.1021 | F100.4 | 10.7 | 0.03405 | | JEI 107- | 1022 | 19.26 | 1.20 | 0066000.0 |
| 98.1 | 0.978 | DATA | SET 162* | 2.44 | 0.03406 | 4.2 | 0.0390 | 1022 | 97.39 | DATA | SET 182* |
| 103.2 | 1.09 | | | 2.85 | 0.03408 | | | 1045 | 101.13 | | |
| 108.7 | 1.19 | 1.16 | 0.03368 | 3.05 | 0.03411 | DAT | SET 170 | 1050 | 102.65 | 1.02 | 0.005216 |
| 114.0 | 1.26 | 1.23 | 0.03368 | 3.25 | 0.03412 | | | 1072 | 103.25 | 1.17 | 0.005230 |
| 119.1 | 1.33 | 1.27 | 0.03368 | 3.47 | 0.03414 | 4.2 | 0.0317 | 1071 | 104.87 | 1.29 | 0.005239 |
| 123.7 | 1.42 | 1.29 | 0.03368 | 3.67 | 0.03417 | | | 1094 | 105.68 | 1.38 | 0.005250 |
| 129.1 | 1.53 | 1.34 | 0.03368 | 3.84 | 0.03417 | DATA | SET 171* | 1100 | 106.19 | 1.49 | 0.005259 |
| 1.12.9 | 1./3 | 45 · T | 0.03368 | 10.4 | 0.03421 | | 0.00 0 | 9711 | 10/.30 | 1. 29 | 0.005272 |
| | 1.80 | 1.1 | 0.03368 | 07.4 | 0.03423 | 4.2 | 0.4810 | | TOL: 440 | 1.08 | 0.005285 |
| 14/./ | 1.71 | 1.28 | 0.03368 | 14.01 | 0.03/UZ | 747 | CET 173# | NIN | JET 1/3- | 90° | 167500.0 |
| 1.541 | 5.22 5.83 C | 1.67 | 000000 | 14.90 | 0.03715 | VIVA | 7/7 190 | 0 78 | 0 005688 | 1.09 | 016500.0 |
| 1.67.4 | 2.03 | 1.77 | 0.03368 | 15.27 | 12750-0 | 6 4 | 0.2637 | 0.410 | 0.005694 | 88 | 0.005342 |
| 173.0 | 3.04 | 1.89 | 0.03368 | 15.94 | 0.03805 | • | | 0.49 | 0,005699 | 2.20 | 0.005363 |
| 178.4 | 3.33 | 2.00 | 0.03368 | 16.40 | 0.03431 | DATA | SET 173* | 0.59 | 0.005709 | 2.29 | 0.005376 |
| 183.3 | 3.54 | 2.09 | 0.03369 | 16.87 | 0.03857 | | | 0.69 | 0.005716 | 2.40 | 0.005396 |
| 186.0 | 3.78 | 2.13 | 0.03369 | 17.31 | 0.03882 | 4.2 | 0.2261 | 0.80 | 6č25vû°0 | 2.50 | 0.005411 |
| 198.0 | 4.30 | 2.16 | 0.03369 | 17.89 | 0.03925 | | | 0.90 | 0.025742 | 2.60 | 0.005430 |
| 206.3 | 4.69 | 2.35 | 0.03369 | 18.39 | 0.03959 | DATA | SET 174* | 1.01 | 0.005761 | 2.70 | 0.005450 |
| 214.3 | 5.12 | 2.46 | 0.03369 | 18.95 | 0.03994 | | | 1.10 | 0.005773 | 2.79 | 0.005465 |
| 0.712 | C#.C | 07.7 | 90550 0 | 19.40 | 0.04026 | 4.2 | 0.2115 | 1.20 | \$6/CON.0 | 06.2 | 0.005503 |
| 2.122 | | 2.00 | 09150 0 | 70.02 | 0.040.0 | ATAC | CET 1754 | DATA | CET 1804 | 0.0 | |
| 240.2 | 6.40 | 1.2 | 011160 | DATA | SET 164 | | TTTT | | 001 TOC | 00. 6 | |
| 244.3 | 6.75 | 2.98 | 0.03369 | | | 4.2 | 0.0371 | 0.38 | 0.005876 | 2.10 | 0.005564 |
| 252.8 | 7.08 | 3.01 | 0.03369 | 0.38 | 0.03395 | 1 | 2 | 0.42 | 0.005879 | 3.40 | 0.005585 |
| 259.1 | 7.51 | 3.09 | 0.03369 | 0.49 | 0.03396 | DATA | SET 176* | 0.49 | 0.005881 | 3.51 | 0.005606 |
| 266.4 | 7.80 | 3.19 | 0.03370 | 0.95 | 0.03398 | | | 0.70 | 0.005888 | 3.60 | 0.005629 |
| 270.5 | 8.39 | 3.28 | 0.03369 | 1.08 | 0.03399 | 4.2 | 9.0136 | 0.80 | 0.005891 | 3.70 | 0.005650 |
| 274.7 | 8.83 | 3.43 | 0.03370 | 1.27 | 0.03400 | | | 0.90 | 0.005898 | 3.79 | 0.005673 |
| 279.4 | . 9.16 | 3.57 | 0.03370 | | | DATA | SET 177 | 10.1 | 0.005905 | 3.89 | 0.005699 |
| 287.2 | 9.33 | 3.78 | 0.03370 | DATA | SET 165* | | | 1.10 | 0.005910 | 4.11 | 0.005745 |
| C.142 | 0 4 0 | 5.8/ | 0/550 0 | c 7 | 0 JJEE | 4.2 | 0.0354 | 1.20 | 0.005917 | | |
| 7.167 | 7.00 | 14.0 | 01050.0 | 7.4 | CC22.U | | | | | | |

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Fe (continued)

EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF IRON

TABLE 9.

والمحافظة والمتعاد والمناخل والمستحد والمستحفظ فالمتنا ويتجاور والمعالية والمعادية

| Т | ρ | T | σ | F | Q | Т | β | T | σ | T | d |
|--------|----------------------|---------------|--------------------|-----------|------------------|--------------|------------------|--------------|------------------------------|--------------|------------|
| DATA | SET 183* | DATA SET | 184(cont.)* | DATA | SET 196* | DATA SET | 205(cont.) | DATA SET | 201 (cont.) | DATA SET | 209(cont.) |
| 1.41 | 0.012080 0.012093 | 17.6 19.05 | 0.02097 0.02248 | 4.2 | 0.0615 | 1677 1736 | 123.5* 124.3* | 360 380 | 13.446 14.699 | 40.1 1.04 | 0.0941 |
| 1.61 | 0.012093 | 20.7 | 0.02454 | DATA | SET 197 | 1816 | 125.3 | 400 | 16.009 | 42.3 | 0.1047 |
| 1.72 | 0.012099 | | | | | 1816 | 131.3 | | | 43.0 | 0.1083 |
| 1.82 | 0.012098 | DATA | SET 185* | 4.2 | 0.0516 | 2001 | 133.2 | DATA SI | <u>st 208</u> | 43.7 | 0.1134 |
| 2.05 | 0.012124 | 4.7 | 0.0566 | DATA | SET 1984 | 2175 | 136.6 | 1878 | 137.5 | 44.9 45 7 | 0.1216 |
| 2.22 | 0.012148 | • | 2000 | | 0/1 170 | 2505 | 137.8 | 1854 | 138.4 | | 0.110 |
| 2.32 | 0.012165 | DATA | SET 186 | 4.2 | 0.0429 | 2699 | 139.4 | 1877 | 138.4 | DATA | ET 210* |
| 2.50 | 0.012183 | 4.2 | 0.0246 | DATA | SET 199* | 2964 | 141.5* | 1915 | 139.7 | 4.5 | 0.027 |
| 2.52 | 0.012193 | | | | | 2997 | 142.0 | 1953 | 141.9 | 5.8 | 0.027 |
| 2.63 | 0.012215 | DATA | SET 187* | 4.2 | 0.0384 | | | 1980 | 142.6 | 6.7 | 0.027 |
| 8/ · 7 | 0.012238 0.012238 | 6 4 | 0 070 0 | DATA A | 00C 133 | DATA S | ET 206 | 20102 | 143.2 4 143.24 | 0.0 | 0.028 |
| 3.09 | 0.012296 | 4 | 2040.0 | NALA | 201 200 | 1726 | 126.7 | 2065 | 144.5* | 6.0 9.6 | 0.028 |
| 3.26 | 0.012329 | DATA | SET 188* | 4.2 | 0.0358 | 1748 | 126.7 | | - - - | 10.5 | 0.028 |
| 3.41 | 0.012364 | | | | | 1772 | 127.6 | DATA | SET 209 | 11.4 | 0.029 |
| 3.62 | 0.012405 | 4.2 | 0.0491 | DATA | SET 201* | 1775 | 127.6 | | | 12.3 | 0.029 |
| 00.0 | 0.012438 | ATA S | 36T 1804 | c 7 | 0 0336 | 19/1 | 128.5 | 0.0 | 0.0410 | 14.3 | 0.030 |
| 4.31 | 0.012571 | VIUA | 101 170 | 4 7 | 00000 | 1822 | 135.2* | 7.2 | 0.0420 | 19.7 | 0.035 |
| | | 4.2 | 0.283 | DATA | SET 202* | 1832 | 135.1* | 8.2 | 0.0423 | 20.9 | 0.036 |
| DATA | SET 184* | | | | | 1838 | 135.5 | 9.1 | 0.0423 | 21.6 | 0.037 |
| | | DATA | SET 190* | 4.2 | 0.0296 | 1852 | 135.9 | 10.0 | 0.0429 | 22.9 | 0.038 |
| 4.7 | 0.01271 | | | | | 1873 | 136.1 | 10.8 | 0.0425 | 24.3 | 0.039 |
| 0°0 | 0.01283 | 4.2 | 0.134 | DATA | V SET 203 | 1884 | 136.9 | 11.6 | 0.0429 | 26.0 | 0.042 |
| | 0.01304 | DATA (| 5PT 101# | 6 7 | 0 0357 | 1061 | 136.3* | 12.6 | 0.0433 | 21.2 | 0.044 |
| 6.1 | 0.01315 | | 1/1 100 | 4 | 1070-0 | CT CT | A. 107 | 17.1 | 0.0458 | 29-9 | 0.048 |
| 6.2 | 0.01329 | 4.2 | 0.109 | DATA | V SET 204 | DATA | SET 207 | 20.7 | 0.0482 | 31.2 | 0.051 |
| 9.0 | 0.01329 | i | | | | ; | | 21.8 | 0.0499 | 31.9 | 0.053 |
| | 0.0177 | NIN | 261 132 | 4.2 | 0.0248 | 0.6 | 1.210 | 23.1 | 0.000 | 0.66 | 0.020 |
| 8.1 | 0.01395 | 4.2 | 0.0926 | DATA S | ET 205 | 120 | 1.907 | 26.2 | 0.0544 | 35.3 | 0.063 |
| 8.6 | 0.01421 | | | | | 140 | 2.654 | 27.5 | 0.0561 | 36.7 | 0.068 |
| 9.2 | 0.01448 | DATA | SET 193* | 1007 | 94.3* | 160 | 3.452 | 28.6 | 0.0579 | 37.8 | 0.073 |
| 9.6 | 0.01479 | • | | 1044 | 102.8* | 180 | 4.299 | 30.0 | 0.0603 | 39.0 | 0.079 |
| r.91 | 41CIU.U | 4.2 | 0.0884 | 1098 | 107.6* | 200 | 5.172 | 31.2 | 0.0632 | 40.3 | 0.085 |
| 11 95 | 0.01622 | 14TA | 10/÷ | 7011 | 49.7TT | 070 | 0/6.0 |).16 1.55 | 0.001.0 | 9.14 0.14 | 0.006 |
| 12.81 | 0.01678 | | L(T 170 | 1295 | 116.4* | 260 | 7,964 | 1.00 | 0.0708 | 6.54 | 0.099 |
| 13.96 | 0.01765 | 4.2 | 0.0799 | 1421 | *1.9.1 | 280 | 8.966 | 35.4 | 0.0746 | 44.0 | 0.105 |
| 15.0 | 0.01850 | | | 1501 | 120.4* | 300 | 10.002 | 36.7 | 0.0788 | 44.9 | 0.114 |
| 15.6 | 0.01892 | DATA | SET 195* | 1627 | 122.5* | 320 | 11.102 | 7.76 | 0.0834 | 47.8 | 0.135 |
| 16.4 | 0.01973 | 4.2 | 0.0635 | 1677 | 123.0* | 340 | 12.255 | 39.3 | 0.0893 | 49.4 | 0.146 |
| | | | | | | | | | | | |

* Not shown on either figure.

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| TABLE |

| ۹ ۲ | F | | L | d | F | d | ÷ | م | H | e |
|--------------------|----------|-------------|------------|------------|----------|------------|----------------|--------------------|----------|-----------------|
| DATA SET 211* | DATA SET | 213(cont.)* | DATA SET 2 | 14(cont.)* | DATA SET | 217(cont.) | DATA SET | 217(cont.) | DATA SET | 217(cont.) |
| 4.4 0.057 | 1803 | 135.9 | 1915 | 137.6 | 453.2 | 20.18* | 923.2 | 77.04* | 1046.95 | 102.33* |
| 6.6 0.057 | | 136.1 | 1915 | 13/./ | 473.2 | 21.82* | 933.2 043 2 | 18.7/# 90 5/# | 1048.2 | 102.58* |
| | 1816 | 2.001 | 1661 | CD - 06T | 2.692 | 23.58# | 948.2 | 81.44* | 1050.7 | 103.00 |
| 0.059 | 1842 | 136.45 | DATA SE | T 215* | 503.2 | 24.51* | 953.2 | 82.40 | 1053.2 | 103.40* |
| 12.4 0.058 | 1857 | 136,65 | | | 513.2 | 25.46* | 958.2 | 83.30* | 1055.7 | 103.77* |
| 4.4 0.059 | 1858 | 136.75 | 1693 | 125.8 | 523.2 | 26.41* | 963.2 | 84.21* | 1058.2 | 104.13* |
| 6.3 0.059 | 1874 | 136.9 | 1773 | 127.1 | 533.2 | 27.38* | 968.2 | 85.12* | 1063.2 | 104.98 |
| 18.7 0.060 | 1875 | 137.0 | 1813 | 132.1 | 543.2 | 28.33* | 973.2 | 85.92* | 1068.2 | 105.63* |
| 13.2 0.064 | 1893 | 137.2 | 1832 | 133.7 | 553.2 | 29.29 | 978.2 | 86.87* | 1073.2 | 106.37* |
| 190 . 0067 | 1900 | 137.35 | 1874 | 137.6 | 563.2 | 30.22* | 983.2 | 87.85* | 1078.2 | 106.89 |
| 9.9 0.071 | 1905 | 137.4 | | | 573.2 | 31.18* | 988.2 | 88.84 | 1083.2 | 107.38* |
| 13.6 0.076 | 1919 | 137.6 | DATA S | ET 216* | 583.2 | 32.16* | 993.2 | 89.56* | 1088.2 | 107.85 |
| 15.7 0.064 | | | | | 593.2 | 33.16* | 995.2 | ×10.07× | 1093.2 | 108.31* |
| 18.2 0.090 | DATA | SET 214* | 1683 | 121.167 | 603.2 | 34.18* | 998.2 | 90.60* | 1098.2 | 108.73* |
| 0.5 0.100 | : | | 1692 | 122.332 | 613.2 | 35.22* | 1000.2 | 91.12* | 1103.2 | 109.14 |
| 2.8 0.112 | 1673 | 127.05 | 1703 | 121.577 | 623.2 | 36.28* | 1003.2 | 91.64* | 1108.2 | 109.53* |
| 6.1 0.130 | 1708 | 127.65 | 1/13 | 122.358 | 633.2 | 37.37* | 1002.7 | AZ.1/* | 1113.2 | 109.93 * |
| | 1728 | 127.95 | 1723 | 121.986 | 643.2 | 38.46* | 1008.2 | 92.72 | 1118.2 | 110.29* |
| MTA SET 212 | 1748 | 128.2 | 1732 | 121.998 | 653.2 | 39.56 | 1010.7 | 93.27* | 1123.2 | 110.63* |
| | 1764 | 128.55 | 1743 | 123.935 | 663.2 | 40.67* | 1013.2 | 93.834 | 1128.2 | 110.96 |
| 5 126.4 | 1111 | 133.45 | 1752 | 124.332 | 673.2 | 41.80* | 1015.7 | 94.38* | | |
| 3 126.65 | 1802 | 136.2 | 1762 | 123.960 | 683.2 | 42.96* | 1018.2 | 94.95* | | |
| 5 127.0 | 1814 | 136.2 | 1783 | 126.678 | 693.2 | 44.14* | 1020.7 | 95.52* | Ŀ | 00- |
| 9 127.35 | 1817 | 136.4 | 1793 | 126.306 | 703.2 | 45.35* | 1023.2 | 96.11* | • | Pr La |
| 6 129.9 | 1822 | 136.15 | 1808 | 126.709 | 713.2 | 46.62* | 1025.7 | 96.70* | | |
| 9 134.1 | 1829 | 136.4 | 1808 | 134.402 | 723.2 | 47.86* | 1028.2 | 97.31* | DATA S | ET 218* |
| 6 135.65 | 1833 | 136.45 | 1812 | 134.792 | 733.2 | 49.11* | 1030.7 | 97.93 | | 017 17 |
| 3 135.85 | 1841 | 136.75 | 1823 | 135.960 | 743.2 | 50.38* | 1033.2 | 98.57* | 10 0 | 0 68 |
| 5 135.9* | 1843 | 136.45 | 1833 | 134.819 | 753.2 | 51.63 | 1034.45 | 98.90 * | 10.49 | 0.0 |
| 4 136.2 | 1845 | 136.65 | 1843 | 131.369 | 763.2 | 52.93* | 1035.7 | 99.24 | 11 11 | 1 13 |
| 5 136.2* | 1850 | 136.7 | 1649 | 138.685 | 773.2 | 54.26* | 1036.95 | 99.58* | 11.80 | 117 |
| 4 136.35 | 1850 | 136.95 | 1853 | 131.382 | 783.2 | 55.61* | 1038.2 | 99.92 * | 12 75 | 1 38 |
| 2 136.5* | 1863 | 136.95 | 1853 | 139.075 | 793.2 | 57.00* | 1039.45 | 100.28 | 11 20 | 1.50 |
| 0 136.55 | 1864 | 137.1 | 1858 | 138.697 | 803.2 | 58.39* | 1039.7 | 100.33* | 07.01 | |
| 5 136.8 | 1866 | 136.8 | 1864 | 133.704 | 813.2 | 59.83* | 1040.2 | 100.47* | 00.61 | 1.04 |
| | 1869 | 137.05 | 1864 | 139.088 | 823.2 | 61.27* | 1040.7 | 100.62* | 14.00 | 74.7 |
| TA SET 213* | 1876 | 137.0 | 1864 | 138.326 | 833.2 | 62.70* | 1041.2 | 100.79* | 26.01 | 16.2 |
| | 1878 | 137.2 | 1874 | 39.486 | 843.2 | 64.17* | 1041.7 | 100.95* | 10.32 | 91.5 5 |
| 6 126.9 | 1879 | 137.35 | | | 853.2 | 65.67 | 1043.2 | 101.39* | 11.11 | 2/.0 |
| 99 127.25 | 1889 | 137.2 | DATA | JeT 217 | 863.2 | 67.20* | 1043.7 | 101.56 | 11.99 | 5 |
| 0 127.55 | 1893 | 137.45 | | | 873.2 | 68.76* | 1044.2 | 101.70* | 10.04 | 4.00 |
| 41 127.9 | 1894 | 137.55 | 373.2 | 14.62* | 883.2 | 70.35* | 1044.7 | 101.83* | 10.00 | 4.97 |
| 50 128.15 | 1896 | 137.35 | 393.2 | 15.88 | 891.2 | +66.12 | 1045.2 | 101.95* | 19.88 | 62.0 |
| 129 4 | 1905 | 57 211 | 6 117 | 17 234 | - EU0 | 79 66 | 1045 7 | 102 00# | 20.47 | 5.69 |
| 115 5 | 1010 | 26 161 | | 10 66 | 2.000 | 15 32 | 6 9701 | 10. 21+ | 21.10 | 6.14 |
| | | | | | 1.1.1 | | | 141.44 | | |

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| <u>\ SET 218(cont.)*</u> 21.78 6.64 22.46 7.12 22.91 7.44 22.45 8.07 23.45 8.74 23.45 8.74 24.40 9.06 | | ٥ | F | ٩ | H | ٩ | ч | ٩ | |
|--|---------------|------------------------|---------------------|--------------------------|----------|------------------------|----------------|------------------------|--|
| 11.78 6.64 22.46 7.12 22.91 7.44 23.23 7.80 23.45 8.07 23.45 8.07 23.40 9.06 24.90 9.64 | DATA SET | 219(cont.)* | DATA S | ET 221* | DATA SET | 222(cont.)* | DATA SET | 223(cont.)* | |
| 22.46 7.12 22.91 7.44 23.23 7.80 23.45 8.07 23.45 8.07 24.40 9.06 | 48.7 | 15.0×10 ⁻² | 1.72 | 0.233 × 10 ⁻² | 2.20 | 0.158×10 ⁻² | 5.41 | 0.122×10^{-2} | |
| 22.91 7.44 23.23 7.80 23.45 8.07 23.40 9.06 24.90 9.64 | 52.8 | 19.2 | 1.85 | 0.235 | 2.40 | 0.159 | 7.61 | 0.190 | |
| 23. 23 7.80 23.45 8.07 24.40 9.06 24.90 9.64 | 58.8 | 26.6 | 2.12 | 0.237 | 2.59 | 0.162 | 10.4 | 0.300 | |
| 23.45 8.07 23.95 8.74 24.90 9.06 | 68.5 | 37.7 | 2.24 | 0.239 | 2.88 | 0.168 | 13.3 | 0.458 | |
| 13.95 8.74 24.40 9.06 24.90 9.64 | 73.7 | 51.5 | 2.41 | 0.241 | 3.13 | 0.171 | 14.7 | 0.545 | |
| 14.40 9.06 14.90 9.64 | 89.8 | 90.0 | 2.49 | 0.241 | 3.36 | 0.176 | 18.2 | 0.839 | |
| (4.90 9.64 r 27 0.02 | 137 | 249 | 2.70 | 0.243 | 3.68 | 0.177 | 22.2 | 1.28 | |
| | 172 | 393 | 2.86 | 0.248 | 4.06 | 0.184 | 25.0 | 1.75 | |
| 12.6 9.20 | 213 | 567 | 3.07 | 0.248 | 4.45 | 0.189 | 29.1 | 2.41 | |
| 5.81 10.32 | 271 | 840×10^{-2} | 3.30 | 0.252 | 5.68 | 0.223 | 35.1 | 4.38 | |
| 6.26 10.90 | | | 3.48 | 0.257 | 6.39 | 0.251 | 39.5 | 6.15 | |
| 6.76 11.58 | DATA | SET 220* | 3.68 | 0.259 | 6.93 | 0.265 | 43.6 | 7.88 | |
| 7.35 12.30 | | | 3.92 | 0.264 | 8.23 | 0.309 | 52.3 | 16.4 | |
| 7.89 13.07 | 1.70 | 0.645×10^{-2} | 4.32 | 0.271 | 9.69 | 0.175 | 60.4 | 24.8 | |
| | 1.88 | 0.645 | 4.73 | 0.276 | 12.6 | 0.512 | 70.4 | 46.8 | |
| | 2.02 | 0.651 | 5.77 | 0.300 | 14.6 | 0.612 | 80.6 | 68.9 | |
| | 16 6 | 0 657 | 717 | 0 337 | 10.41 | 0.000 | 0.000 1. Ag | 00 J | |
| T C | 87.7 7 7 8 | 0.054 | 00 0 | 015.0 | 3 76 | 0.920 | | 102 | |
| | 2 · · · | 0.000 | 0.10 | 104 0 | | 1.4.1 10.1 | 7.76 | 201 | |
| ATA SET 2104 | 11.7 | 700.0 | 0.4.61 | 104.0 | | 40.1 | 7.02 | 011 | |
| ATT 130 110 | | 0.002 | 1 2 1 | 0.407 | 1.40 | 00.0 | 761 | 101 | |
| 1.73 2.68*10 | 3.40 | 0.674 | 14.9 | 969.0 | | 21.2 | 147 | 201 | |
| 1 88 2 70 | 1.666 | 0.674 | 16.0 | 0 770 | 0.02 | 3.15 | 173 | 2/2 | |
| 2.02 2.70 | 3.83 | 0.673 | 21.3 | 1.20 | 82.6 | 8.04 | 000 | 579 | |
| 2.19 2.70 | 4.23 | 0.686 | 24.6 | 1.55 | 88.9 | 6.77 | 237 | 502 | |
| 2.73 | 4.79 | 0.685 | 27.2 | 2.00 | 114 | 151 | 276 | 934 | |
| 1 CT 2 T | 5.54 | 0.710 | 11.5 | 1.23 | 461 | 214 | 202 | 1020×10 ⁻² | |
| 1.00 2.7 | 7.13 | 0.757 | 37.4 | 4.80 | 164 | 335 × 10 ⁻² | 4 | | |
| 1 to 2 11 | | | | | 101 | | | | |
| | 0.0 | 0.025 | T - T | 76.6 | | | | | |
| | (') I | 1.66/ | * | 0.01 | NIN | 121 223 | | | |
| 6/.7 01.4 | 7-61 | 0.1 | 1.00 | 1.22 | | · | | | |
| C/.7 7C.C | A-97 | 1.30 | C.67 | 42.0 | 1. J | 0.Ub3Lx 10 | | | |
| 5. 38 2. /B | 20.9 | 1.54 | 106 | 123 | 1.70 | 0.0631 | | | |
| 7.43 2.78 | 33.5 | 3.79 | 119 | 180 | 1.82 | 0.0643 | | | |
| 8.35 2.83 | 49.2 | 11.8 | 127 | 192 | 1.92 | 0.0643 | | | |
| 0.0 2.85 | 54.9 | 17.3 | 172 | 358 | 2.11 | 0.0661 | | | |
| 1.0 2.93 | 67.1 | 30.0 | 200 | 517 | 2.24 | 0.0673 | | | |
| 1.9 2.99 | 1.9.1 | 56.5 | 240 | 645 | 2.45 | 0.0692 | | | |
| 4.2 3.10 | 99.4 | 116 | 268 | 782×10^{-2} | 2.64 | 0.0718 | | | |
| 6.3 3.24 | 107 | 133 | | | 2.76 | 0.0738 | | | |
| 7.5 3.33 | 138 | 237 | DATA S | ET 222* | 2.91 | 0.0765 | | | |
| 1.1 3.69 | 165 | 345 | | | 3.21 | 0.0801 | | | |
| 7.4 4.85 | 191 | 446 | 1.62 | 0.154×10^{-2} | 3.58 | 0.0846 | | | |
| 7.5 7.60 | 258 | 718 | 1.75 | 0.155 | 3.84 | 0.0894 | | | |
| 0.3 8.96 | 301 | 981×10^{-2} | 1.88 | 0.158 | 4.17 | 0.0953 | | | |
| 3.3 11.0×10 ⁻² | | | 2.06 | 0.158×10^{-2} | 4.52 | 0.103×10^{-2} | | | |

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3.4. Nickel

There are more than 100 data sets available for the electrical resistivity of nickel. The information on specimen characterization and measurement condition for each of the data sets is given in table 11. The data are tabulated in table 12 and shown partially in figures 7 and 8.

Since nickel belongs to the same group in the periodic table as iron and is also ferromagnetic, the electrical resistivity of nickel is expected to resemble that of iron. For example, the solute resistivities of dilute nickel alloys are similar to those of dilute iron alloys in magnitude and in temperature dependence (Schwerer and Cuddy [148]). However, since nickel is not as strongly magnetic as iron (with a spontaneous magnetization of 6.4 kG as compared to 21.8 kG for iron), the magnetic effect on the electrical resistivity is not as strong in nickel as it is in iron. While the minimum in the longitudinal magnetoresistance at 4 K of a pure iron specimen occurs at \gtrsim 750 Oe (\sim 60 x 10³ Am⁻¹) (for example, see Fujii and Morimoto [112]), it occurs at \sim 250 Oe for pure nickel (Wycisk and Feller-Kniepmeier [209] and Fujii [210]). Furthermore, for iron the resistivity at the minimum can be as low as one third of the value at zero applied magnetic field. For nickel, it was only about 18% lower [209,210].

The electrical resistivity of nickel has not been investigated as widely as that of iron, and there has been apparently lesser effort spent in its purification. In fact, among the data sources reporting the electrical resistivity of nickel, less effort was made to analyze the impurity content of the specimen than those reporting the electrical resistivity of iron. Nonetheless, there are a few data sets which show very good agreement on the residual resistivity of pure nickel: $0.0033 \times 10^{-8} \Omega m$ at 2.32 K from White and Tainsh [210] (data set 31), $0.0031 \times 10^{-8} \Omega m$ at 1.85 K from Ehrlich et al. [212] (data set 73), and $0.0033 \times 10^{-8} \Omega m$ from Wycisk and Feller-Kniepmeier [209] (data set 96). The recommended values for the residual resistivity (at 1 K) is based on these data sets. The specimens of the first two sources were described as "high purity" and "pure", respectively. The specimen of the last source was 99.999% pure and was five-time electron beam zone-refined.

The temperature-dependent part of the electrical resistivity has been reported to contain mostly of a T^2 component at low temperatures (≤ 10 K): see,

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for example, White and Woods [21] (data sets 33-34), Ehrlich and Rivier [213] (data set 10), Greig and Harrison [214] (data set 4), Fert and Campbell [215] (data set 48), Price and Williams [80] (data set 55), and Sudovtsov and Semenenko [203] (data sets 77,78). An analysis similar to that applied in treating the low-temperature data on the electrical resistivity of iron, i.e., plotting the quantity

$$\rho - \rho_0 - A \left(\frac{T}{\theta_R} \right)^5 \int_0^{\theta_R/T} \frac{x e^x}{(e^x - 1)^2} dx$$

with values of A and $\theta_{\rm R}$ equal to 39.1 x $10^{-6}\;\Omega\,m$ and 456 K, respectively, gives very similar results. It increases as T^2 at temperatures below ~ 50 K. It then varies much less rapidly with temperature: with some data sets (e.g., data sets 55,57) there is a plateau at \sim 110 K, and with some (e.g., data sets 3,43) there is a minimum at around the same temperature. At temperatures above 150 K, it increases more rapidly and approaches a T^3 dependence. The coefficient of the T² term (for temperatures below about 50 K) varies between $0.5 \times 10^{-5} \Omega m K^{-2}$ (data set 48) and $\sqrt{3.5} \times 10^{-5} \Omega m K^{-2}$ (data set 57), and furthermore there is no discernible correlation between these coefficients and the residual resistivities of the specimens. However, the agreement between data sets with the lowest reported residual resistivities are good. The data set of White and Tainsh [211] (data set 31) yields a coefficient of 2.7 x $10^{-5} \Omega m K^{-2}$ and a residual resistivity of $\sqrt{0.0033} \times 10^{-8} \Omega m$, that of Ehrlich and Rivier [213] (data set 10) yields 2.4 x $10^{-5} \Omega \text{ m K}^{-2}$ and 0.0031 x $10^{-8} \Omega \text{ m}$, respectively. The data set of Farrell and Greig [216] (data set 11) yields 2.6 x $10^{-5} \Omega m K^{-2}$ and 0.0095 x 10^{-8} Ω m, and that of Ehrlich et al. [212] (data set 73) yields 2.3 x $10^{-5} \Omega m K^{-2}$ and 0.0031 x $10^{-6} \Omega m$. The recommended values below 60 K are based on the above four data sets, with the values of the coefficient, 2.6 x $10^{-5} \Omega m K^{-2}$ is also the mean of the above four values. It should be mentioned that the plateau or the minimum region in the quantity

$$\rho - \rho_0 - A \left(\frac{T}{\theta_R}\right)^5 \int_0^{\theta_R/T} \frac{x e^x}{(e^x - 1)^2} dx$$

at around 110 K could not be eliminated by an effort in adjusting the values of A and θ_R . As a consequence, the value of θ_R was taken to be 456 K and the value of A was chosen so that the range of applicability of the T² term could be extended to as high a temperature as practicable. As an illustration, the

data of Farrell and Greig [216] (data set 11) deviate from the T^2 line by +0.005 x $10^{-8} \Omega m$ at 50 K; this deviation increases to -0.02 x $10^{-8} \Omega m$ at 60 K.

In the temperature range from about 60 K to room temperature, a number of authors reported data sets which agree well with each other: White and Woods [21] (data sets 33,34), Farrell and Greig [216] (data set 11), Laubitz et al. [217] (data set 52). In particular, the last two data sets merge very well at 90 K. The recommended values in this temperature range is based on the above four data sets, with more weight given to the last two.

For temperatures from the ice point up to the Curie point, a number of data sets agree to within $0\pm4\%$: Pallister [218] (data set 14), Powell et al. [219] (data sets 17,20), Kierspe et al. [78] (data set 37), Schroeder and Giannuzzi [98] (data set 51), Laubitz et al. [217] (data set 52), Potter [199] (data set 53), Schwerer and Cuddy [148] (data set 65), and Ahmad and Greig [220] (data sets 89,90). Of these, the data of Laubitz et al. and of Potter show particularly good agreement ($\pm2\%$). The recommended values in this temperature range are based on these results, with more weight given to those of Laubitz et al. [13] (data set 52) and of Potter [199] (data set 53).

The Curie temperature of nickel has been reported to be 631 K by Zumsteg and Parks [221] (data set 91), 631 K by Standley and Reich [222] (data set 2), 630 K by Dutta-Roy and Subrahmanyam [223] (data set 3), \sim 630 K by Laubitz et al. [13] (data set 52), 632.7 K by Jackson and Saunders [224] (data set 103), and from 629.3 to 629.8 K, depending on specimen, by Potter [199] (data set 53). Judging from the resistivity data of Pallister [218] (data set 14), the Curie temperature is \sim 627 K, of Kirichenko and Mikryukov [225] (data set 27), \sim 631 K, of Schwerer and Cuddy [148] (data set 65), \sim 628 K, of Kaul [226] (data set 67), 620-640 K, of Shirakawa [141] (data set 76), ~633 K, and of Schroeder and Giannuzzi [98] (data set 51), ~638 K. Among these sources, only two, Potter [199] (data set 53) and Zumsteg and Parks [221] (data set 91), give in detail the change of electrical resistivity at around the Curie temperature. The agreement between these are very good: $\pm 0.5\%$ below and $\pm 1\%$ above the Curie temperature. The recommended values in the vicinity $(\pm 25 \text{ K})$ of the Curie temperature are based on this reference, with more weight given to the result of Zumsteg and Parks at temperatures above the transition. The resultant values are within 0.3% of those calculated on the basis of the $d\rho/dT$ values reported by Jackson and Saunders [224].

At temperatures from the Curie point to about 1300 K, the following data sets fall into a band of width $\sim 2 \times 10^{-8} \Omega$ m: Pallister [218] (data set 14), Bode [227] (data set 16), Powell et al. [219] (data set 20), Davis et al. [228] (data set 32), Laubitz et al. [217] (data set 52), and Potter [199] (data set 53). The recommended values in this temperature range are based on these data sets, with more weight given to the data of Laubitz et al. [217] (data set 52). Data set 52 is also used as basis for recommendation for lower temperatures.

Unfortunately, most of the data sets mentioned in the previous paragraph are for temperatures below 1300 K. For higher temperatures, the available data sets show large discrepancies. In addition, the resistivity values for lower temperature given in these sets are quite different from the recommended values (for example, data sets 37,72). However, for temperatures slightly below the melting point, the data of Güntherodt et al. [92] (data set 93) and of Kita et al. [93] (data sets 100-101) are within $\sim 0.5 \times 10^{-8} \Omega m$ of each other. Extrapolations, either graphically or numerically using a cubic expression, from recommended values for lower temperatures give values that are also within $0.5 \times 10^{-8} \Omega m$ of the values reported by these authors. The recommended values are, therefore, obtained from the numerical extrapolation.

At temperatures immediately above the melting point, the available data sets show a spread of about 6 x $10^{-8} \Omega m$. Between the data of Güntherodt et al. [92] (data set 93) and of Kita et al. [93] (data sets 100-102), which well agree below the melting point, the difference is about 4 x $10^{-8} \Omega m$. The recommended value for the liquid phase at the melting point is based on the results of Güntherodt et al. [92] (data set 93), Seydel and Fucke [87] (data set 92). and Mokrovskii and Regel [158] (data set 56), which agree to within 0.2 x $10^{-8} \Omega m$. The temperature dependence of the electrical resistivity in the molten state has been generally reported to be linear, e.g., Kita et al. [93] (data sets 100,101), Güntherodt et al. [92] (data set 93), Seydel and Fucke [87] (data set 92), Samarin [94] (data set 87), Mokrovskii and Regel [158] (data set 56), Eliutin et al. [88] (data set 49), and Ono and Yagi [89] (data set 61). The recommended values are generated with a temperature coefficient of 0.011 x $10^{-6} \Omega m K^{-1}$, which is slightly (6%) lower than that given by Kita et al. [93], and slightly higher (\sim 1%) than that determined from the data of Güntherodt et al. [92] (data set 93).

The recommended values for the solid state both uncorrected and corrected for thermal expansion of the material and those for the liquid state corrected

for thermal expansion are presented in table 10, and the values except those corrected for thermal expansion of the solid are also shown in figures 7 and 8 along with the experimental data. These values at temperatures above 100 K are for nickel of purity 99.99% or higher, while those below 100 K are applicable only to highly purified zone-refined nickel having a residual resistivity of $0.00320 \times 10^{-8} \Omega m$. The estimated uncertainty in the recommended values is $\pm 5\%$ below 150 K, $\pm 3\%$ from 150 to 1300 K, $\pm 5\%$ from 1300 K to the melting point, and $\pm 10\%$ for the liquid state.

For slightly less pure nickel having different residual resistivity, its electrical resistivity values can be calculated from the recommended values using the Matthiessen's rule, which will not introduce serious errors. For example, the data of Ahmad and Greig [220] (data set 90) show that for a specimen with a residual resistivity less than 0.009 x $10^{-8} \Omega$ m, the application of Matthiessen's rule causes an error of about 2% at 40 K and about 1% at 260 K. Also the data of Greig and Harrison [214] (data set 4), Ahmad and Greig [220] (data set 89), Berger and Rivier [229] (data set 23), White and Woods [21] (data sets 33,34), and of Kemp et al. [130] (data set 43), which are for specimens with residual resistivities of the order of a few tenths of a n Ω m, show that the application of Matthiessen's rule causes errors generally of about 3% for temperatures below 300 K. The most interesting comparison is made with the data of Rowlands [230] (data set 57), since his data extend from liquidhelium temperatures up to above the Curie temperature. For this data set, the errors are less than 1% below 20 K, 10% at ~ 60 K, $\sim 6\%$ from ~ 100 to ~ 300 K, and drop to $\sim 3\%$ from ~ 500 K to above the Curie temperature. This behavior is consistent with the solute resistivities for dilute nickel alloys (see, for example, Schwerer and Cuddy [148]). Thus, when the Matthiessen's rule is used for calculating the electrical resistivity of less-pure nickel with a residual resistivity less than 0.05 x $10^{-6} \Omega m$, the values are likely to be lower by $\sqrt{3}$ than the true values from 40 K to room temperature, and are likely to lower by <1% at temperatures below 40 K and above the Curie temperature. For specimens of even lower purity, with a residual resistivity of about 0.3 x $10^{-8} \Omega m$, the probable errors are about 2% at high and at low temperatures, but may be as high as -10% at intermediate temperatures (40-300 K).

The recommended values for the solid state uncorrected for thermal expansion and those for the liquid state given in table 10 can be represented approximately by the following expressions to within $\pm 0.5\%$.

1-60 K: $\rho = 0.0032 + 2.5 \times 10^{-5} T^{2} + 39.1 \left(\frac{T}{456}\right)^{5} \int_{0}^{456/T} \frac{x^{5} e^{x}}{(e^{x}-1)^{2}} dx$

60-150 K:

$$\rho = 0.4214558798 - 2.07384562 \times 10^{-2}T + 3.48017305 \times 10^{-4}T^{2} - 8.609303313 \times 10^{-7}T^{3}$$
(36)

(35)

150-500 K:

$$\rho = -1.355285714 + 2.103190475 \times 10^{-2}T + 1.141428571 \times 10^{-5}T^{2} + 4.523809524 \times 10^{-6}T^{3}$$
(37)

500-600 K:

$$\rho = -50.1320558 + 2.978166536 \times 10^{-1}T - 5.156360117 \times 10^{-4}T^{2} + 3.824418489 \times 10^{-7}T^{3}$$
(38)

600-630 K:

$$\rho = 28.71 - 1.2315000 \times 10^{-1} (T_{C} - T) + 5.749999984 \times 10^{-4} (T_{C} - T)^{2}$$
(39)

631-670 K:

$$\rho = 28.71 + 9.060833333 \times 10^{-2} (T-T_C) - 1.809583333 \times 10^{-3} (T-T_C)^2 + 3.9416666667 \times 10^{-5} (T-T_C)^2 - 3.5416666667 \times 10^{-7} (T-T_C)^4$$
(40)

670-1400 K:

$$\rho = -6.329325957 + 8.023011038 \times 10^{-2} T - 4.451156858 \times 10^{-5} T^{2} + 1.201757591 \times 10^{-8} T^{3}$$
(41)

1400-1728 K:

$$\rho = -9.255955877 + 7.140577598 \times 10^{-2} T - 2.771379283 \times 10^{-5} T^{2} + 5.589224949 \times 10^{-9} T^{3}$$
(42)

1728-3000 K:

$$\rho = 63.22 + 1.10 \times 10^{-2} T \tag{43}$$

It should be emphasized that these expressions do not necessarily suggest any theoretical justification, and should be treated, most appropriately, as numerical aids only. It should also be understood that giving these expressions does not imply a recommendation for the temperature derivative of the electrical resistivity.

| т | (| ρ | T | | ρ |
|-----|-------------|-----------|------|-------------|------------------------|
| | uncorrected | corrected | | uncorrected | corrected |
| 1 | 0.00320 | 0.00320 | 630 | 28.71 | 28.86 |
| 4 | 0.00360 | 0.00359 | 670 | 31.06 | 31.24 |
| 7 | 0.00443 | 0.00442 | 700 | 32.14 | 32.34 |
| 10 | 0.00573 | 0.00572 | 800 | 35.52 | 35.80 |
| 15 | 0.00901 | 0.00899 | 900 | 38.58 | 38.95 |
| 20 | 0.0140 | 0.00140 | 1000 | 41.41 | 41.88 |
| 25 | 0.0212 | 0.0212 | 1100 | 44.06 | 44.65 |
| 30 | 0.0317 | 0.0316 | 1200 | 46.62 | 47.33 |
| 40 | 0.0678 | 0.0676 | 1300 | 49.15 | 50.00 |
| 50 | 0.135 | 0.134 | 1400 | 51.73 | 52.73 |
| 60 | 0.242 | 0.242 | 1500 | 54.36 | 55.54 |
| 70 | 0.377 | 0.376 | 1600 | 56.94 | 58.31 |
| 80 | 0.545 | 0.544 | 1700 | 59.50 | 61.07 |
| 90 | 0.741 | 0.739 | 1728 | 60.22(s) | 61.85(s) |
| 100 | 0.959 | 0.957 | 1728 | | 82.23 ^b (l) |
| 150 | 2.21 | 2.20 | 1800 | | 83.02 ^b |
| 200 | 3.67 | 3.67 | 1900 | | 84.12 ^D |
| 250 | 5.32 | 5.32 | 2000 | | 85.22 ^b |
| 273 | 6.16 | 6.16 | 2500 | | 87.72 ⁵ |
| 293 | 6.93 | 6.93 | 3000 | | 90.22 ^D |
| 300 | 7.20 | 7.20 | | | |
| 350 | 9.34 | 9.35 | | | |
| 400 | 11.78 | 11.80 | | | |
| 500 | 17.67 | 17.72 | | | |
| 600 | 25.54 | 25.66 | | | |

TABLE 10. RECOMMENDED VALUES FOR THE ELECTRICAL RESISTIVITY OF NICKEL^a

[Temperature, T, K; Electrical Resistivity, ρ , $10^{-8} \Omega$ m]

^a The values are for nickel of purity 99.99% or higher, but those below 100 K are applicable only to nickel having a residual resistivity of 0.00320 x 10⁻⁸ Ωm. The columns headed uncorrected and corrected refer to values uncorrected and corrected for thermal expansion, respectively. Solid line separating tabular values indicates solid to liquid state transformation. Provisional value.





| Data No. | Kef. | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------------|-------|---|------|----------------|------------------|-------------------------------------|--|
| | 129 | Kondorskii, E.I., Galkina, O.S., and Chernikova, L.A. | 1958 | × | 2~2 | N | Chemically pure; wire specimen 0.1 to 0.2 mm in diam and 150 to 160 mm long; annealed in vacuum at 1173 K for 1 h; slowly cooled at 100 K/h; residual resistivity 0.20 x 10^{-6} A m. |
| 7 | 222 | Standley, K.J. and Reich, K.H. | 1955 | | 293,473 | Ĩ | Ingot heated in argon to about 1273 K for 12 h; slowly cooled; rolled to a sheet about 0.5 mm thick; discs of the required dismeter punched out; polished on fine emery, annealed in vacuo and electrolytically polished, then annealed in vacuum; $T_{\rm C}$ = 631 K. |
| °. | 223 | Dutta-Roy, S.K. and Subrahmanyam, A.V. | 1969 | 2 | 80-735 | | "Spectrographically pure," from Johnson Matthey Co.; 6 x 0.3 x 30 mm; annealed for 24 h at 1073 K in a vacuum furnace; cleaned in aqua regia; T _C = 630 K. |
| 4 | 214 | Greig, D. and Harrison, J.P. | 1965 | o | 5.6-41 | JM 893; A | Pure; 0.0016 total impurity (mostly Fe and Si); polycrystalline; grain size 0.1 mm ; from Johnson Matthey Co. (JM 893); annealed at 1023 K for 12 h; resistivity values calculated from reported ideal resistivity and ρ_{0}/L_{0} ratio (2.11 \pm 0.01 W ⁻¹ cm ² /K ⁻²). |
| Ś | 231 | Svensson, B. | 1936 | ₽ | 323-623 | | 0.102 Fe, 0.036 Al and S1 each; from Hilger of London; 1 mm in diam and 1 cm long; annealed at 1173 K; resistivity values calculated from measured resistance ratios and a $\rho(273 \text{ K})$ value of 6.58 x 10 ⁻⁸ Ω m from Landolt-Börnstein: Physik-Chem. Tabellen Σ Auft. 5, 1050 (1923). |
| Ŷ | 161 | Broom, I. | 1952 | 8 | 90-373 | | 0.12 Mg, <0.05 Cr, Cu and Mn each, 0.03 C, and 0.01 Co; wire specimen 0.056 cm in diam; annealed at 873 K for 2 h, furnace cooled. |
| 1* | 232 | Lavine, J.M. | 1961 | • | 73-633 | 499 alloy | 99.9 pure; from Driver Harris Co.; T_{C} = 631 K. |
| # | 176 | Kondorskii, E.I. and Sedov, V.L. | 1960 | ۲ | 4.2 | | Electrolytically pure; 5.9 mm in diam and 112 mm long. |
| 6 | 176 | Kondorskii, E.I. and Sedov, V.L. | 1960 | < | 4.2 | | Technically pure; cylindrical specimen 5,9 mma in diam and 112 mm long; vacuum annealed at 1273 K for 8 h; furnace cooled. |
| 10# | 213 | Ehrlich, A.C. and Rivier, D. | 1968 | | 1.6-19 | | "High purity"; polycrystalline plate, electropolished to a thickness of 0.19 mm; $\rho(293 \text{ K})/\rho(4.15 \text{ K}) \approx 2200;$ only $\rho(T) - \rho(0)$ reported where $\rho(0)$ is the resistivity extrapolated to 0 K from data in the 1.75 to 4.15 K range, in which the resistivity is reported to be proportional to T^2 . |
| 11 | 216 | Farrell, T. and Greig, D. | 1968 | < | 4.2-273 | | Pure; 3 mm in diam and 9 cm long; annealed for 15 h at 1123 K; resistivity values calculated from reported $\rho(0)$ and tabular values of $\rho(T)$. |
| 12 | 233 | Kondorskii, E.I., Galkina, O.S., and Chernikova, L.A. | 1957 | < | 1.7-20 | N | 99.9 pure; wire specimen 0.1 to 0.2 mm in diam; supplied by Central Scientific Research Institute of Ferrous Metallurgy; cold drawn; annealed in neutral gas at 1173 K for 1 to 12 h; residual resistivity 1.54 x 10^{-8} Ω m. |
| * Not | shown | in figure. | | 1 | | | |

| Set. | Ref. No. | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|------|-------------|---|------|----------------|-------------------|-------------------------------------|---|
| 1 | 234 | Kurbanniyazov, N., Cheremushkina, A.V., and Akmuradov, B.A. | 1973 | < | 373-773 | d | Pure; specimen of dimensions $3 \times 6 \times 100$ mm; homogenize annealed in vacuum at 1273 K for 24 h, slow cooled in furnace; values from graph. |
| 14 | 218 | Pallister, P.R. | 1965 | < | 273-1550 | ы | 99.84 N1, <0.03 Fe, <0.01 A1, Co, Cr, Cu, Ng, Mn, Mo, Si, Sn, T1, Zn, and Zr each, <0.005 Pb and <0.002 B; supplied by International Nickel Co. (Mond) Ltd.; annealed; measurements made in vacuum; smooth values from table; reported electrical resistivities based upon room temper- ature dimensions. |
| 15 | 235 | Sager, C.F. | 1930 | œ | 327~1016 | | Pure; wire specimen about 0.2 cm in diam and 35 cm long; electrolyzed from Mond anodes; vacuum melted under a pressure of 0.3 mmHg, chill cast, forged, hot rolled and cold drawn through a steel die plate; flash annealed, held at 1023 K for "considerable periods" and "later more thoroughly annealed"; current and potential leads of nickel silver soldered to specimen; density 8.74 g cm ⁻³ . |
| 16 | 227 | Bode, K.H. | 1961 | + | 1098-1241 | | 99.95 pure; wire specimen 1 mm in diam; vacuum melted, cast, polished annealed for 12 h at about 1273 K; measured by compensation method. |
| 17 | 219 | Powell, R.W., Tye, R.P., and Hickman, M.J. | 1965 | × | 293-1123 | Sample l | <pre><0.03 Fe, <0.01 Al, Cr, Co, Cu, Mg, Mn, Mo, Si, Sn, Tl, Zn, and Zr each, <0.005 Pb, and <0.002 B; spectroanalyzed by International Nicke Co.; tubular specimen of 1.272 cm I.D., 1.908 cm 0.D. and 20 cm long; supplied by the Castner Kellner Alkali Co.; density 8.61 g cm⁻³.</pre> |
| 18 | 219 | Poweil, R.W., et al. | 1965 | ~ | 373-773 | Sample 2 | "Very high purity"; electrolytic; tubular specimen of 0.634 cm I.D., 2.801 cm 0.D., and 19 cm long; supplied by National Engineering Lab.; density 8.90 g cm ⁻¹ . |
| 19 | 219 | Powell, R.W., et al. | 1965 | < | 293-623 | Sample 4 | Commercial N1; rod specimen 2.54°cm in diam and about 20 cm long; supplied by Explosives Research and Development Establishment. |
| 20 | 219 | Powell, R.W., et al. | 1965 | × | 293-1323 | Sample 5 JM Lab, No. 4497 | "High spectrographic purity"; trace amounts of Al, Ca, Cu, Li, Mg, Si Ag, and Na; rod 0.5 cm in diam and 15 cm long; supplied by Johnson, Matthey and Co.; density 8.91 g cm ⁻¹ . |
| 21 | 236 | Martynyuk, M.M. and Tsapkov, V.I. | 1973 | t | 298,1726 | | 99.93 pure; specimen 0.3-1 mm in diam and 50 cm long; specimen heated in air by a 400 µsec pulse of 1-4 kAmp; voltage and current measured by double beam pulse oscilloscope; resistivity ¢t melting point deter- mined from break points corresponding to the onset and end of fusion on the relative resistance curve; data not corrected at higher temper- ature. |
| 22 | 229 | Berger, L. and Rivier, D. | 1962 | £ | 4.2-292 | (1) [105]N | Specimen 0.15 cm in diam and 5.2 cm long; supplied by Johnson, Mathe and Co.; annealed for 4 h at 1273 K in a vacuum of 10 ⁻⁵ mmHg; furnace cooled at a rate of 150 K/h; p(273 K)/p(4.2 K) = 60. |
| 234 | 229 | Berger, L. and Rivier, D. | 1962 | 80 | 4.2-273 | (11) 1105 M | Specimen 0.19 cm in diam and 5.0 cm long; from the same stock as the above specimen; annealed for 10 h at 1573 K in hydrogen at 1573 K in a vacuum of 10 ² mmHg for 2 h; p(273 K)/p(4.2 K) = 298. |
| ź | BUICH | in ligure. | | | | | |

| Set . | ke f. | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|--------------|-------|--|------|----------------|------------------|-------------------------------------|---|
| * | 237 | Kronmueller, H. and Buck, O. | 1964 | * | 4-273 | | 99.99 pure; from Johnson, Matthey and Co.; single crystal with one axis parallel to <111>; specimen 3.2 mm in diam and 120 mm long. |
| 4 5.7 | 238 | Neimark, B.E. and Bykova, T.I. | 1965 | | 293-773 | No. 1 | 99.87 (Ni + Co); tube 8.51 mm 0.0. and 8.025 mm I.D.; smoothed values from table. |
| 26# | 238 | Neimark, B.E. and Bykova, T.I. | 1965 | | 373-748 | No. 2 | Tube 12.96 mm 0.D. and 11.025 mm I.D.; smoothed values from table. |
| 2) | 225 | Kirichenko, P.I. and Mikryukov, V.E. | 1964 | | 313-1172 | | 99.999 [†] pure; 0.3 cm in diam and 30 cm long; forged from sheet; an- nealed in vacuum for 48 h at 1173 K; furnace cooled. |
| 28 | 239 | Jain, S.C., Goel, T.C., and Chandra, I. | 1967 | t | 1152-1320 | | 99.95 pure; filaments 0.05 cm thick, 1 cm wide, and 14 cm long; ob- tained from Johnson, Matthey and Co.; data from figure; experimental method same as Jain and Krishnan, Proc. R. Soc. London, <u>A225</u> , 7, 1954. |
| 29 | 240 | Watson, T.W. and Robinson, H.E. | 1964 | 2 | 110-803 | | 99.85 N1, 0.11 Co, 0.026 Cu, 0.006 Fe, 0.001 A1, <0.004 S1, <0.002 T1, <0.001 Cr and Mg each, and <0.0005 Mn; electroformed nickel from International Nickel Co.; 2.54 cm in diam and 37 cm long; smoothed values from table. |
| 00 | 240 | Watson, T.W. and Robinson, H.E. | 1964 | ٨ | 384-680 | | The above specimen measured with decreasing temperature. |
| 31 | 211 | White, G.K. and Tainsh, R.J. | 1967 | | 2.3-14 | | "High purity"; speicmen 0.1 cm × 0.1 cm × 7 cm; prepared by Bell Telephone Laboratories; annealed in vacuum of 10 ⁷ Torr at 773 K; p(273 K)/p(4 K) = 2500. |
| 32 | 228 | Davis, M., Densem, C.E., and Rendall, J.M. | 1955 | | 293-1273 | | 0.01-0.2 0, 0.07 C, 0.016 S1, 0.013 Fe, 0.003 S, 0.0005 Mn, and 0.0003 Mg; grade A carbonyl nickel powder; supplied by Mond Nickel Co.; sintered and annealed; density 8.9 g cm ³ ; Curie point 626 K. |
| 5 | 21 | White, C.K. and Woods, S.B. | 1959 | U | 4.2-298 | N1 2 | 99.997 pure, 0.0010 Fe, 0.0010 Si, 0.0003 Cr and Mg each, 0.0002 Ca, Cu, and Mn each, and 0.0001 Ag, from Johnson, Matthey and Co. (JM 10389); rod specimen 2 mm in diam and 6 to 8 cm long; vacuum annealed at 1073 K; resistivity values calculated from reported ρ_1 , $\rho(4, 2 \text{ K})/\rho(295 \text{ K}) = 3.23 \times 10^{-3}$ and $\rho_1(295 \text{ K}) = 7.04 \times 10^{-3}$ G |
| 34 | 21 | White, G.K. and Woods, S.B. | 1959 | с | 4.2-252 | N1 3 | Similar to the above specimen except (1) specimen 0.63 mm in diam, (2) resistivity ratio $\rho(4,2 \text{ K})/\rho(295 \text{ K}) = 4.51 \times 10^{-3}$, (3) $\rho_1(295 \text{ K}) = 7.33 \times 10^{-8} \Omega$ m; because of slight uncertainty in R/A , ρ_1 was normalized to the value for the above specimen for which R and A are more accurately known. |
| 35 | 241 | Reddy, B.K. and Goel, T.C. | 1975 | > | 1163-1641 | | 99.95 pure; tubular specimen 0.75 cm 1.D., 0.3 mm wall thickness, and 18 cm iong; obtained from Johnson, Matthey and Co.; specimen heated for about 1 h at -1630 K and rooled to room tumperature repeatedly for 6 or 7 times. |
| ¥ot • | nuode | in figure. | | | | | |

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| 97 Kovenskii, I.I. and 1963 78 Kierspe, W., and 1967 Samsonov, G.V. 1967 Samsonov, G.V. 1967 Samsonov, G.V. 1967 Samsonov, S.K. and 1961 Bitras, R.R. and 1961 bey, S.K. and 1961 bevelopment Conska, H. N. 1955 Laboratories for Research and Development Laboratories for Research and Development 244 Coltman, R.R., and 1967 Klabunde, C.E., and Ream, J.K.N. 1967 245 Sharma, J.K.N. 1967 313 130 Kemp, W.R.G., and Mitte, G.K. 1927 313 130 Kemp, W.R.G., and 1956 43 130 Kemp, W.R.G., and 1956 44 246 Masumoto, H. 1927 bittrich, K. 1971 247 Rubanenko, I.R. and 1969 Crossman, M.I. Reden, M.I. Renes, P.G., and Revolution, I.R. and Revolu | Method Used | Temp. Range, K Do | Name and Specimen signation | Composition (weight percent), Specifications and Remarks |
|--|----------------|----------------------|-----------------------------------|---|
| 7 78 Kierspe, W., and Conska, H. and Conska, H. Conska, R., and Conska, R. and Dev, S.K. 33* 243 Eirss, R.R. and Development 80 244 Franklin Institute, 1953 Laboratories for Research and Development 81 179 Niccolai, G. 1967 Redman, J.K.N. 1967 Redman, J.K.N. 1967 Redman, J.K.N. 1968 82 245 Sharma, J.K.N. 1967 Redman, W.R.G., and Mitte, G.K. and Mitte, G.K. 1928 83 130 Kemp, W.R.G., and Masumoto, H. 1927 Dittrich, K. 1927 Dittrich, K. 1921 Dittrich, K. 1921 Reseman, M.I. Redman, M.I. Redman, M. Redman, J.K.N. 1968 84 246 Masumoto, H. 1927 Dittrich, K. 1921 Dittrich, K. 1921 Dittrich, K. 1921 Reseman, M.I. Redman, Redman, P. C.A. | + | 891-1673 | | 9.86 Ni, 0.10 C, 0.01 Co, 0.008 Cu, 0.004 Fe, and 0.002 Si and S ach; wire specimen; measured in argon atmosphere, specimen heated by assing an electric current through; smoothed values from figure. |
| 36* 242 Biras, R.K. and 1961 Dey, S.K. 1953 39* 243 Franklin Institute, 1953 1.aboratories for Research and Development 40 244 Coltman, R.R., and Redman, J.K. 1967 419 Niccolai, G. 1908 419 Niccolai, G. 1908 419 Niccolai, G. 1966 4245 Sharma, J.K.N. 1967 43 130 Kemp, W.R.G., and Mitte, G.K. 43 130 Kemp, W.R.G., and Mitte, G.K. 44 246 Masumoto, H. 1927 45 Lucken, A. and Dittrich, K. 47 248 Mitchell, M.A., Reynolds, C.A. | 8 | 73-1668 | | 0.0003 Si, 0.0002 Fe and Mg each, <0.0001 Al, Cu and Ag each; ob- ained from Koch-Light Laboratories Ltd.; smoothed values from figure |
| 194 243 Franklin Institute, 1953 Laboratories for Research and Development 100 244 Coltman, R.R., and Redman, J.K. 1967 Redman, J.K.N. 1908 1179 Niccolai, G. 1908 130 Kemp, W.R.G., and Mitte, G.K. 1310 Kemp, W.R.G., and Mitte, G.K. 1310 Kemp, W.R.G., and Mitte, G.K. 14 246 Masumoto, H. 1927 Dittrich, K. 1927 Dittrich, K. 1927 Dittrich, K. 1928 Rubanenko, I.R. and 1959 Grossman, M.I. 1971 Reynolds, C.A. | | 78-1306 | | moothed values from graph of $ ho$ vs. T/0, with $	heta$ apparently equal to 70 K. |
| 244 Coltman, R.R., 1967 Klabunde, C.E., and Redman, J.K. 1908 11* 179 Niccolai, G. 1908 245 Sharma, J.K.N. 1967 13 130 Kemp, W.R.G., and Mitte, G.K. 1956 4 246 Masumoto, H. 1927 163 Eucken, A. and 1927 163 Eucken, A. and 1969 247 Rubanenko, I.R. and 1969 37 248 Mitchell, M.A., 1971 Reynolds, C.A. | | 73-830 | - | o details reported. |
| 1* 179 Niccolai, G. 1908 2 245 Sharma, J.K.N. 1967 13 130 Kemp, W.R.G., and Mite, G.K. 1956 4 246 Masumoto, H. 1927 5 163 Eucken, A. and 1927 6 247 Rubanenko, I.R. and 1969 6 247 Rubanenko, I.R. and 1969 7 248 Mitchell, M.J. 1971 7 248 Mitchell, M.J. 1971 | | 3.2 | | 9.99 ⁺ nominal purity; 0.025 cm in diam and 5 cm long; annealed at 223 K in air at a pressure of 8 x 10 ⁻⁶ Torr; furnace-cooled. |
| 2 245 Sharma, J.K.N. 1967 13 130 Kemp, W.R.G., and White, G.K. 1956 4 246 Masumoto, H. 1927 5 163 Eucken, A. and 1927 6 247 Rubanenko, I.R. and 1969 6 247 Rubanenko, I.R. and 1969 7 248 Mitchell, M.A., 1971 Reynolds, C.A. | æ | 84673 | | ire specimen 0.5 mm in diam and 8 m long wound on an insulating pool. |
| 3 130 Kemp, W.R.G., and Klemens, P.G., and White, G.K. 1927 4 246 Masumoto, H. 1927 5 163 Eucken, A. and 1927 6 247 Rubanenko, I.R. and 1969 6 247 Rubanenko, I.R. and 1969 7 248 Mitchell, M.A., 1971 7 248 Mitchell, M.A., Ryonids, C.A. | D | 1.5,293 | | 9.995 pure; polycrystalline; wire specimen obtained from Johnson, atthey and Co.; ℓ/A ratio 2.88 x 10^3 cm ⁻¹ . |
| 4 246 Masumoto, H. 1927 5 163 Eucken, A. and 1927 6 247 Rubsnenko, I.R. and 1969 7 248 Mitchell, M.A., 1971 7 248 Mitchell, M.A., Reynolds, C.A. | U | 4.2-293 | | 9.99 ⁺ pure, traces of Al, Ca, Cu, S1 and Ag, and very faint traces f L1, Ng, and Na; 2 mm in diam; obtained from Johnson, Matthey and ω ; annealed in vacuum at 1023 K for 4 h; ideal electrical resistivity, ρ_1 , from figure; ρ_0 taken as 0.0347 x 10 ⁻⁸ Ω m, $\rho = \rho_1 + \rho_0$. |
| 5 163 Eucken, A. and 1927 b1ttrich, K. 1927 6 247 Rubanenko, I.R. and 1969 6 248 Mitchell, M.A., 1971 7 248 Mitchell, M.A., Reynolds, C.A. | | 303 | | .10 Fe, 0.037 C, 0.019 S, 0.013 Cu, 0.006 S1, and trace. of A1, Co, n, and P; 5 mm in diam and 20 cm long: obtained from Mond & Co.; ast and machined; annealed at 1073 K for 40 min. |
| 6 247 Rubanenko, I.R. and 1969 Grossman, M.I. 7 248 Mitchell, M.A., 1971 Klemens, P.G., and Reynolds, C.A. | > | 80,273 | н | lectrolytic. |
| .7 248 Mitchell, M.A., 1971 Klemens, P.G., and Reynolds, C.A. | | 293 | | x 7 x 28 mm; measuring temperature assumed 293 K. |
| | v | 4.2 | 0. 5 . | 9.9 pure; single crystal, grown by a variation of the Bridgman ethod; specimen axis along <lil> direction; annealed in vacuum at 203 K for 48 h.</lil> |
| 16* 215 Fert, A. and 1968 Campbell, I.A. | | 4-79 | - | deal resistivity reported only. |

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TABLE 11. MEASUREMENT INFORMATION ON THE ELECTRICAL RESISTIVITY OF NICKEL NI (continued)

| R S E | | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|-------------|-------|---|------|----------------|-------------------|-------------------------------------|--|
| 49 | 88 | Eliutin, V.P., Turov, V.D., and Maurakh, M.A. | 1965 | × | 1013-1997 | | 98.5-99.0 pure; electrolytic; liquid state obtained by melting in graphite crucible either in an atmosphere of helium or in vacuum. |
| 501 | 249 | Starr, C.D. | 1969 | | 811 | Nickel 270 | 100 nominal purity; temperature coefficient of resistivity $\alpha(298,378) = 0.00565$ and $\alpha(218,298) = 0.00461/deg;$ data from table at 811 K only. |
| 514 | 86 | Schroeder, K. and Glannuzzi, A.J. | 1969 | | 375-825 | | 99.999 pure; wire specimen; annealed in an inert gas atmosphere (92 He, 8 Ar) for 2 h at \sim 150 K above the Curie temperature; resistivity values calculated from reported $\rho(T)/\rho(T_C)$, with $\rho(T_C) = 29.288 \times 10^{-8} \Omega m$, taken from data set 52. |
| 22 | 217 | Laubitz, M.J., Hatsumura, T., and Kelly, P.J. | 1976 | ۲. | 90-1250 | | 99.999 pure (nominal); 0.0016 C, 0.0014 Si, 0.0007 Fe, 0.0006 Cu, 0.0005 Al and 0 ₂ , 0.0003 F, 0.0002 K, Na, and S each, 0.0001 Ta, 0.00007 CI, 0.00005 Ca, 0.00003 Ti and N ₂ each, 0.00002 Cr and Mn each, 0.00001 Pb, Mg and Ag each, 0.00004 V and 0.00002 B by mass spectrographic analysis: from Metals Research Ltd.; polycrystalline; spectrographic analysis: from Metals Research Ltd.; polycrystalline; spectrographic analysis: from Metals Research Ltd.; polycrystalline; spectrographic analysis: from Ad and 10 cm 0.00004 V and 0.00002 B by mass spectrographic analysis: from Ad and Ag each, 0.00004 V and 0.00002 B by mass spectrographic analysis: from Metals Research Ltd.; polycrystalline; spectment 2 cm in diam and 20 cm long; unnealed in vacuum of 5 x 10 ⁻⁶ Torr at 1400 K for 2 h; slow cooled for measurements between 300 and 1250 K; machined to 1 cm in diam and 10 cm long, unannealed for measurements between 90 and 370 K; density 8.908 ± 0.001 g cm ⁻³ at 293 K; T _c about 630 K; residual resistivity ratio 220 ± 10; smoothed values from table. |
| * E5 | . 199 | Potter, H.H. | 1937 | > | 77-1153 | | 99.971 pure; 0.018 Fe and 0.010 C; obtained from Adam Hilger; specimen 2 mm in diam and 8 cm long, bent into U shape; resistance ratio R/R_{273} K reported; reference value of $\rho(273 \text{ K}) = 6.16 \times 10^{-6} \Omega \text{ m}$ assumed; T _C reported to be 629.3 or 629.8 K, depending on specimen. |
| 54* | 250 | Araj, S. | 1961 | > | 0-1000 | | Pure; 0.01 Fe and Cu each, and traces of C. Co, S, and Si; wire speci- men 1.5 mm in diam; enclosed in silica tubes evacuated to 10 ⁻⁵ mmHg; annealed for 68 h at 1400 K; quenched in saline solution at room tem- perature; original data reported graphically; extracted from the re- ported smooth curve. |
| \$ | 80 | Price, D.C. and Williams, G. | 1973 | ۲ | 4-300 | | 99.998 pure; specimen 0.15 x 0.2 x 10 cm; supplied by Johnson, Matthey and Co.; cold rolled between Melinex sheets, etched and annealed for 24 h in vacuo at 873 K; ideal resistivity reported graphically; total resistivity obtained by adding the reported residual resistivity $\rho(4.2 \text{ K}) = 0.0299 \times 10^{-6} \Omega \text{ m}$ to the reported ideal resistivity. |
| 9 2 | 158 | Mokrovskii, N.P. and Regel, A.R. | 1953 | ĸ | 1073-1964 | | 99.7 pure; specimen contained in corundum crucible v12 mm in diam and 25 mm high; smoothed values from graph. |
| 57 | 230 | Rowlands, J.A. | 1973 | ¥ | 1.7-672 | | Pure; from Sherritt Gordon Mines, annealed; ቦo = 0.28195 x 10 ⁻⁶ በ m; data in tabular form supplied by author. |

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* Not shown in figure.

| 31 Now, M.Y. 1964 - 993-3 (north start st | Pata Set a | Ref. | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---|---------------|------|---|------|----------------|------------------|-------------------------------------|---|
| 30 31 Wow, N.Y. 1960 - 99-1479 Explate to the above aperiame accept electrically beated in at at at 17.3 K for 53 min. 60 331 Boa, N.Y. 1966 - 910-1608 Statiate to the above aperiame accept electrically beated in at at at at 17.3 K for 53 min. 61 391 Boa, V. and Vagi, T. 1973 8 1123 K for 53 min. 910-1608 Statiate accept electrically beated in at at at. 113.4 K at at at. 62 323 Schnaffer, A.L., and Vagi, T. 1932 8 1230-1898 910-1608 | 85 | 251 | Vong, H.Y. | 1966 | Ť | 998-1381 | | 99.92 pure; wire specimen 0.081 cm in diam and 61 cm long; supplied by British Driver-Harris Co. Ltd.; electrically heated in air at 1173 K for 5 min, oxide formed had olive-gree color; measured in vacuum of about 2 x 10 ⁻⁶ Torr; data extracted from figure. |
| 60 33. Mong, N.Y. 196. - 910-108 Spailar to the above spectamen except electrically hereed in at or the standard regit. T. 197. R regilization standard regilization provide above spectament of the at or the standard regilization standard regilization regilization standard regilization standard regilization regilization standard regilization regi regilization regilization regi regilization regi regili | 59 | 251 | Wong, H.Y. | 1966 | + | 993-1479 | | Similar to the above specimen except electrically heated in air at 11/3 K for 15 min. |
| 80 Ono, Y. and Yagi, T. 1972 R 1728-1898 99.⁹ Pure: In liquid actes: contained in a 10 mm. Literation and tag a | 60 | 251 | Wong, H.Y. | 1966 | t | 970-1408 | | Similar to the above specimen except electrically heated in air at 1173 K for 25 min. |
| Schindler, A.I., 1956 Schindler, A.I., 1956 Latt, N.J., and Sauth, K.J., and Sauth, K. | 61 | 89 | Ono, Y. and Yagi, T. | 1972 | × | 1728-1898 | | 99.9 ⁺ pure; in liquid state; contained in a 10 mm I.D. recrystallized alumina crucible; density data of Saito et al. (Bull. Res. Inst. Min. Dress. Metall., Tohoku Univ., $\underline{25}$, 67, 109, 1969) used to calculate specimen volume; data given as the formula $\rho(10^{-8} \text{Rm}) = 0.0280 \text{T(C)} + 44.32.$ |
| 6.1* 136 Dewar, J. and 1893 B 70-469 Pure; prepared by Mr. Mond, nickel tubes formed by passing vapor of into a very films spittal on lattels tubes formed by passing vapor of into a very films. J.A. 7.1. 12.1. 11. 11. 11. 11. 11. 11. 11. 11 | 62* | 252 | Schindler, A.I., Smith, R.J., and Salkovitz, E.I. | 1956 | 6 2 | 6-292 | | 99.99 pure; material obtained from International Nickel Co.; specimen 2.0 mm in diam and 16.3 cm long; fabricated from spectrographic rod; vacuum annealed at 1073 K for 2 h then gradually cooled for 24 h. |
| 64.*253Dewar, J. and Flewing, J.A.1892B91-368Pure, carbonyl nickel; wire specimen had probable dimensions of 0.0076 cm in diam and 50 to 100 cm long; from Johnson, Matthey and Co.; measurement of resistance repeated several times, mean observed resistivity reported; data uncorrected for thermal expansion; data extracted from table.65a148Schwerer, F.C. and Cuddy, L.J.1970V4-940"High purity"; rod specimen 1.8 mm in diam; p(4.2 K) = 0.024 x 10^{-8} 3m; measurement made "quasi-statically" with temperature decreasing at 1 C min ⁻¹ .66234Kalinovich, D.F.1972657-1291"High purity"; rod specimen 1.8 mm in diam; p(4.2 K) = 0.024 x 10^{-8} 3m; measurement made "quasi-statically" with temperature decreasing at 1 C min ⁻¹ .66234Kalinovich, D.F.1972657-1291Pure; original data reported graphically.67236Kaui, S.N.1972657-1291Pure; original data reported graphically.68234Kovenskii, I.TSaolin, M.D.; and69236Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui, S.N.1974C6920Kaui scone supplied by author. | 63* | 138 | Dewar, J. and Fleming, J.A. | 1893 | œ | 76-469 | | Pure; prepared by Mr. Mond, nickel tubes formed by passing vapor of nickel carbonyl through heated glass tube, portion of nickel tube cut into a very fine spiral on lathe; resistance ratio reported; data uncorrected for thermal expansion; data extracted from table; $p(273 \text{ K}) = 12.323 \times 10^{-8} \Omega$ m, Matthiesen's value as given in Everett's "Physical Units" used to convert resistance ratio to resistivity; temperatures at 76.1, 191.3, and 229.6 K measured by platinum resistance thermometer. |
| 65* 148 Schwerer, F.C. and 1970 V 4-940 "High purity"; rod specimen 1.8 mm in diam; p(4.2 K) = 0.024 x 10⁻⁶ ?m; measurement made "quasi-statically" with temperature decreasing at 1 C min⁻¹. 66 254 Kalinovich, D.F., 1972 657-1291 Pure; original data reported graphically. 66 254 Kalinovich, D.F., 1972 657-1291 Pure; original data reported graphically. 67 256 Kaul, S.N. 1974 G 84-900 Values from table supplied by author. | 64* | 253 | Dewar, J. and Fleming, J.A. | 1892 | £ | 91-368 | | Fure, carbonyl nickel; wire specimen had probable dimensions of 0.0076 cm in diam and 50 to 100 cm iong; from Johnson, Matthey and Co.; measurement of resistance repeated several times, mean observed resistivity reported; data uncorrected for thermal expansion; data extracted from table. |
| 66 254 Kalinowich, D.F., 1972 657-1291 Pure; original data reported graphically. Kovenskii, I.I., Smolin, M.D., and Stateenko, V.M. 67 226 Kaul, S.N. 1974 G 84-900 Values from table supplied by author. | 65* | 148 | Schwerer, F.C. and Cuddy, L.J. | 1970 | > | 4-940 | | "High purity"; rod specimen 1.8 mm in diam; p(4.2 K) = 0.024 × 10 ⁻⁸ 3 m; measurement made "quasi-statically" with temperature decreasing at 1 C min ⁻¹ . |
| 67 226 Kaul, S.N. 1974 G 84-900 Values from table supplied by author. | 6 6 | 254 | Kalinovich, D.F., Kovenskii, I.I., Smolin, M.D., and Stataenko, V.M. | 1972 | | 657-1291 | | Pure; original data reported graphically. |
| | 67 | 226 | Kaul, S.N. | 1974 | 3 | 84-900 | | Values from table supplied by author. |

| d. 10. kurdi, 1.A. and J.32. A 4.5.35 Polycrystallate vice 0.03 ca in diam and 5 ca long; data free solid transition kurtices have solid solid | 8 % B | | Author (s) | Year | Method Used | Temp. Range, K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---|-------|-----|--|------|----------------|-------------------|-------------------------------------|---|
| Boulementa, LM, 1951 - 29,1736 Boulementa, LM, 1953 - 29,1246 Boulementa, LM, 1951 - 2, 29,126 Boulementa, LM, 1951 - 2, 29,126 Boulementa, LM, 1951 - 2, 29,126 Boulementa, LM, 1951 - 2, 29,129 Boulementa, LM, 1951 - 2, 29,130 Boulementa, LM, 1951 - 1, 295 Boulementa, LM, 1951 - 1, 200 Boulementa, LM, 1950 - 1, 200 Boulementa, LL, and 1950 - 1, 200 Boulementa, LL, and 1950 - 1, 200 Boulementa, LL, and 1950 - 1, 200 Boulementa, LL, and | 3 | 103 | Norak, J.A. and Blewitt, T.H. | 1972 | ¥ | 4.5,295 | | Polycrystalline; wire 0.025 cm in diam and 5 cm long; data from table |
| 70 23 Generative, LW. 1915 - 39.1736 Statist to the above except meanered by heating the vire alouty in versus. 71 23 Genere, W., and Shila, W., and Shila, Y., and Shila, Y., and Shila, W., and Shila, Y., and Shila, Y., and Shila, Y., and Shila, J., and Shila, Y., and Y., and Y., and Shila, Y., and | 69 | 255 | Borodovskala, L.N. and Lebedev, S.V. | 1955 | + | 293,1726 | | Wire specimen 0.015 cm in diam; measured by pulse heating of the wire with current density 6×10^{6} to 5×10^{6} Amp cm ⁻² ; voltage and current measured by pulse oscillogram. |
| 1 24 Concert, W. and Millian, W. 191 + 293 91.9 purer; Mond Michel; vacuum mached in Migh Frequency over; our- consistent Millian, W. 1961 A 293-1473 H=00 99.8 pure; electrolytic. 1 23 Valention, M.V. and Lonameter, M.V. and Lonameter, M.V. and 1961 A 293-1473 H=00 99.8 pure; electrolytic. 1 23 23 197 1.9-20 Mill "machine electrolytic." 1097 state of 5 % atm ⁻¹ , restat- tivity value calculated from restored of 23 % atm ⁻¹ ; restat- tivity value calculated from restored of 23 % atm ⁻¹ ; restat- tivity value calculated from restored of 23 % atm ⁻¹ ; restat- tivity value calculated from restored of 23 % atm ⁻¹ ; restat- tivity value calculated from restored at a rate of 5 % atm ⁻¹ . 1733 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 16 141 Miltahaw, Y. 1939 V 78-1133 % and coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 17 203 101 N 78-1133 % and coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not coded at a rate of 5 % atm ⁻¹ . 1033 % not code at a rate of 5 % atm ⁻¹ . | 20 | 255 | Borodovskala, L.N. and Lebedev, S.V. | 1955 | + | 293,1726 | | Similar to the above except measured by heating the wire slowly in vacuum. |
| 2 32 Verretion, N.Y. and biometry, N.Y. and biometry, N.Y. 39 39-14/3 9.0 9.8 pure: electrolytic. 3 31 Britch, A.C., et al. 196 1.9-20 M 11 "Pure", polycrystal in the form of far platers: from Johnson, Matchy buowle, D. 3 212 Britch, A.C., et al. 196 -1.2 M 1 "Britch, A.C., et al. 1967 -1.2 M 1 "Britch actor of far platers: from Johnson, Matchy buowle, D. 10(3) Factor. 10(4) Factor. 10(4) Factor. 10(4) Factor. 10(4) Factor 10(4) Factor. <t< td=""><td>11</td><td>256</td><td>Köster, W. and Gmöhling, W.</td><td>1951</td><td>÷</td><td>293</td><td></td><td>99.9 pure; Mond Nickel; vacuum melted in a high frequency oven; out- gassed; measured by compensation method.</td></t<> | 11 | 256 | Köster, W. and Gmöhling, W. | 1951 | ÷ | 293 | | 99.9 pure; Mond Nickel; vacuum melted in a high frequency oven; out- gassed; measured by compensation method. |
| 73 212 Burlich, A.C., Martin, 1967 1.9-20 M 111 "ure", polygystal in the form of flat platee; from Johnson, Matthe River, D., River, Riv | 72 | 257 | Vedernikov, M.V. and Kolomoets, N.Y. | 1961 | × | 295-1473 | 00-N | 99.8 pure; electrolytíc. |
| 74 212 Enritch, A.C., et al. 1967 4.2 Mt I Statiar to the above specimen except annealed at 1473 K and coded at a rate of 5 K min ⁻¹ . 75 212 Enritch, A.C., et al. 1967 4.2 Mt I A different specimen cut from the same stoch as the above; annealed at 1473 K and cooled at a rate of 5 K min ⁻¹ . 76 141 Shirakawa, Y. 1939 V 78-1123 0.02 F ₁ , 0.00 S, 0.00 S, 1, and 0.01 P and Mm each; electron 176. in the same stoch an diam and 3.95 can long. 76 141 Shirakawa, Y. 1939 V 78-1123 0.02 F ₁ , 0.00 S, 0.00 S, 1, and Mm each; electron 176. in the same stoch an diam and 3.95 can long. 77 203 Sudortsor, A.I. and 1956 A 1.2-4 Ntih specimen in the same stoch an in diam and 3.95 can long. 78 203 Sudortsor, A.I. and 1956 A 1.2-4 Ntich specimen in the same stoch and the sum exterest direction. 78 203 Sudortsor, A.I. and 1956 A 1.2-4 Ntich specimen in the same stoch and in the sa | 73 | 212 | Ehrlich, A.C., Huguenin, R., and Rivier, D. | 1967 | | 1.9-20 | III FN | "Fure", polycrystal in the form of flat plates; from Johnson, Matthey and Co.; annealed at 1273 K; cooled at a rate of 3 K min ⁻¹ ; resistivity value calculated from reported $\rho(293 \text{ K})/\rho(T)$ ratio; $\rho(293 \text{ K}) = 6.93 \times 10^{-6} \Omega \text{ m}$. |
| 7.3 212 Bnrlich, A.C., et al. 1967 4.2 Ni I A different specianen cut from the same stock as the above; anmealed at 1273 K and cooled at a rate of 5 K min ⁻¹ . 76 141 Shirahawa, Y. 1939 V 78–1123 0.02 Fe, 0.01 C, 0.003 S, 0.002 Si, and 0.001 P and the each; electronism constrained and cooled at a rate of 145 specianen in the seat-west direction shows and cool. 00606 cm in diam and 3.35 cm cooled at a rate of inclusi from the mean and cool colors. 71 203 Sudovteov, A.I. and 1956 A 1.2-4 Polycrystalline specianen in the form of this riboni from Hilgeri scannealed at 1123 K for 1 h in vacuum, with specianen dor collar measurement dor vib in seat-west direction. 71 203 Sudovteov, A.I. and 1956 A 1.2-4 Polycrystalline specianen in the form of this riboni from Hilgeri scannealed at 1123 K for 1 h in vacuum, with resistivity value calculation. 71 203 Sudovteov, A.I. and 1956 A 1.2-4 Polycrystalline specianen in the form of this riboni from Hilgeri scalculated to be 1.048 x 10 ⁻⁵ transtructures specianen descenter of the color in the measurement dor calculation with transitivity value calculation with resistivity value calculation with transitivity at 273 K taken to be 6.16 x 10 ⁻⁶ f. 703 Sementerko, I.E. A 14-20 The above specianen measured at hydrogen temperatures; specianen descenter in the castructed iffor to to fol (x 10 ⁻⁶ f.) traken to be 6.16 x 10 ⁻⁶ f.< | 14 | 212 | Ehrlich, A.C., et al. | 1967 | | 4.2 | I IN | Similar to the above specimen except annealed at 1473 K and coded at a rate of 5 K min ⁻¹ . |
| 76 141 Shirahawa, Y. 1939 V 78-1123 0.02 Fe, 0.01 C, 0.003 S, 0.002 Si, and 0.001 P and Mn each; electron in the east-vess in the ast-vess in the east-vess in the east-vest east-vest east-vest in the east-vest in the east-ves | 5 | 212 | Ehrlich, A.C., et al. | 1967 | | 4.2 | N1 I | A different specimen cut from the same stock as the above; annealed at 1273 K and cooled at a rate of 5 K min ⁻¹ . |
| Z03 Sudovtsov, A.I. and 1956 A 1.2-4 Peiyergatalline specimen in the form of this ribbon; from Hilger; Semeneako, E.E. Semeneako, E.E. R(4,2 K)/R(273 K) reported to be 1.0148 x 10⁻²; reeistivity value calculated from reported resistance ratio, with resistivity at 273 K taken to be 6.16 x 10⁻⁶ Ω m. R04 sover A.I. and 1962 A 14-20 The above specimen measured at hydrogen temperatures; specimen described at 99.94 pure; sealed in glass tube with helium gas; values calculated from reported from reported from reported in glass tube with helium gas; values (T)⁴ 2.38 × 10⁻⁶ Ω m. R04 sove, T.M. 1974 319-1042 99.99 pure; electrolytic; measured in a vacuum of ~10⁻⁶ mmlk. Peninov, R.I., and Indov, T.I., and Indov, A.I. | 76 | 141 | Shirakava, Y. | 1939 | > | 78-1123 | | 0.02 Fe, 0.01 C, 0.003 S, 0.002 Si, and 0.001 P and Mn each; electro- lytic nickel from Monson and Co.; 0.0608 cm in diam and 3.95 cm long; annealed at 1273 K for 1 h in vacuum, with specimen in the east-west direction; slowly cooled; lead wire of nickel soldered by pure silver reannealed at 1123 K for 1 h in vacuum; slow cooled; measurement done with specimen in the east-west direction. |
| 78 203 Sudovtsov, A.I. and 1962 A 14-20 The above specimen measured at hydrogen temperatures; specimen searched at 99.94 pure; sealed in glass tube with helium gas; values Semeneako, E.E. Galculated from reported R(T)/R(273 K) = 1.00986 x 10 ⁻² + 4.85 x 10 ⁻¹¹ T ⁵ ; with p(273 K) taken to be 6.16 x 10 ⁻⁶ Ωm. 2.88 x 10 ⁻⁶ T ² + 4.85 x 10 ⁻¹¹ T ⁵ ; with p(273 K) taken to be 6.16 x 10 ⁻⁶ Ωm. Muradov, T.I., and Instance American Substance Ame | " | 203 | Sudovtsov, A.I. and Semeneako, E.E. | 1956 | × | 1.2-4 | | Polycrystalline specimen in the form of this ribbon; from Hilger; $R(4.2 \text{ K})/R(273 \text{ K})$ reported to be 1.0148 x 10 ⁻² ; resistivity value calculated from reported resistance ratio, with resistivity at 273 K taken to be 6.16 x 10 ⁻⁸ Ω m. |
| 79* 258 Panakhov, T.M., 1974 339-1042 99.99 pure; electrolytic; measured in a vacuum of ∿10 ^{-*} maHg. Peninov, R.I., Muradov, T.I., and Ibragimov, A.I. | 78 | 203 | Sudovtsov, A.I. and Semeneako, E.E. | 1962 | < | 14-20 | | The above specimen measured at hydrogen temperatures; specimen described at 99.94 pure; sealed in glass tube with helium gas; values calculated from reported $R(T)/R(273 \text{ K}) = 1.00986 \times 10^{-2} + 2.88 \times 10^{-6} \Omega \text{ m}$. |
| | *6/ | 258 | Panakhov, T.M., Peninov, R.I., Muradov, T.I., and Ibragimov, A.I. | 1974 | | 339-1042 | | 99.99 pure; electrolytic; measured in a vacuum of ${\rm vl0^-}^{\circ}$ mmHg. |

والإنباط المتحد ماليفة فالمتعاقبة والأخراب فيعطهم ومعاملا متراجع والمستحد ومعالمه
| Re | Anthone (a) | Year | Nethod | Temp. | Name and Specimen | Composition (weight percent), Specifications and Remarks |
|---------|--|------|--------|------------|----------------------|---|
| 2 | | | Used | Kange, K | Designation | |
| 52 | 9 Tyagunov, C.V., Raum, B.A., shd Kushniv, M.N. | 1972 | æ | 1573, 1973 | | 99.98 pure. |
| 1 191 | 9 Holborn, L. | 1919 | | 80-672 | | Wire spectaten 0.5 mm in diam; resistivity values calculated from reported R(T)/R(273 K), with $p(273 \text{ K})$ taken to be 6.16 x 10 ⁻⁸ Ω m. |
| ē. | 8 Schimank, H. | 1914 | * | 20-273 | | Wire specimen 1-2 m long; from Hartmann and Braun; resistivity value calculated from reported R(T)/R(273 K), with $p(273 K)$ taken to be 6.16 x 10 ⁻⁶ Ω m. |
| 3 36 | 7 Güntherodt, H.J. and Künz1, H.U. | 1973 | υ | 1726 | | 99.998 pure; from Johnson, Matthey and Co.; in liquid state; tempera- ture = 1726 K assumed. |
| 6* 26 | 0 Busch, G., Güntherodt, H.J., Künzi, H.U., Meier, H.A., and Schlapbach, L. | 1970 | | 1726 | | No details reported. |
| 5 15 | 9 Baum, B.A., Tyagunov, C.V., Gel'd, P.V., and Khasin, C.A. | 1671 | æ | 1573,1873 | | 99.99 pure; zone refined; specimen contained in either an alumina or zirconia crucible; measured in an atmosphere of helium. |
| 6* 19 | Bubini, E., Esin, O.A., and Vatolin, N.A. | 1969 | | 1873 | | "High purity"; measured in purified helium. |
| *2 | k Sewarin, A.M. | 1962 | 22 | 1728-1900 | | Messured in an atmosphere of helium; rotating field apparatus calibrated against an iron specimen with resistivity value at welting taken from R.W. Powell, Philos. Mag. 44 , 772, 1953; resistivity value calculated from reported conductivity = (32.35 - 0.88 × 10 ⁻³ T(C)) × 10 ⁴ (ohm cm) ⁻¹ ; (this equation is apparently erroneous). |
| 8* 2(| il Schwerer, F.C. and Silcox, J. | 1968 | | 16.4-56.3 | | No details reported; $p(273 \text{ K})/p(4.2 \text{ K}) \sim 1400$; values of $p(T)-p(1.4 \text{ K})$ reported only. |
| 9 23 | 0 Ahmad, H.M. and Grieg, D. | 1974 | 4 | 10-873 | Pure N1(I) | "Spec-pure" nickel from Johnson, Matthey and Co.; 0.5 mm in diam and 10 cm long; annealed in vacuum at 1223 K for 24 h; TC = 631 K; data below 260 K supplied by author; values from table. |
| 5: 0 | 20 Ahmsd, H.M. and Crieg, D. | 1974 | × | 10-260 | Pure Ni([]) | Similar to the above; data supplied by author. |
| 1* 2 | 21 Zumsteg, F.C. and Parks, R.D. | 1970 | > | 623-650 | | 99.999 pure; 0.005 cm thick, 0.05 cm wide and 50 cm long; swaged; annealed 1-30 days in situ before measurement; sample mounted on fiberglass; resistivity values calculated from reported $R(T)/R(T_C)$ and $\rho(T_C)$ taken to be 28.70 x 10 ⁻⁸ Ω m. |

| (continued) |
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| N1 |
| NICKEL |
| õ |
| RESISTIVITY |
| ELECTRICAL |
| 3HL |
| NO |
| INFORMATION |
| MEASUREMENT |
| TABLE 11. |

| e Be | Ref. | , Author (a) | Var | Method | Temp. | Name and | |
|-------------|-----------|---|--------------|--------|-----------|-------------|---|
| X | ŝ | | | Used | Range, K | Designation | composition (weight percent), Specifications and Kemarks |
| 92 | 87 | Seydel, U. and Fucke, W. | 1977 | * | 508-2989 | | 99.99 pure; 0.0015 Fe, 0.0003 Cu, 0.0002 Si, 0.0001 Ag, Al and Ca each, and <0.0001 Cr, Mg, Mn, and Sn each (chemical analysis); measured by an exploding wire technique; measurement error 43 ; smoothed values from curve. |
| 66 | 92 110 | Güntherodt, H.J., Hauser, E., Künzi, H.U., and Müller, R. Müller, R. | 1975 1976 | + | 1723-1843 | | 99.999 pure, from Johnson, Matthey and Co.; measured with a potential method in which the sample material was enclosed in an alumina tube with four protrusions setting as current and potential contacts. |
| * 46 | 262 | Yao, Y.D., Arajs, S., and Anderson, E.E. | 1975 | × | 4-300 | | 0.0010 Fe, 0.0007 Al, 0.0005 Si, 0.0002 Ca, Cu, and Mg each, and <0.0001 <u>Ag</u> and Mn; from Johnson, Matthey and Co., R(4.2 K)/R(298 K) = 3.3 x 10 ³ . |
| 95* | 209 | Wycisk, W. and Feller-Kniepmeier, M. | 1976 | < | 295-1390 | | 99.999 pure, <0.0005 Si, 0.0003 Fe, <0.0001 Mg and Ag each, 0.00001 Co, and 0.00005 Ca, Cd, Cu and Pb each; 5 mm diam and 150 mm long rod from Gallard-Schlesinger Chemical Corp.; zone-refined 5 times in electron beam; rolled and drawn to 60 µm diam wire with diamond tools; electrolytically cleaned after each rolling and drawing with a 7X acetic acid and 23X perchloric acid solution; annealed 1/2 to 1 h at 573-673 K in a vacuum of <10 ⁷ Torr; flushed with helium; then slowly lowered over a liquid helium bath, with copper guard roof the eads of which are immersed in liquid helium; heated to 1073 K for 40 min; then 1273-1373 for 5 min and 1473 K for 1 min; potential leads knotted and sintered to wire specimen at the highest temperature; $p(4,2 K)$ reported to be 0.0027 x 10 [°] 0 m its a longitudinal magnetic field of 250 Ge; resistivity values calculated from reported R(50 K)/R(4.2 K) = 1923. |
| 8 | 209 | Wycisk, W. and Feller-Kniepmeler, M. | 1976 | × | 1.5-4.2 | | Similar to the above, except $R(296 K)/R(4.2 K) = 1845$; resistivity values calculated from reported $\Delta R/R(4.2 K)$; measured wire a current density of $v3.5 \times 10^{\circ}$ A cm ⁻² , and in a magnetic field of 250 Oe. |
| *19 | 209 | Wycisk, W. and Feller-Kniepmeler, M. | 1976 | ¥ | 4.2 | | Similar to the above, except measured without a longitudinal magnetic field, resistivity value calculated from reported R(296 K)/R(4.2 K), with $\rho(296 \text{ K}) = 5.191 \times 10^{-8} \Omega$ m from data set 96. |
| +86 | 209 | Wycisk, W. and Feller-Kniepmeier, M. | 1976 | ¥ | 4.2 | | Similar to the above, except single crystal 5 mm in diam and 10 cm long. |
| # 66 | 209 | Wycisk, W. and Feller-Kniepmeier, M. | 1976 | × | 4.2 | | Similar to the above, except measured in a longitudinal magnetic field of 250 0e. |
| 100 | 93 | Kita, Y., Ohguchi, S., and Morita, Z. | 1978 | | 1654-1882 | | 0.08 Co, 0.007 Fe, 0.005 Si, 0.0025 Cu, C. ³² Mg, 0.001 Al, and 0.0007 S; measured with a four probe method in which the electrodes are made of the same material as the specimen; measured in a vacuum of 10 ⁻¹ Torr; data points taken at temperatures in the sequence: 1770, 1788, 1796, 1814, 1840, 1857, 1869, 1882, 1867, 1852, 1836, 1817, 1799, 1791, 1767, 1748, 1711, 1692, 1772, and 1654 K; values corrected for |
| 1 | a hour | 1- (1 | | | | | thermal expansion; values from table supplied by authors. |

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* Not shown in figure.

| (10.1 (1) (1) (10.1. M) | F Set a | Ře. | Author (s) | Year | Method Used | Temp. Range,K | Name and Specimen Designation | Composition (weight percent), Specifications and Remarks |
|---|---------|-----|--|------|----------------|------------------|-------------------------------------|--|
| 10 ¹⁰ 11 11 ¹⁰ <th1<sup>10</th1<sup> | 101* | 66 | Kita, Y., Ohguchi, S., and Morita, Z. | 1978 | + | 1648-1872 | | Same as the above; a second melt; temperature sequence: 1755, 178 1798, 1818, 1838, 1856, 1872, 1855, 1836, 1821, 1805, 1793, 1769, 1756, 1740, 1693, 1667, and 1648 K. |
| 10 24 Jackawa, P.J. and Jold 393-673 99.999 pure (10 pm metallic fauorities); polycrystalline; anuadas: anuadas: fauodas: anuadas: fauodas: fauoda | 102* | 66 | Kita, Y., et al. | 1978 | t | 1720-1888 | | Same as the above; a third melt; temperature sequence: 1751, 1766 1782, 1800, 1811, 1826, 1844, 1865, 1888, 1873, 1857, 1841, 1823, 1808, 1795, 1781, 1765, 1741, and 1720 K. |
| 104* 30. Sperifs, 1:1, and Markin, A.Y. 1916 - 31-813 Phycrystallite spectroscopic nickel supplied by the National Neural Markin, A.Y. Remain, A.Y., Amail, A.Y., Manil, A.Y., Manil, S.Y., and 1910 A 4.2 0.003 C, 0.0007 G, 0.0001 H, 0.0003 H and Fe sech, 0.0002 SI sech matrix, A.Y., and 105* 210 Mylli, T. 1910 A 4.2 0.0018 C, 0.0007 G, 0.0001 H, 0.0003 H and Fe sech, 0.0002 SI sech matrix, A.Y., and 0.0001 H, with a sech matrix of the matrix of | 103 | 224 | Jackson, P.J. and Saunders, N.H. | 1968 | | 293-673 | | 99.999 pure (10 ppm metallic impurities); polycrystalline; anneale data from table supplied by N.H. Saunders. |
| 105*210Fujii. T.1970A4.20.0000 K, 0.0000 K, 0. | 104* | 263 | Sherif, I.I., Ibrahim, A.F., Chani Avad, A.A., Ammar, A.S., and Esmail, S.A. | 1976 | t | 373-873 | | Polycrystalline spectroscopic nickel supplied by the National Resc Center, Cairo; either dumbell-shaped specimen with long ends about 3 cm long and 0.9 cm in diam or wire specimen of gauge length 2.5 measured by a four probe method in an over flushed with inert gas. |
| 106*210Nulli, T.1970A4.20.0040 C, 0.0010 0, <0.0002 H, and 0.0001 N; metallic septementation reasoner and rate as a fraction to the forms of for 2 h at 1173 N; "hhat are reasoner earbon easily by volatization in vacuum vit reasoner earbon easily by volatization in vacuum vit reasoner earbon easily by volatization in vacuum vit reasoner earbon easily by volatization in vacuum vit reasone earbon easily by volatization in vacuum vit easone strated in vacuum vit a same to reasone earbon easily by volatization in vacuum vit easone strated in vacuum vit a same to reasone earbon easily by volatization in vacuum vit easone strated in vacuum vit i resistivity value calculated by the same method a grant of mile earbon vacuum va | 105* | 210 | Fujii. I. | 1970 | × | 4.2 | | 0.0050 C, 0.0007 O, 0.0004 H, 0.0003 N and Fe each, 0.0002 S1 and each, and <0.0001 Ag, Al, Ca and Cu each; supplied by Johnson, Mat and Co.; carbon impurities determined by vacuum fusion method, nitrogen and oxygen impurities determined by vacuum fusion method high purity silicon; metallic impurities determined by the supplie 5 mm in diam and 20 mm long; annealed at 1273 K for 1 h; grain siz reported to be 9 grams cm ² ; resistivity value calculated frcm reported p(295 K)/p(4.2 K) with p(295 K) taken to be 7.004 x 10 ⁻⁸ f) |
| 107* 210 Fujii, T. 1970 A 4.2 Similar to the above except containing 0.0020 C, <0.0002 0. <0.1 and trace amount of N and 3 pass zone-refined in vacuum at 1 mm grain size 3-5 grain cm². 106* 210 Fujii, T. 1970 A 4.2 Similar to the above except containing 0.0010 C, <0.0002 0 and amounts of hydrogen and nitrogen and 5 pass zone-refined in vac 1 mm min⁻¹; grain size 4 grain cm². 109* 210 Fujii, T. 1970 A 4.2 Similar to the above except containing 0.0010 C, <0.0002 0 and amounts of hydrogen and nitrogen and 5 pass zone-refined in vac 1 mm min⁻¹; grain size 4 grain cm². 109* 210 Fujii, T. 1970 A 4.2 Similar to the above except oxygen content is reduced to 0.0001 | 106 # | 210 | Pujii, T. | 1970 | < | 4.2 | | 0.0040 C, 0.0010 0, <0.0002 H, and 0.0001 N; metallic inpurities r determined; the above material after surface oxidation treatment t remove carbon in an air atmosphere for 2 h at 1173 K; "this treatment is aimed to remove carbon easily by volatization in vacuum, with a chemical reaction to the forms of CO or CO_2 from N10 in the process of molten containing excessive oxygen during zone meiting"; I pass of molten containing excessive oxygen during zone meiting"; I pass of molten to vacuum at 3 mm in ¹ ; 1.5 mm in diam and 50 mm lor made by diameter controlled operation in zone refining process; gaseous impurities determined by the methods given above; grain si 4 grains cm ⁻² ; resistivity value calculated by the same method as |
| 106* 210 Fujii, T. 1970 A 4.2 Similar to the above except containing 0.0010 C, <0.0002 0 and amounts of hydrogen and nitrogen and 5 pass zone-refined in vacciment in the amounts of hydrogen and nitrogen and 5 pass zone-refined in vacciment is reduced to 0.0001 1 mm min⁻¹; grain size 4 grain cm⁻². 109* 210 Fujii, T. 1970 A 4.2 Similar to the above except oxygen content is reduced to 0.0001 cm⁻¹; grain size 4 grain cm⁻¹; grain size 4 grain cm⁻². | 107* | 210 | Fujti, T. | 1970 | < | 4.2 | | Similar to the above except containing 0.0020 C, <0.0002 0, <0.000 and trace amount of N and 3 pass zone-refined in vacuum at 1 mm mi grain size $3-5$ grain cm ⁻² . |
| 109* 210 Fujii, T. 1970 A 4.2 Similar to the above except oxygen content is reduced to 0.0001 pass zone-refined in vacuum at 1 mm min ⁻¹ ; grain size 4 grain c | 106* | 210 | P ujii, T. | 1970 | ۲ | 4.2 | | Similar to the above except containing 0.0010 C, <0.0002 0 and tra amounts of hydrogen and nitrogen and 5 pass zone-refined in vacuum 1 mm min ⁻¹ ; grain size 4 grain cm ⁻² . |
| | #60] | 210 | Pujii, T. | 1970 | < | 4.2 | | Similar to the above except oxygen content is reduced to 0.0001 ; l pass zone-refined in vacuum at 1 mm min ⁻¹ ; grain size 4 grain cm ⁻² |

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| NICKEL |
| OF |
| RESISTIVITY |
| ELECTRICAL |
| THE |
| NO |
| DATA |
| EXPERIMENTAL |
| 12. |
| TABLE |

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[Temperature, T, K; Electrical Resistivity, $\rho,~10^{-8}~\Omega$ m]

| - | ٩ | 4 | ٩ | т | ٩ | Т | Φ | Т | PT−P₀ | H | ٩ |
|---------|--------------|------------|--------------|----------|------------|------------|-----------|----------|------------|----------|--------------|
| DATA | <u>ser 1</u> | DATA S | <u>ier 3</u> | DATA SET | f 4(cont.) | DATA SET 7 | (cont.)* | DATA SET | 10(cont.)* | DATA SET | 12(cont.) |
| 2.0 | 0.19 | 80 | 0.570 | 18.7 | 0.0592* | 240 | 5.2 | 1.965 | 0.000108 | 3.24 | 0.329 |
| 2.4 | 0.19 | 90 | 0.600 | 20.2 | 0.0606 | 245 | 5.3 | 2.537 | 0.000188 | 3.89 | 0.333 |
| 3.0 | 0.20 | 8 6 | 0.776 | 20.5 | 0.0613* | 260 | 6.1 | 2.560 | 0.000194 | 14.84 | 0.345 |
| 3.5 | 0.20 | 120 | 1.34 | 21.7 | 0.0631 | 279 | 6.7 | 3.056 | 0.000271 | 15.92 | 0.345* |
| 4.2 | 0.22 | 141 | 1.72 | 22.3 | 0.0629* | 298 | 7.6 | 3.131 | 0.000276 | 16.53 | 0.345 |
| 5.0 | 0.22 | 159 | 2.29 | 22.3 | 0.0636* | 321 | 8.4 | 3.552 | 0.000362 | 16.97 | 0.345* |
| 5.9 | 0.22 | 180 | 3.06 | 24.2 | 0.0661 | 329 | 8.8 | 3.587 | 0.000357 | 17.49 | 0.345* |
| 7.9 | 0.22 | 201 | 3.63 | 24.4 | 0.0667* | 363 | 10.4 | 3.974 | 0.000450 | 17.99 | 0.346 |
| 6.9 | 0.22 | 220 | 4.40 | 24.4 | 0.0692* | 411 | 12.7 | 3.993 | 0.000448 | 19.42 | 0.346* |
| 10.9 | 0.22 | 249 | 5.35 | 25.1 | 0.0684* | 475 | 16.6 | 13.79 | 0.00470 | 20.24 | 0.346 |
| 13.2 | 0.24 | 272 | 6.31 | 27.4 | 0.0733 | 493 | 17.5 | 14.64 | 0.00520 | | |
| 15.4 | 0.24 | 295 | 7.46 | 30.3 | 0.0793 | 508 | 18.8 | 15.54 | 0.00591 | DATA SI | ST 13 |
| 17.3 | 0.24 | 304 | 7.84 | 30.3 | 0.0807 | 528 | 20.3 | 16.42 | 0.00658 | | 1 |
| 18.5 | 0.24 | 375 | 11.29 | 32.6 | 0.0884 | 548 | 21.8 | 16.62 | 0.00691 | 373 | 11.9 |
| 21.1 | 0.24 | 429 | 13.97 | 35.2 | 0.0973 | 565 | 23.2 | 17.09 | 0.00711 | 473 | 18.3 |
| 22.8 | 0.26 | 458 | 15.88 | 4.6).8 | 0.1222 | 574 | 23.9 | 17.53 | 0.00749 | 573 | 25.2 |
| 24.8 | 0.26 | 480 | 17.03 | | | 579 | 24.2 | 17.93 | 0.00784 | 673 | 32.5 |
| 26.9 | 0.29 | 542 | 22.01 | DATA S | ET 5 | 585 | 24.8 | 18.44 | 0.00832 | 773 | 47.5* |
| 29.4 | 0.29 | 556 | 23.92 | | | 591 | 25.3 | 19.04 | 0.00887 | | |
| 31.4 | 0.29 | 585 | 26.98 | 323.2 | 8.65 | 597 | 25.9 | 19.77 | 0.00961 | DATA SI | ST 14 |
| 33.0 | 0.29 | 616 | 30.62 | 423.2 | 13.6 | 602 | 26.6 | 19.77 | 0.00965 | | |
| 35.0 | 0.29 | 648 | 32.72 | 523.2 | 20.3 | 610 | 27.3 | | | 273 | 6.36 |
| 36.6 | 0.29 | 693.177 | 33.876 | 623.2 | 28.8 | 614 | 27.7 | | | 293 | 7.01 |
| 39.3 | 0.29 | 734 | 35.024 | | | 628 | 29.4 | | | 300 | 7.31 |
| 41.9 | 0.33 | | | DATA S | ET 6 | 634 | 30.0 | - | đ | 400 | 11.65 |
| 44.7 | 0.40 | DATA | SET 4 | | | 643 | 30.6 | | | 500 | 17.6 |
| 47.0 | 0.40 | | | 90 | 1.77 | | | DATA S | ET 11 | 550 | 21.1 |
| 48.7 | 0.42 | 5.6 | 0.0523 | 194.7 | 4.59 | DATA | SET 8* | | | 600 | 25.25 |
| 50.7 | 0.44 | 6.0 | 0.0523 | 273 | 7.37 | | | 4.2 | 0.0095 | 627 | 28.15 |
| 53.9 | 0.44 | 7.5 | 0.0526 | 373 | 11.56 | 4.2 | 0.034 | 10 | 0.0115 | 650 | 29.9 |
| 56.6 | 0.51 | 8.1 | 0.0529 | | | | | 20 | 0.0195 | 700 | 32.0 |
| 59.2 | 0.51 | 10.2 | 0.0533 | DATA SE | */ L | DATA | SET 9 | 30 | 0.0385 | 800 | 35.45 |
| 62.8 | 0.54 | 10.2 | 0.0535* | | | | | 40 | 0.0775 | 006 | 38.5 |
| 65.3 | 0.57 | 11.8 | 0.0544 | 74 | 0.4 | 4.2 | 1.18 | 20 | 0.1495 | 1000 | 41.25 |
| 67.3 | 0.58 | 12.1 | 0.0544* | 84 | 0.6 | | | 60 | 0.2295 | 1100 | 43.8 |
| 69.9 | 0.62 | 13.5 | 0.0551 | 92 | 0.8 | | | 70 | 0.3695 | 1200 | 46.4 |
| 73.1 | 0.69 | 13.6 | 0.0555* | 101 | 1.0 | e | | 80 | 0.5495 | 1300 | 48.75 |
| | | 14.2 | 0.0555* | 118 | 1.3 | 1 | 0 d-Ld | 90 | 0.7495 | 1400 | 50.95 |
| DATA SI | 12 | 14.5 | 0.0564 | 125 | 1.6 | | | 273 | 6.31 | 1550 | 54.25 |
| | | 15.1 | 0.0564* | 145 | 2.4 | DATA | SET 10* | | | | |
| 293.2 | 6.8 | 16.3 | 0.0569* | 173 | 3.0 | | | DATA S | ET 12 | DATA SI | <u>17 15</u> |
| 413.2 | 16.0 | 16.3 | 0.0572 | 197 | 3.6 | 1.612 | 0.0000777 | , | | | |
| | | 17.2 | 0.0585* | 205 | 4.0 | 1.736 | 0.0000852 | 1.73 | 0.329 | 300 | 8.77 |
| | | 10.7 | 0.0386 | 262 | 4.9 | 1.924 | 0.000105 | 2.50 | 0.329 | 327 | 10.42 |

* Not shown in figure.

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TABLE 12. EXPERIMENTAL DATA IN THE ELECTRICAL RESISTIVITY OF NICKEL NI (continued)

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| μ | p | 1 | D | Ţ | d | T | d | 1 | d | L | d |
|----------------|-----------------|--------|---------|--------|--------|------------|----------|---------|---------|----------|-----------|
| DATA SET | 15(cont.) | DATA S | SET 19 | DATA S | ET 25* | DATA SET 2 | 7(cont.) | DATA SI | 2T 30 | DATA SET | 34(cont.) |
| | | | | | | | | | | | |
| 576 | 12.55 | 293 | 10.1 | 293 | 7.90 | 579 | 24.2 | 384 | 11.9 | 5.5 | 0.0322 |
| 452 | 16.81 | 323 | 11.3 | 323 | 9.30 | 631 | 29.3 | . 438 | 15.0 | 6.1 | 0.0323 |
| 519 | 21.10 | 423 | 16.3 | 373 | 11.50 | 647 | 29.1 | 493 | 18.0 | 6.9 | 0.032 |
| 558 | 24.39 | 523 | 22.8 | 423 | 14.16 | 555 | 35.3 | 551 | 22.6 | 7.7 | 0.0328 |
| 89 95 | 25.13 | 623 | 31.5 | 473 | 17.24 | 794 | 36.4 | 615 | 27.7 | 8.5 | 0.033 |
| 630 | 30.49 | | | 498 | 18.71 | 864 | 38.8 | 680 | 32.7 | 9.5 | 0.0335 |
| 680 | 33.00 | DATA S | SET 20 | 523 | 20.70 | 666 | 42.3 | | | 10.4 | 0.0338 |
| 683 | 00.66 | | | 548 | 22.50 | 1053 | 44.4 | DATA | SET 31 | 10.8 | 0.0342 |
| 766 | 35.46 | 293 | 7.1 | 573 | 24.70 | 1124 | 45.9 | | | 14.7 | 0.0363 |
| 803 | 36.76 | 323 | 8.3 | 598 | 27.19 | 1172 | 46.1 | 2.32 | 0.00329 | 17.9 | 0.0391 |
| 803 | 36.50 | 423 | 13.1 | 623 | 28.88 | | | 2.97 | 0.00339 | 105.6 | 1.15 |
| 86 | 39.06 | 523 | 19.4 | 648 | 30.51 | DATA SI | 5T 28 | 3.24 | 0.00346 | 115.1 | 1.36 |
| 5 5 5 5 | 40.49 | 623 | 28.3 | 673 | 31.84 | | | 3.83 | 0.00366 | 123.8 | 1.60* |
| 1016 | 43.10 | 723 | 33.2 | 698 | 32.69 | 1152 | 50.3 | 4.36 | 0.00377 | 134.1 | 1.87 |
| 1018 | 43.10 | 823 | 36.4 | 723 | 33.63 | 1178 | 51.1 | 5.72 | 0.00417 | 179.1 | 3.17 |
| | | 923 | 39.2 | 748 | 34.57 | 1209 | 51.6 | 7.31 | 0.00476 | 199.5 | 3.78 |
| DATA | iet 16 | 1023 | 42.1 | 173 | 35.36 | 1236 | 51.5 | 9.12 | 0.00553 | 226.6 | 4.62 |
| l | 1 | 1123 | 44.7 | | | 1277 | 53.7 | 13.1 | 0.00780 | 252.2 | 5.41 |
| 1098 | 43.8 | 1223 | 47.5 | DATA S | ET 26* | 1305 | 54.6 | 14.1 | 0.00859 | | |
| 1104 | 43.9 | 1323 | 49.8 | | | 1320 | 55.7 | | | DATA SE | T 35 |
| 1115 | 44.2 | | | 293 | 8.08 | | | DATA S | ET 32 | | |
| 1124 | 44.6 | DATA S | SET 21 | 323 | 9.36 | DATA S. | ET 29 | | | 1163 | 48.1 |
| 1174 | 45.8 | | | 373 | 11.60 | | } | 293 | 6.8* | 1217 | 50.7 |
| 1183 | 46.0 | 298 | 7.50* | 423 | 14.11 | 110 | 2.0 | 1073 | 44 | 1300 | 53.7 |
| 1235 | 47.0 | 1726 | 60 | 473 | 17.29 | 138 | 2.7 | 1273 | 67 | 1400 | 57.1 |
| 1241 | 47.1 | 1726 | 84 | 498 | 18.70 | 147 | 3.5 | | | 1454 | 59.2 |
| | | | | 523 | 20.54 | 164 | 3.5 | DATA | SET 33 | 1502 | 60.7 |
| DATA S | ET 17 | DATA S | ET 22 | 548 | 22.51 | 194 | 4.6 | | | 1560 | 61.8 |
| 1 | | | | 573 | 24.74 | 203 | 4.8 | 4.2 | 0.022 | 1606 | 63.1 |
| 293 | 7.1 | 4.18 | 0.11 | 598 | 26.91 | 225 | 5.5 | 10.5 | 0.024 | 1641 | 63.7 |
| 323 | 8.3 | 80.5 | 0.676 | 623 | 29.18 | 256 | 6.6 | 11.8 | 0.025 | | |
| 423 | 13.0 | 292 | 7.16 | 648 | 30.75 | 265 | 6.9 | 13.4 | 0.026 | DATA SE | T 36 |
| 523 | 19.4 | | | 673 | 32.01 | 327 | 9.7 | 15.3 | 0.027 | | |
| 623 | 28.0 | DATA | SET 23* | 869 | 32.70 | 363 | 10.8 | 16.8 | 0.029 | 891.2 | 39.1 |
| 723 | 32.8 | | | 723 | 33.23 | 395 | 13.0 | 18.6 | 0.030 | 947.2 | 43.0 |
| 823 | 36.1 | 4.18 | 0.0213 | 748 | 33.98 | 399 | 12.7 | 177.0 | 3.06 | 983.2 | 43.0 |
| 923 | 39.3 | 80.5 | 0.60 | | | 405 | 13.1 | 188.3 | 3.41 | 1077.2 | 47.8 |
| 1023 | 42.4 | 273 | 6.35 | DATA S | ET 27 | 438 | 14.5 | 204.3 | 3.87 | 1174.2 | 52.3 |
| 1123 | 45.2 | 298 | 6.48 | | | 469 | 17.1 | 233.4 | 4.79 | 1273.2 | 54.0 |
| | | | | 313 | 8.3 | 479 | 17.4 | 272.2 | 6.17 | 1378.2 | 57.1 |
| DATA | SET 18 | DATA S | SET 24 | 364 | 10.9 | 517 | 20.0 | 295.0 | 7.06 | 1475.2 | 61.2 |
| | | | | 373 | 11.5 | 554 | 22.2 | 298.1 | 7.24 | 1574.2 | 64.1 |
| 373 | 10.6 | 4.2 | 0.37 | 411 | 13.0 | 559 | 22.8 | | | 1673.2 | 68.1 |
| 533 | 18.5 | 90 | 0.92 | 483 | 17.2 | 637 | 29.7 | DATA | SET 34 | | |
| 263 | 20.7 | 198 | 4.12 | 505 | 18.7 | 683 | 32.3 | | | DATA SI | T 37 |
| 773 | 33.2 | 273 | 7.46* | 535 | 20.7 | 721 | 33.4 | 4.2 | 0.0319 | | |
| | | | | | | 803 | 36.8 | 5.0 | 0.0321 | 73 | 0.6 |
| * Not si | hown in figure. | | | | | | | | | | |

| Ni (continued) |
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| OF NICKEL |
| RESISTIVITY |
| ELECTRICAL |
| N THE |
| DATA O |
| EXPERIMENTAL |
| TABLE 12. |

| F | ٩ | ч | ٩ | Т | ٩ | T | σ | ł | PT-Po | 1 | ٩ |
|-------------|------------|-----------------|--------------|------------|-----------------|---------------|---------|----------|--------------|------------|--------------------|
| DATA SET | 37(cont.) | DATA SET 3 | 8(cont.)* | DATA SET 3 | 9(cont.)* | DATA | SET 43 | DATA SET | . 48(cont.)* | DATA SET | 1(cont.)* |
| 123 | 1.6 | 355.2 | 10.3 | 496 | 16.8 | 4.2 | 0.0347 | 1.67 | 0.00057 | 650 | 29.57 |
| 5 | 3.0 | 362.2 | 10.9 | 541 | 19.9 | 13.6 | 0.0391 | 7.96 | 0.00066 | 658 616 | 29.43 |
| (77 (12) | 1.6 | 0/C 77F | 12.0 | 900 | 22.0 | 7-0T | 0.0402 | 10.5 | 0.00173 | C/0 | 30.05 |
| 323 | 8.0 | 388.5 | 12.7 | 613 | 26.3 | 24.3 | 0.0510 | 18.7 | 0.00512 | 002 | 31.84 |
| 676 | 10.1 | 395.9 | 13.0 | 636 | 28.3 | 28.0 | 0.0587 | 20.8 | 0.00682 | 716 | 32.04 |
| 423 | 12.4 | 432.9 | 15.4 | 665 | 29.5 | 33.7 | 0.0787 | 24.0 | 0.0103 | 721 | 32.67 |
| 673 | 15.0 | 484.7 | 18.7 | 701 | 30.9 | 38.9 | 0.101 | 41.5 | 0.0638 | 744 | 32.96 |
| 523 | 17.7 | 499.5 | 19.4 | 762 | 34.1 | 57.8 | 0.235 | 49.7 | 0.1128 | 768 | 34.19 |
| 573 | 21.5 | 543.9 | 23.0 | 822 | 36.4 | 67.3 | 0.325 | 79.3 | 0.6032 | 111 | 33.62 |
| 623 | 25.2 | 543.9 | 23.6 | | | 79.3 | 0.491 | | | 791 | 34.80 |
| 673 | 29.1 | 584.6 | 26.6 | IVO | V SET 40 | 93.3 | 0.778 | | | 825 | 35.57 |
| 123 | 31.2 | 584.6 | 21.9 | | | 111 | 1.29 | T | đ | | |
| 611 | 33.1 | 592.0 | 28.6 | 3.2 | 0.0104 | 136 | 1.76 | | | DATA | SET 52 |
| (70 | 24.95 | 7.410 2.41 7 | 1 00 | DATA C | 18r 614 | 1/1 | 0C.7 | DATA SE | T 49 | 00 | +676 0 |
| C/0 | 0.UC | 7.100 | 1.00 | VIVO | 11 11 | 196 | 47.C | | | 2 | -70/ 0 |
| 626 | 0.0C | 0.000 |).10 2 10 | ă | 701 C | 077 | 4.17 | 1013 | 54.6 | | 1.5054 |
| 676 | 2.2 | 006.4 | 32.0 | 47 G | 001.2 | 067 | 70.0 | 1456 | 61.3 | C71 | 1.385 [#] |
| 1023 | C. 65 | /14.1 | 9.55 | 86 | 2./03 | 2 062 | /.14 | 1647 | 64.3 | 150 | 2.237* |
| 10/3 | 40./ | 1.16/ | 94.9 | [7] | 3./48 | 293.2 | 1.22 | 1713 | 81.3 | 200 | 3.703 |
| 1123 | 41.9 | 780.70 | 36.2 | 148 | 4.866 | | | 1760 | 87.7 | 250 | 5.384 |
| 1173 | 43.2 | 821.4 | 37.1 | 173 | 6.049 | DATA S. | ET 44 | 1997 | 92.3 | 300 | 7.237* |
| 1223 | 44.4 | 851.0 | 38.1 | 198 | 7.352 | | | | | 400 | 11.814 |
| 1273 | 45.8 | 895.4 | 39.2 | 223 | 8.825 | 303.2 | 8.58 | DATA SE | T 50* | 200 | 17.704 |
| 1323 | A . 04 | 9.32.4 | 40.4 | 847 | /07.01 | | | | ł | 600 | 22.24 |
| 6/61 | 48.4 | 962.0 | 41.4 | 273 | 12.005 | DATA S | SET 45 | 811 | 7.8 | 630 | 28.862* |
| 1423 | 49.3 | 1036.0 | 43.1 | 298 | 13.808 | | | | 2 | 635 | 29.288* |
| 1473 | So. 3 | 1061.9 | 43.6 | 323 | 15.723 | 80 | 1.109 | DATA S | ET 51* | 650 | 30.142 |
| 1523 | 51.4 | 1113.7 | 44.7 | 348 | 17.946 | 273 | 7.663 | | | 8 | 32.237 |
| 1573 | 52.8 | 1154.4 | 45.2 | 373 | 20.207 | | | 375 | 10.05 | 800 | 35.637 |
| 1623 | 53.9 | 1176.6 | 46.1 | 398 | 22.514 | DATA St | 5T 46 | 388 | 11.08 | 006 | 38.676 |
| 1008 | 74.4 | 1209.9 | 40.0 | 423 | 25.025 | | | 419 | 13.12 | 1000 | 41.496 |
| | 400 * | 7.0#21 | 41.4 | 011 | 000.12 | 7.667 | ۰.۷ | 424 | 12.20 | 0011 | 007.44 |
| TO VIVA | | | | 6/4 | 30.404 | | : | 475 | 15.50 | 0071 | 40.128 |
| 10 | 3 0 | DATA SI | - 19- | 979 | 13.33/ | ATAU | SET 4/ | 489 | 17.23 | 0621 | 41.912 |
| 170 5 | | 11 | | 670 | 200,0C | c 7 | 775 0 | 515 | 19.09 | | ET 530 |
| 169.1 | | 711 | | | 17.400 | 7.4 | | 520 | 18.06 | NIN | EL JJ |
| | | #CT | 0.1 | 5/5 | 47.127 | | | 548 | 21.56 | ł | |
| 102.8 | 7.4 | ROZ | 9. 5 | 598 | 46.243 | | | 560 | 21.39 | 11 | 0.554 |
| 185 | 0.0 0 | 240 | 5.0 | 623 | 49.722 | F | 01-D0 | 575 | 23.69 | 8 | 0.770 |
| 196.1 | 0.4 | 274 | 6.2 | 648 | 53.390 | | | 597 | 24.40 | 169 | 2.71 |
| 214.0 | 4 (2 (| 298 | 1.2 | 673 | 57.257 | DATA | SET 48* | 600 | 26.27 | 273 | 6.16 |
| 1.62 | 2.2 | 330 | 4.8 | DATA | SET 42 | | 25 120 | 625 | 27.50 | 373 | 10.35 |
| 281.2 | | 375 | 10.3 | | 100 | 4 17 | 0.00017 | 019 | 28.39 | 435 | 13.52 |
| 336.7 | 9.5 | 164 | 13.1 | 1.5 | 0.1044 | 5.86 | 0.00035 | 618 | 28.71 | 483.5 | 16.50 |
| 340.4 | 9.8 | 469 | 15.1 | 293.2 | 10.44 | >> • • • • | | , , | 4 | 526 | 19.40 |
| | | | | | | | | | | | |

* Not shown in figure.

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TABLE 12. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF NICKEL N1 (continued)

1.900 6.110 7.470 12.350 13.494 18.913 0.024 1.0 7.3 7.3 7.3 7.3 7.3 7.3 11.9 11.9 25.6 25.6 25.6 38.8 38.8 38.0 38.0 1.908 7.242 9.456 9.456 112.323 112.402 114.653 114.653 114.653 114.653 114.653 114.653 114.653 23.730 23.730 -0.08 0.41 6.13 6.84 65# 35.2 \$63 *79 62* a 66 SET SET SET SET SET DATA DATA DATA DATA 76.1 191.3 229.6 274.30 274.30 363.50 468.5 DATA 4.2 100 200 200 500 500 500 500 500 500 800 800 800 91 173 193 274.4 293 367.7 65 77 272 292 657 568 Ś E 85.06 87.08 89.12 89.82 40.6 41.6 41.6 41.6 44.9 44.9 550.8 550.8 551.7 555.7 551.7 555.7 39.8 ٩ 5 60 ŝ SET SET SET DATA DATA DATA 970 1001 1021 1021 1042 1062 1162 1164 1164 11178 11267 11267 11267 11267 11267 11267 11360 11385 1408 993 1020 1020 1042 1083 11083 11168 11168 11168 11168 11168 11204 1239 12395 11305 11305 11305 11305 11305 11305 11305 11281 11606 11706 11606 11706 1 1728 1800 1873 1873 H 57 (cont.) 0.3122 8 SET DATA SET 27.85 37 39 43 60 60 70 70 70 70 70 70 53 84 64 55 519 558 646 628 646 646 672 672 DATA 998 1016 1040 1059 11077 11077 11178 11178 11177 11195 11195 11294 11294 11294 11294 11339 11339 11339 11339 1.052 1.177* 1.177* 1.1868 1.18566 1.18566 1.18566 1.18566 3.3394 4.1659 3.300 3.300 4.1658 5.094* 5.094* 5.094* 7.366* 7.346 7.346 7.346 7.346 0.2820 0.2821 0.2826 0.2837 0.2837 0.2837 0.2837 0.2872 0.2872 0.2913 0.2913 0.2913 DATA SET 55(cont. SET 57 a 48.1 55.6 55.2 55.2 57.8 57.8 60.3 62.7 83.5 83.5 83.5 84.5 85.6 86.1 56 SET DATA 1.74 6.6 8.0 9.2 12 16.6 19.1 22.3 100.2 105.7 113.5 113.5 113.4 113.4 154.2 154.2 154.2 154.2 154.2 182.0 191.4 191.4 191.4 255.4 255.4 255.4 255.4 255.4 300.0 3.0 DATA 1073 1173 1173 11773 11673 11673 11728 11728 11728 11728 11728 11728 11728 11728 11728 11728 11728 11728 11728 11728 11778 11778 11778 11778 11778 11779 11773 11775 11775 11775 11775 11775 11775 11775 11775 11775 11775 117 0.0299 0.0306 0.0310# 0.0311# 0.03114 0.0315 0.0316 0.0316 0.0316 0.0336 0.0336 0.0336 0.0336 0.03374 0.03374 0.03374 0.03374 0.03374 0.03376 0.033777 0.03557 0.005537 0.005537 0.005537 0.005537 0.005537 0.007556 0.007556 0.007556 0.007556 0.007556 0.007556 0.007557 0.007556 00 0.2310 0.3127 0.4036 0.5157 .6601* 0.5813* 0.7338 0.8178 0.9367 54(cont.)* **SET 55** 27.0 30.8 33.4 36.8 40.1 43.3 DATA DATA SET н DATA SET 53(cont.)* 43.51 44.75 1.1 4.0 8.0 12.7 18.7 a 54* SET 641.1 642.3 642.3 651.8 653.8 653.8 7734.8 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 785.0 1004.0 1016.0 11128.2 11128.2 11128.2 628.6 628.9 629.2 629.4 630.5 631.1 633.4 633.4 621.5 626.9 635.2 637.1 638.7 \$51.5 617.5 627.8 DATA 88888

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| | | | | | | | والمعادية والمتلافة فتتركر والمتركم والمتركب | | | | |
|------------|------------------|------------|----------------|-------------------------|--------------|-------------|--|------------|----------------------|----------|----------|
| ۲ | ٩ | H | ٩ | н | ٥ | н | ٩ | H | ٩ | T | a |
| DATA SET | 66(cont.) | DATA SET | 67(cont.) | DATA S | ET 69 | DATA SET | 6(cont.) | DATA SET | r 78(cont.) | DATA SET | 1 84* |
| 673 | 35.2* | 160 | 2.50* | 293 | 8,5* | 373 | 11.35 | 18 | 0.0669 | 1726 | 85.1 |
| 683 | 36.0 | 180 | 3.10 | 1726 | 63 | 482 | 17.1* | 20 | 0.0673 | | |
| 969 | 37.1* | 200 | 3.70* | i | | 562 | 21.9 | | 105 | DATA SE | 1 85 |
| 104 | 37.4 | 220 | 4.38 | DATA SI | <u>17 70</u> | 596 | 22.6 | DATA SE | - / / / / | 1673 | 7 03 |
| 11 | 37.6* | 240 | 5.10 | | | 621 | 27.3 | 000 | | 1075 | 0.00 |
| <u> </u> | 38.2 | 260 | 5.95 435 2 | 97/1 | 04 0 | 523 | 4.82 20.14 | 255 195 | C.4 | C/01 | 07.4 |
| 747 | 38.)# 26. 64 | 790 | 5, /J# | 1/20 | c.18 | 740 | 29.1 " | 105 | 14.2 | DATA SFT | 86* |
| 64) 764 | 20.92 | | *05 X | DATA | KET 21 | 409 9999 | 11.7* | 203 | 18.3 | 170 0100 | 8 |
| 166 | 40.04 | 340 | 9.45 | UTUA | | 680 | 31.8 | 536 | 21.5 | 1873 | 125 |
| 22 | 39,5# | 360 | 10.35* | 293 | 7.61 | 702 | 32.7 | 583 | 24.0 | | |
| 787 | 39.5* | 380 | 11.35* | | | 772 | 34.9 | 618 | 27.8 | DATA SE | T 87* |
| 795 | 40.2 | 400 | 12.40 | DATA S | ET 72 | 873 | 38.6 | 662 | 29.2 | | |
| 806 | 40.4* | 420 | 13.50 | | | 996 | 41.2 | 695 | 30.9 | 1728 | 3.24 |
| 817 | 41.6* | 440 | 14.65 | 295 | 8.4 | 1073 | 44.1 | 731 | 32.0 | 1800 | 3.25 |
| 855 | 43.0 | 460 | 15.90 | 432 | 16.0 | 1123 | 45.5 | 776 | 33.4 | 1900 | 3.26 |
| 861 | 43.3* | 480 | 17.15* | 568 | 25.7 | | | 865 | 36.7 | | |
| 873 | 43.5* | 200 | 18.50 | 969 | 35.8 | DATA | SET 77 | 928 | 39.0 | | |
| 902 | 44.5 | 520 | 20.25* | 725 | 36.8 | | | 666 | 40.4 | ч | PT-P1.4K |
| 945 | 45.2 | 540 | 22.00* | 881 | 42.2 | 1.23 | 0.0628 | 1042 | 42.0 | | |
| 952 | 45.4* | 560 | 24.10 | 1063 | 47.7 | 1.23 | 0.0629* | | | DATA | SET 88* |
| 962 | 45.6* | 580 | 26.30* | 1273 | 54.3 | 1.30 | 0.0628* | DATA SET | 80 | | |
| 166 | 47.5 | 009 | 28.75 | 1473 | 0.80 | 1.40 | 0.0629 | | ţ | 16.4 | 0.00521 |
| 1019 | 47.5# | 620 | 31.25 | 1 | | 1.28 | 1.0629F | 5/01 | 22 | 19.5 | 0.00801 |
| 1036 | 48 0 * | 640 | 32.75 | TAG | A SET 73 | 1.62 | 0.0629# | 6/61 | 8/ | 23.5 | 0.0123 |
| 1078 | 49.1 | 660 | 33.25 | | | 1.73 | 0.0629 | | | 28.3 | 0.0214 |
| 1089 | 49.4# | 680 | 33.75 | 1.85 | 0.00308 | 2.01 | 0.0629* | DATA | SET 81 | 32.7 | 0.0325 |
| 1127 | 51.0 | 700 | 34.25 | 4.15 | 0.00346 | 2.20 | 0.0629 | 1 | | 37.4 | 0.0497 |
| 1141 | 51.4* | 720 | 34.75 | 14.1 | 0.00753 | 2.41 | 0.0629* | 80.2 | 0166.0 | 41.6 | 0.0720 |
| 1165 | 51.3 | 740 | 35.25 | 20.1 | 0.01237 | 2.52 | 0.0629* | 80.9 | 0.9666 | 46.3 | 0.102 |
| 1173 | 52.04 | 760 | 35.75 | | | 2.73 | 0.0630 | 1.94./ | 4.0486 | 51.8 | 0.147 |
| 1187 | 52.6* | 780 | 36.25 | ITAD | V SET 74 | 3.00 | 0.0630 | 3/3 | 7601.4 | 56.3 | 0.192 |
| 1200 | 8-25 | 008 | 36.75 | | 2010 0 | 3.18 | 0.0630 | + 10C | 0CU/.CT | | |
| 1121 | 5.50 | 820 | 57.75 27.75 | cl. ⁴ | 0.040/ | | 0.0630 | 0.1.0 | 70//07 | | |
| 7771 | | 040 | c | | | 70.0 | 0.000 | | 400 400 | ų | đ |
| 0/21 | | 998 098 | 38.25 | ING | C/ 13S A | () · · | 0.0630 | DAIA | 221 07* | | |
| 12/3 | | 098 0 | 20.00 | | | 40.0 0 | -TCON-0 | | 2020 1 | ATAN | 6T 00 |
| 1921 | | 86 | CZ. 60 | 4.10 | 1410.0 | 18.5 | 0.0031 | 20.2 | 07/7.1 | DALA | DE1 07 |
| 1671 | 7.00 | | 40, muu | | 76 83 | 40°7 | 0.0031 | 80.4 | 1.005 | 01 | 770 0 |
| | ., | VIVO | SET 08" | NATA | 11 | 5.4.5 | 0.0631 | 4.CY1 | 1101.4 | 07 | 0.044 |
| NIN | 261 0/ | | | 1 | | 4.18 | 0.001 | 2/3.1 | 0022.0 | 0, 0 | 2160.0 |
| ě | | 4.5 | 0.0116 | 8/ | 1.28 | | ot 110 | | 5 | 2 | 0.0098 |
| 8 5 | 67°0 | (67 | 10.1 | 0/T | 4.02 | VIVO | 27 190 | DAIA SI | CO 13 | 9 9 | 0 204 |
| 120 | 1.65# | | | ()) ()) | -02.1 | 71 | 0.0665 | 1726 | 87.1 | 2 | 0.625 |
| 140 | 2.05 | | | 323 | 9.14 | 16 | 0.0666 | N | | 100 | 1.033 |

N1 (continued)

TABLE 12. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF NICKEL

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TABLE 12. EXPERIMENTAL DATA ON THE ELECTRICAL RESISTIVITY OF NICKEL N1 (continued)

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Ser.

| H | þ | L | d | Ţ | φ | L | d | T | đ | T | p |
|----------------|-----------------|----------------|----------------|----------|--------------|---------------|---------|----------|-------------|------------|------------------|
| DATA SET | . 89(cont.) | DATA SET | 91(cont.)* | DATA SET | 92(cont.) | DATA SET 94 (| cont.)* | DATA SET | 4(cont.)* | DATA SET 9 | 5(cont.)* |
| 160 | 2.584 | 631.6 | 28.78 | 1496 | 57.1 | 74.1 | 0.30 | 271.2 | 6.35 | 875.2 | 26.360 |
| 200 | 3.784* | 631.7 | 28.80 | 1589 | 59.4 | 76.6 | 0.30 | 276.2 | 6.35 | 897.0 | 26.728 |
| 202 | 1,001 | 0.100 | 20,02 | 5621 | 9.20 | 1 /0 | 0.20 | 2.107 | 7 31 | 7.CU6 | 016.02 |
| | 8.747* | 1 263 | 28.85 | 67/1 | 07.0 86.6 | 04.1 86.6 | 0.94 | 205.0 | | 071 7 | 01 010 |
| 576 | 10.54* | 632.5 | 28.88 | 2176 | 86.1 | 89.1 | 0.61 | 301.3 | 7.63 | 940.6 | 27.647 |
| 433 | 12.52 | 632.7 | 28.91 | 2391 | 87.6 | 91.6 | 0.93 | | 8 1 • | 971.2 | 28.016 |
| 473 | 14.69* | 633.2 | 28.94 | 2606 | 88.7* | 94.1 | 0.61 | DATA S | ET 95* | 993.0 | 28.572 |
| 533 | 18.37* | 633.7 | 28.97 | 2719 | 89.6* | 99.2 | 0.93 | | | 1006.1 | 28.753 |
| 573 | 21.20* | 634.3 | 29.00 | 2875 | 90°6* | 102.9 | 0.93 | 294.8 | 5.161 | 1010.5 | 28.753 |
| 673 | 29.93* | 634.8 | 29.05 | 2989 | 91.3 | 106.7 | 1.25 | 303.5 | 5.348 | 1019.2 | 28.940 |
| | 33.32" 36 0/ | 635.5 635 0 | 80.62 | 0 TATA 0 | ст 03 | 111./ | 1.25 | 312.3 | 5.80P | 102/.9 | 29.122 |
| | | 636.3 | 20.14 | | | 120.5 | 1.57 | 1.926 | 5.898 | 1058.5 | 29.859 |
| DAT | A SET 90 | 636.9 | 29.20 | 1723 | 57.0 | 124.3 | 1.24 | 338.5 | 6.267 | 1062.8 | 29.859 |
| | | 637.7 | 29.23 | 1723 | 60.8 | 128.0 | 1.89 | 382.1 | 7.741 | 1089.0 | 30.228 |
| 10 | 0.0037 | 638.2 | 29.25 | 1724 | 79.6 | 129.3 | 1.89 | 390.8 | 7.741 | 1097.7 | 30.415 |
| 20 | 0.016 | 638.8 | 29.31 | 1733 | 83.4 | 134.3 | 1.89 | 399.5 | 8.110 | 1106.5 | 30.597 |
| ຂ | 0.036 | 639.5 | 29.34 | 1757 | 83.4 | 139.3 | 1.56 | 408.3 | 8.445 | 1115.2 | 30.597 |
| 40 | 0.0792 | 640.1 | 29.37 | 1779 | 83.5 | I43.I | 2.21 | 434.5 | 9.584 | 1115.2 | 30.965 |
| 93 | 0.2623 | 640.5 | 29.40 | 1782 | 83.5* | 146.9 | 2.20 | 451.9 | 10.140 | 1132.6 | 30.965 |
| 80 | 0.5764 | 641.1 | 29.46 | 1812 | 83.6 | 153.2 | 2.20 | 456.3 | 10.509 | 1145.7 | 31.339 |
| 001 | 0.985 | 641.5 | 29.46 | 1843 | 83.7 | 160.7 | 2.20 | 478.1 | 11.615 | 1158.8 | 31.708 |
| 160 | 2.503 | 642.1 | 29.48 | | | 165.7 | 2.84 | 499.9 | 12.352 | 1180.6 | 31.889 |
| 200 | 3.683 | 642.8 | 29.54 | DATA | SET 94* | 169.5 | 2.84 | 521.7 | 13.458 | 1193.7 | 32.076 |
| 260 | 5.735 | 643.2 | 29.54 | | | 175.8 | 2.84 | 547.9 | 14.932 | 1198.1 | 32.258 |
| | | 644.0 | 29.60 | 1.5 | 0.10 | 180.8 | 3.16 | 569.7 | 16.407 | 1206.8 | 32.258 |
| DATA | SET 91* | 644.7 | 29.66 | 8.7 | 0.10 | 183.3 | 3.16 | 587.2 | 17.326 | 1224.3 | 32.627 |
| 0 | | 642.3 | 29.69 | 10.2 | 0.11 | 188.3 | 3.80 | 591.5 | 17.594 | 1241.7 | 32.627 |
| 6.220 | 21.13 | 6.040 | 29.14 | 14.6 | 0.11 | 193.3 | 3.80 | 9.262 | 17.694 | 1267.9 | 33.364 |
| 1.620 | 70.12 | 04/.4 | 11.67 | 23.1 | 0.12 | 1.141 | 3.80 | 600.5 | 17.881 | 17/0.1 | 53, 504 |
| 024.4 675.7 | 16.12 | 040.0 | 29.83 20.02 | 2.82 | 0.13 | 203.4 | 3.8U | 0.4.0 | 18.003 | 1302.8 | 54-101 14 470 |
| 626 7 | 28 11 | 6.040 | 20.07 70.86 | 0.00 | 51.0 | 7 616 | 4.12 | 1.110 | 10 160 | 1.1251 | 15 075 |
| 626.9 | 28.17 | 649.6 | 29.89 | 8.85 | 0.16 | 217.2 | 4.76 | 635.2 | 19.538 | 1363.9 | 35.207 |
| 627.3 | 28.25 | 650.1 | 29.91 | 4.1.4 | 0.18 | 221.0 | 4.76 | 635.2 | 20.275 | 1390.1 | 35.576 |
| 627.7 | 28.31 | | | 44.1 | 0.20 | 226.0 | 4.76 | 643.9 | 20.643 | | |
| 628.2 | 28.37 | DATA 5 | SET 92 | 45.9 | 0.21 | 232.2 | 4.75 | 670.1 | 21.199 | DAT | A SET 96 |
| 628.8 | 28.42 | | | 50.2 | 0.30 | 236.0 | 5.40 | 687.5 | 21.936 | | |
| 629.2 | 28.48 | 508 | 20.0* | 52.7 | 0.30 | 239.8 | 5.40 | 709.4 | 22.487 | 1.51 | 0.002574 |
| 629.8 | 28.54 | 638 | 31.8* | 55.2 | 0.30 | 243.5 | 5.39 | 7.35.5 | 22.855 | 1.79 | 0.002581 |
| 630.2 | 28.60 | 769 | 37.9* | 59.0 | 0.30 | 247.3 | 5.72 | 761.7 | 23.592 | 1.93 | 0.002593 |
| 630.7 | 28,68 | 886 | *6 .14 | 62.8 | 0.30 | 252.3 | 6.04 | 787.9 | 24.330 | 2.08 | 0.002600 |
| 631.0 | 28.71 | 1029 | 45.9* | 65.3 | 0.30 | 256.1 | 6.03 | 814.1 | 24.698 | 2.20 | 0.002626* |
| 631.2 | 28.74 | 1206 | 50.3 | 67.8 | 0.30 | 262.4 | 6.35 | 840.3 | 25.436 | 2.44 | 0.002638* |
| 4°760 | 28.11 | 1345 | 53.5 | 70.3 | 0.30 | 266.1 | 6.35 | 857.1 | 25.991 | 2.64 | 0.00264/* |
| | | | | | | | | | | | |

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* Not shown in figure.

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| Mrs. Str. M(cert.) Mrs. Str. M(cert.) Mrs. Str. M(cert.) Mrs. Str. M(cert.) $2, 0 = 0.000331$ 19.0 1.4 5.3 2.10 $1, 0 = 0.000331$ 19.0 1.4 5.3 2.10 $1, 0 = 0.000331$ 19.0 1.5 5.3 2.10 $1, 0 = 0.000331$ 19.0 1.5 5.3 2.10 $1, 0 = 0.000331$ 19.0 1.3 1.3 1.3 $1, 0 = 0.000314$ 19.0 1.3 1.3 1.3 $1, 0 = 0.000314$ 19.0 1.3 1.3 1.3 $1, 0 = 0.000314$ 19.0 1.3 1.3 1.3 $1, 0 = 0.000314$ 19.0 1.3 1.3 1.3 $1, 0 = 0.000314$ 19.0 1.3 1.3 1.3 $1, 2 = 0.000314$ 19.1 1.3 1.3 1.3 $1, 2 = 0.000314$ 19.1 1.3 1.3 1.3 $1, 2 = 0.000314$ 19.1 1.3 1.3 1.3 $1, 2 = 0.000314$ 10.1 | MXA SFT MAXA SFT IOI (cont.) MXA SFT IOI (cont.) | <pre>IO1(cont.)* DATA SET 103(cont.)</pre> |
|---|--|--|
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | |
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| (62 (6).75 1766 87.65 42 0.0145 7/16 87.05 1792 87.05 1792 87.05 7/16 87.05 1792 87.05 1792 88.05 M/IA SET 107* 7/17 60.13* 1806 88.05 M/IA SET 107* 0.0834 7/17 60.13* 1806 88.2 42 0.00834 7/18 87.4 1806 88.2 42 0.00834 7/19 87.55* 1823 88.35 M/IA SET 108* 42 0.00834 7/19 87.55* 1823 88.35 M/IA SET 109* 42 0.0054 7/19 87.5 1824 88.65 42 0.0054 42 0.00424 7/10 87.1 88.15 9.1 42 0.00424 81 87.1 1877 88.45 42 0.00424 81 88.45 9.1 42 0.00424 42 0.00424 | 692 60.75 1766 87.65 4.2 0.0145 711 61.2 1792 88.05 88.05 97.25 1795 88.05 97.16 770 87.25 1795 88.05 96.05 97.42 0.0145 770 87.25 1795 88.05 96.05 97.42 0.00834 770 87.25 1800 88.05 97.42 0.00834 799 87.55 1802 88.35 97.1 97.9 794 87.55 1823 88.35 97.1 97.9 817 87.9 1826 88.35 97.1 97.9 817 87.9 186.5 88.6 97.1 97.2 840 88.1 1865 88.6 97.2 0.00424 857 88.3 98.1 4.2 0.00424 866 88.45 97.00 97.100 4.2 0.00424 867 88.45 97.103 4.2 0. | 87.7 DATA SET 106* |
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4. ACKNOWLEDGMENTS

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5. APPENDICES

5.1. Methods for the Measurement of Electrical Resistivity

At the Center for Information and Numerical Data Analysis and Synthesis (CINDAS) of Purdue University, the experimental methods for the measurement of electrical resistivity have been classified into various categories according to a similar scheme used by CINDAS for the classification of methods for the measurement of thermal conductivity [264, pp. 13a-25a]. This classification scheme of CINDAS is presented below. Note that the letters in parentheses following the respective methods are the code letter used in the "Method Used" column of the Table of Measurement Information for indicating the experimental methods used by the various authors.

Methods for the Measurement of Electrical Resistivity

- A. Steady-State Methods
 - Voltmeter and ammeter direct reading method (V) [265, p. 159; 266, pp. 244-5]
 - 2. Direct-current potentiometer method (A) [267, pp. 151-8]
 - a. 4-probe potentiometer method
 - 3. Direct-current bridge methods (B) [267, pp. 144-51]
 - a. Kelvin double bridge method
 - b. Mueller bridge method
 - c. Wheatstone bridge method
 - 4. Van der Pauw method (P) [268, 269]
 - 5. Galvanometer amplifier method (G) [270, pp. 159-62]

B. Non-Steady-State Methods

- 1. Periodic current method
 - a. Direct connection to sample
 - (1) Alternating-current potentiometer method (C) [267, pp. 161-2]
 - (2) Alternating-current bridge method (D) [267, p. 162]
 - b. No connection to sample
 - (1) Mutual inductance method (M) [271]
 - (2) Self-inductance method (S) [272]
 - (3) Rotating field method (R) [273]

- 2. Non-periodic current method
 - a. Direct connection to sample
 - (1) Transient (subsecond) method (T) [154]
 - b. No connection to sample
 - (1) Eddy current decay method (E) [273; 267, p. 103]

5.2. Conversion Factors for the Units of Electrical Resistivity

The recommended values and experimental data for the electrical resistivity tabulated in this work are in the units: $10^{-8} \Omega m$. Conversion factors for the units of electrical resistivity, which may be used to convert the values given in $(10^{-8} \Omega m)$ to values in other units, are given below.

| Units to be Converted to | Multiply the Value Given in (10 ⁻⁸ Ωm) by |
|--|---|
| ohm-meter (Ω m) | 1×10^{-8} |
| ohm-centimeter (Ω cm) | 1×10^{-6} |
| ohm-inch (Ω in.) | 3.937×10^{-7} |
| ohm-foot (Ω ft) | 3.281×10^{-8} |
| microohm-centimeter ($\mu\Omega$ cm) | 1 |
| abohm-centimeter (ab Ω cm) | 1×10^{3} |
| statohm-centimeter (stat Ω cm) | 1.113×10^{-18} |
| emu (= abΩ cm) | 1×10^{3} |
| esu (= statΩ cm) | 1.113×10^{-18} |
| ohm-circular mil per foot (Ω cmil ft ⁻¹) | 6.015 |

Conversion Factors for the Units of Electrical Resistivity

Example: $1.000 \times 10^{-8} \Omega m = 3.937 \times 10^{-7} \Omega$ in..

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